

MESOSCALE COMPONENTS OF THE GEOSTROPHIC
FLOW AND ITS TEMPORAL AND SPATIAL
VARIABILITY IN THE CALIFORNIA
CURRENT OFF MONTEREY BAY
IN 1973-74

Richard Earl Greer

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THESIS

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IN 1973-74

by

Richard Earl Greer

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Seasonal variations of the geostrophic flow and salt transport were congruent with Skogsberg's [1936] annual cycle composed of three distinct oceanographic seasons.

The flow and structure in the area are complex with flow elements less than 10 km in width. The data suggest that observations on a sampling grid length less than 10 km transverse to the current flow, and extensive independent current measurements are required to describe adequately the small-scale features of the flow, structure and its time variations.

Mesoscale Components of the Geostrophic Flow
and its Temporal and Spatial Variability
in the California Current off Monterey Bay
in 1973-74

by

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ABSTRACT

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Patterns of current flow indicated by drogues and geostrophy tend to confirm an analysis of the structure which has alternating elements of poleward and equatorward flow. Surface current flow patterns are similar to those found at depths to 375 m. The bottom topography influences the direction of flow inside the 1,000 fathom curve.

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I. INTRODUCTION

Eastern boundary currents, in particular, the California Current, have held the interest of investigators for many years. This is due largely to an avid interest in coastal upwelling, and its important implications on commercial fisheries and related economic enterprises. However, there are other important aspects. Of interest is the poleward countercurrent found close to the prevailing equatorward surface currents. The countercurrent is usually narrower, and found shoreward of the equatorward flow. During the winter months (November through February), and in the absence of prevailing north-northwesterly winds, the poleward countercurrent extends to the surface and is known as the Davidson Current north of Pt. Conception. With the onset of north-northwesterly winds in the spring, upwelling begins to occur along the California coast, and the poleward countercurrent disappears above 200 m. Where the flow is submerged, the countercurrent has been termed an "undercurrent." Of importance is that the poleward countercurrent continues throughout the year at speeds approximately 30 cm/sec or less. Consequently, the water off the California coast tends to have some of the high temperature and salinity characteristics of the low-latitude or "southern waters" (in the Northern Hemisphere). Accordingly, with the poleward transport of warm and salty southern waters, the resulting flow and structure along the California coast will necessarily

be highly complex. In fact, spatially dense observations in consecutive years in a region within 50 km of the continental shelf show a complex structure of southern water undergoing dilution by mixing as it flows northward [Wickham, 1975].

At present, there are many questions still outstanding about the countercurrent, and the resulting highly complex current regime off the California coast. It is the intent of this author to provide answers to a few of them. Specifically, using a data base constructed from spatially dense STD observations off Monterey Bay in 1973-74, an attempt will be made to examine the following,

- (1) The patterns of current flow, and their structure with depth,
- (2) The temporal variation of the geostrophic flow,
- (3) Mesoscale components of the geostrophic current and salt transport.

Additionally, attention will be given to the influence of bottom topography on the direction of flow inside the 1,000 fathom curve, the dependence of geostrophic current on the choice of reference level, and the use of geostrophy to depict small-scale features of the complex flow.

II. THE DATA

A. AREA OF INVESTIGATION AND DATA COLLECTION

The area of investigation is shown in figure 1, in which the major features of the bottom topography are depicted. The major topographical features of the area include Monterey Bay and the Monterey Canyon. The area of investigation lies within the rectangular parallelepiped located just west of the continental shelf off Monterey, California. It extends from the surface to a maximum depth of 725 meters and is bounded by the coordinates, $36^{\circ} 20'N$, $36^{\circ} 50'N$, $122^{\circ} 00'W$, and $123^{\circ} 00'W$.

The data were obtained from thirteen cruises aboard the *Acania*, the oceanographic vessel of the U.S. Naval Postgraduate School, during the months August 1973 through August 1974. A cruise was conducted once each month during various days of the thirteen-month period. On each cruise observations were made along a horizontal grid much finer than traditionally used in oceanographic surveys to permit increased horizontal definition. Specifically, stations were located along four constant latitude lines normal to the coast at a maximum spacing of 5.6 km between stations; at least one line of stations being occupied on a cruise. Station positions are shown in figure 2, and listed in table I.

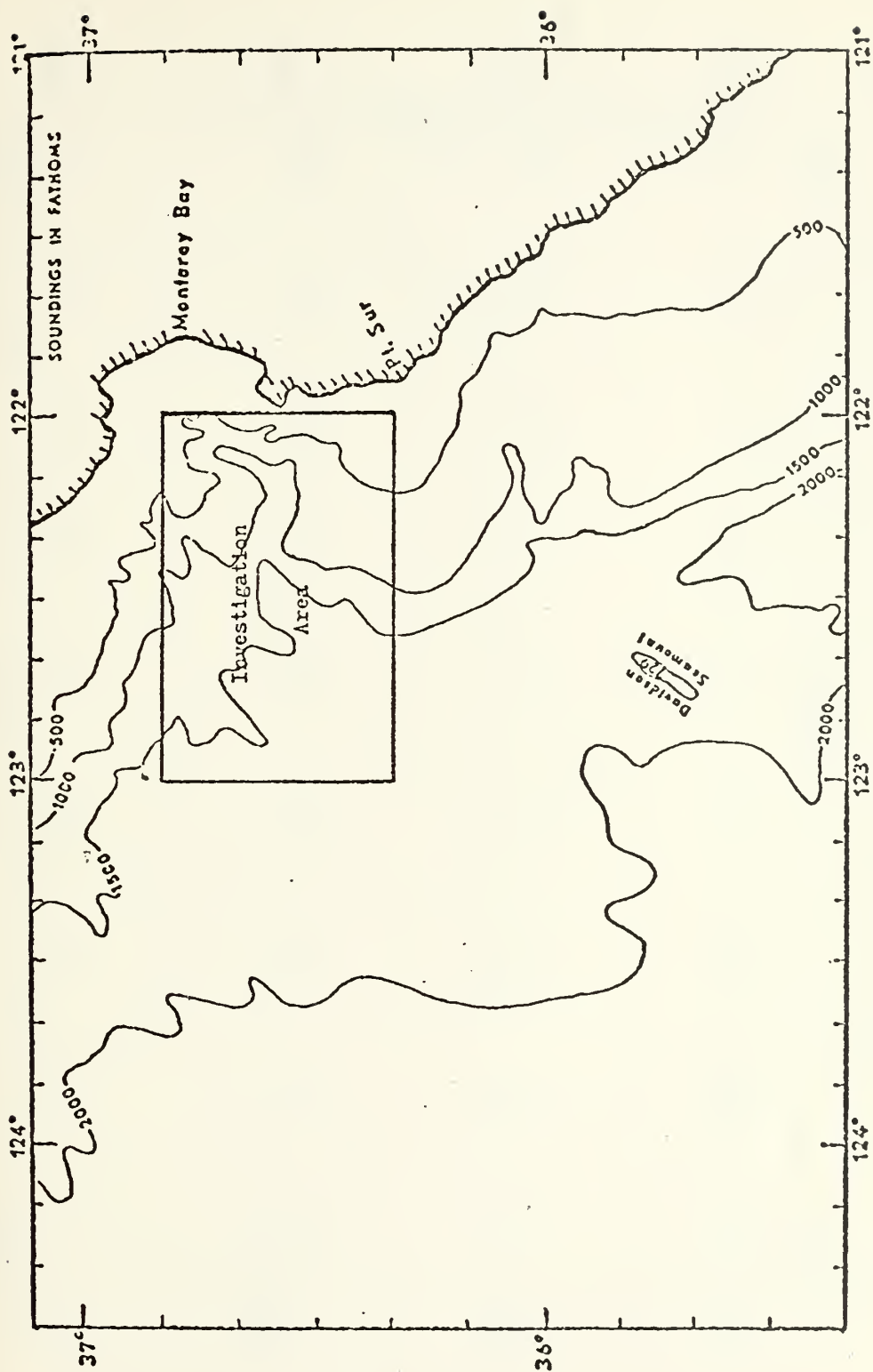


Fig. 1. Major Geographical and Topographical Features of the Investigation area.

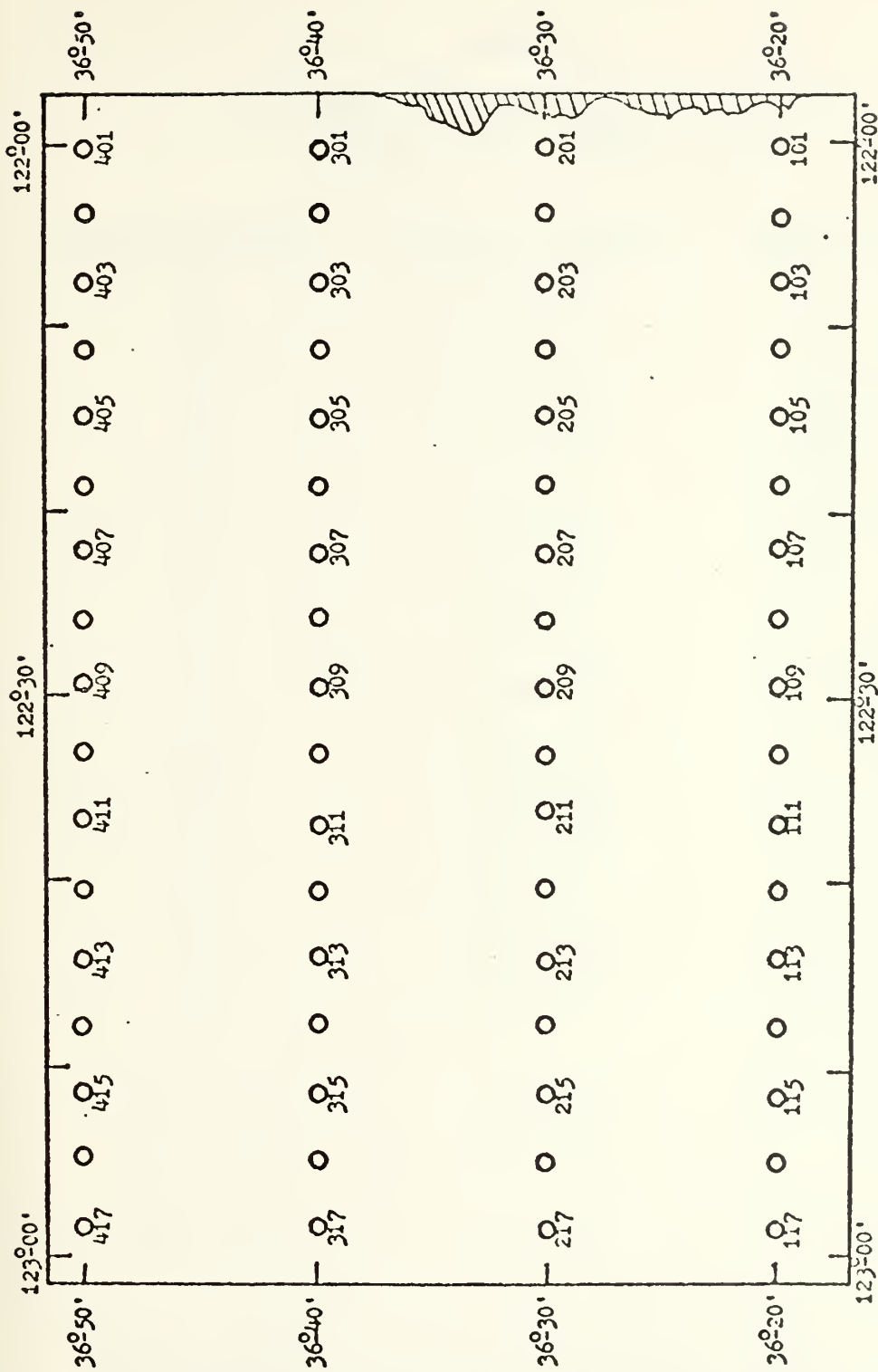


Fig. 2. The Location of Station Positions within the Investigation Area.

TABLE I
LATITUDE AND LONGITUDE OF STATIONS
(August 1973 - August 1974)

<u>Station Numbers</u>	<u>Latitude (North)</u>	<u>Longitude (West)</u>
101	36 ⁰ 20.0'	122 ⁰ 00.0'
102	36 ⁰ 20.0'	122 ⁰ 03.6'
103	36 ⁰ 20.0'	122 ⁰ 07.3'
104	36 ⁰ 20.0'	122 ⁰ 10.9'
105	36 ⁰ 20.0'	122 ⁰ 14.5'
106	36 ⁰ 20.0'	122 ⁰ 18.2'
107	36 ⁰ 20.0'	122 ⁰ 21.8'
108	36 ⁰ 20.0'	122 ⁰ 25.4'
109	36 ⁰ 20.0'	122 ⁰ 29.1'
110	36 ⁰ 20.0'	122 ⁰ 32.7'
111	36 ⁰ 20.0'	122 ⁰ 36.4'
112	36 ⁰ 20.0'	122 ⁰ 40.0'
113	36 ⁰ 20.0'	122 ⁰ 43.6'
114	36 ⁰ 20.0'	122 ⁰ 47.3'
115	36 ⁰ 20.0'	122 ⁰ 50.9'
116	36 ⁰ 20.0'	122 ⁰ 54.5'
117	36 ⁰ 20.0'	122 ⁰ 58.2'
201 - 217	36 ⁰ 30.0'	*
301 - 317	36 ⁰ 40.0'	*
401 - 417	36 ⁰ 50.0'	*

* Station with same last two digits as 100 series have the same longitude with the exception of station 211, which is located at 36⁰ 30.0'N, and 122⁰ 35.8'W.

B. PROCEDURE

The thirteen cruises aboard the Acania during the period August 1973 through August 1974 provided the data base for this study. Original cruise plans called for all thirteen cruises to utilize the Bissett-Berman continuous profiling STD as the primary observational tool in conjunction with reversing thermometers and Nansen samples, which would provide independent measurements for comparison of temperature and salinity and standardization of the STD. Additionally, expendable bathythermograph (XBT) and surface (bucket) temperatures would provide data for further comparisons. However, due to STD malfunction or in the interest of time-saving the original cruise plans were modified. Specifically, seven cruises utilized the STD as their primary observational tool, while five of the remaining six cruises utilized the XBT. The remaining cruise conducted during April 1974 was terminated early due to equipment malfunction and poor weather conditions.

On STD cruises, a Bissett-Berman continuous profiling instrument (STD) sensed the vertical distributions of temperature and salinity. To obtain vertical definition of approximately two meters, the STD was lowered at a rate of 30 meters per minute. Profiles were recorded for both descent and ascent of the STD so that, during the digitizing of analog traces, spurious spikes in the salinity record could be recognized and eliminated by manual trace smoothing techniques described in the section on data processing. The spikes are known to be caused by a mismatch of time constants between the temperature and conductivity sensors.

On other cruises, expendable bathythermograph (XBT) soundings were utilized to delineate the vertical distributions of temperature. To supplement the XBT temperature data, three Nansen casts were conducted per station line at the eastern, western and mid-sectors of the investigation area. Water samples were taken at the following nine depths: 0, 20, 50, 100, 200, 300, 400, 500 and 750 meters. Obviously, the spacing between hydrocast stations and the interval between water sampling depths did not permit the vertical and horizontal definition of salinity achieved on cruises where the STD was primary. However, hydrocast stations added importantly to the information obtained in the study area.

On all thirteen cruises, independent measurements of temperature and salinity were made, respectively, with reversing thermometers and with laboratory conductivity analysis of sea water samples taken from Nansen bottles. Additionally, surface (bucket) and thermograph temperatures were recorded at each station. These independent measurements and their use are discussed later in the section on data processing.

C. INSTRUMENTATION

The STD instrument used was the Bissett-Berman STD Model 9006. Manufacturer's specifications claim an accuracy of $\pm 0.02^{\circ}\text{C}$ and ± 0.02 ppt for temperature and salinity, respectively.

Data were recorded on a continuous analog chart recorder during both descent and ascent of the STD. Data obtained during ascent of the STD were used only to smooth the salinity

record and eliminate false salinity spikes. Although data taken from the up and down casts were in good general agreement, only down trace data were digitized and used for analyses. See Data Processing section for further details.

III. DATA PROCESSING

A. PROCEDURE

Analog strip chart data obtained from the thirteen cruises conducted during August 1973 through August 1974 were manually smoothed, digitized and recorded on a Calma Digitizer 7-track tape recorder. The digitized salinity, temperature and depth data were then read, converted and processed by means of program "DIGISTD" developed for use with the IBM 360 computer. The temperature, salinity and depth data along with calculated values of sound velocity and sigma-t were then grouped according to chronological order and station and written onto 9-track tape. Additionally, salinity and temperature data for every 2.5 meters of depth were output to punched cards for use with a modified version of the HYDRO program to make dynamic height and geostrophic current calculations. These geostrophic current velocities were then used in computations of geostrophic salt transport.

B. DATA PREPARATION

Prior to digitization of the analog data, false salinity spikes caused by the mismatch of time constants between the sensors for temperature and conductivity used to calculate salinity had to be recognized and eliminated. Recognition of spurious salinity spikes was accomplished by comparison of the trace records obtained from the descent and ascent of the STD. Specifically, salinity spikes which were of opposite

sign between the up and down traces of a particular station were assumed to be spurious, and were eliminated. This elimination was accomplished by manually smoothing through the spike along the general trend of the salinity record. This technique involves some qualitative judgment or artistic license; however, salinity trace smoothing was done consistently and appears to represent quite well the true structure. This is borne out by the fact that within the accuracy limitations of the other steps in the digitization process, the densities (sigma-t values) computed from the temperature and smoothed salinity data increased monotonically with increasing depth with few exceptions. The paucity of apparent instabilities, i.e., regions of

$$\frac{d\sigma_t}{dz} < 0 ,$$

and the uniformity of the trace-smoothing process tends to justify the data preparation process.

C. DIGITIZATION

Digitization of the cruise data was a portion of the joint (Greer, Blumberg and Hughes) data work-up. Both the STD and XBT strip chart data obtained from the thirteen cruises conducted during August 1973 through August 1974 were digitized on two Calma Digitizers owned by the Fleet Numerical Weather Center, Monterey, California. The Calma Company Model 480 Digitizer reduces analog graphical data to digital form for computer processing and analysis.

To digitize analog graphical data directly on computer compatible 7-track magnetic tape, the operator selects tracer mode and manually traces the graphical data with a moveable stylus/carriage assembly. The movements of the stylus in the X and Y directions are transmitted to magnetic encoders, which convert the stylus movements in 0.01 inches to digital signals. These signals are processed and formatted for output to 7-track computer magnetic tape. The digital data are recorded on tape at a bit density of 556 BPI.

In addition to the digitization tracer mode, the Calma Digitizer has a manual keyboard entry mode for identification of data on the tape, entering inter-record gaps, record errors, and delete records. The keyboard mode was used in conjunction with each digitized trace segment to identify the particular data station number, month and year, temperature, salinity and depth scales, last trace segment, and whether it was a temperature or salinity trace. Consequently, the output tape was constructed so that every other record was a 13-character keyboard mode entry which identified the following data trace record.

The Calma Digitizer variable interval programmer monitors the output recorder and generates signals every 0.01 inches of stylus movement in the X and Y directions if the stylus is moved at a rate less than 125 inches per minute. At higher rates, the data signals are recorded at 0.02 inches of stylus travel. All cruise data were digitized at 0.01 inches of stylus movement.

The STD data were digitized in segments since the temperature and salinity traces were not continuous due to scale changes in salinity, temperature and depth during collection of the data. Typically, an STD trace consisted of four temperature and two salinity segments. In contrast, the XBT traces consisted of one continuous segment. Consequently, digitizing an STD trace took approximately five times as long as an XBT trace.

D. CALIBRATION AND STANDARDIZATION

On all thirteen cruises, independent measurements of temperature and salinity were made, respectively, with reversing thermometers and with laboratory conductivity analysis of sea water samples taken from Nansen bottles. These independent measurements were used for field calibration of the STD, and to provide standardization of the STD and XBT data permitting qualitative discussion and comparison of the seasonal variation over the thirteen-month period.

In standardizing both the STD and XBT data, the Nansen temperatures and salinities were considered to be the actual or correct temperature and salinity values. Upon examination and comparison of the STD data with the Nansen data, the STD was found to read high in temperature by 0.08°C for all primary STD data collection months, and low in salinity by 0.04 ppt for data months November 1973 through January 1974, and August 1974. Consequently, the STD temperatures and salinities were decreased and increased respectively to align the STD data with the independent Nansen data.

Standardization of the XBT data was accomplished in a similar manner. However, independent Nansen data were not available, in all cases, for corresponding XBT data stations. Therefore, when corresponding Nansen data were not available, the XBT was corrected to the already standardized STD. Adjustment of the XBT to the standardized STD data made qualitative discussion and comparison of the seasonal variation over the thirteen-month period possible. The corrections were determined by a best-fit curve developed by a computer routine fitting the XBT data with Nansen data when available or with the standardized STD data. Generally, temperature corrections varied from $+0.13^{\circ}\text{C}$ to -0.37°C for data months August 1973 through August 1974.

E. AUTOMATIC DATA PROCESSING PROGRAMS

Two computer programs, DIGISTD and DIGIXBT, were utilized to read, convert, and process the digitized salinity, temperature and depth data from the 7-track tapes produced on the Calma Digitizers. Both DIGISTD and DIGIXBT are extensively modified versions of an original program MIZ2 by R. G. Paquette. Indicative of their names, DIGISTD processes STD data and DIGIXBT processes expendable bathythermograph data. See appendices A and B for program documentation and listing.

DIGISTD and DIGIXBT convert and store STD and XBT data, respectively, every 0.01 inches of depth on the scale of the digitizer for output to printer, punched card or 9-track tape. Additionally, DIGISTD computes both sound velocity and sigma-t for each set of primary data.

During the data processing phase, all three output media, printer, punched card and 9-track tape, were utilized. Specifically, STD data were output every 0.08 inches of depth (approximately 2.5 meters) to punched card for later direct input into the HYDRO program to compute dynamic heights and geostrophic velocities. Although the number of output data cards produced by punching data points every 2.5 meters appeared to be unwieldy at the outset, this procedure proved manageable, and avoided needless programming problems in getting the correct data off the tape, and in the right order for input to program HYDRO.

F. GEOSTROPHIC CURRENT AND DYNAMIC HEIGHT CALCULATIONS

Geostrophic currents were computed by the dynamic method utilizing a modified version of the computer program, HYDRO, developed for use with the IBM 360 computer by the U.S. Naval Postgraduate School Department of Oceanography. A modified version of the HYDRO program is presented in appendix C. The two basic program modifications are: (1) an increased capability to process temperature and salinity data on a finer vertical scale (approximately 2.5 meters) than traditionally used in oceanographic surveys, and (2) an output card punching routine which produces composite data cards, each containing depth, temperature, salinity, geostrophic velocity, dynamic heights and mass transport values. The composite data cards are useful as input for plotting and contouring computer programs. Specifically, contour and plotting routine, CONTUR, was utilized to display graphically contours of dynamic heights, geostrophic

velocities and geostrophic salt transport on the off-line Calcomp plotter.

Dynamic heights and geostrophic speeds were calculated every ten meters of depth for the first 300 meters of depth, and less frequently for the remaining 200 meters. The ten meter interval proved extremely effective in depicting the complex velocity structure. However, the resulting detailed description of the structure and flow indicated that a larger data interval (every 20 meters for the first 300 meters, and every 50 meters thereafter) would have been sufficient to represent the fine scale structure. Consequently, data in the vertical need not be processed on an interval less than 20 meters. For the investigator processing STD data via cards, this will significantly reduce the number of data cards required for input into HYDRO.

G. GEOSTROPHIC SALT TRANSPORT CALCULATIONS

Geostrophic transport of salt or the salt flux per unit time-area is readily calculated as the product of density, average salinity and geostrophic velocity. Algebraically, the geostrophic salt transport, F_s , may be written as:

$$F_s = (V_{gs})(S)(\rho_{s,t,o}) \quad (1)$$

where

V_{gs} = geostrophic velocity (cm/sec)

S = average salinity (ppt)

$\rho_{s,t,o}$ = density (gm/cm³)

F_s = geostrophic transport of salt (gm/sec-cm²)

The total salt transport, T_s , or salt flux per unit time in area length, ΔX , in a layer of thickness, ΔZ , would be given by,

$$T_s = \int_{\Delta X} \int_{\Delta Z} F_s dz dx \quad (2)$$

Values of geostrophic transport of salt were calculated for every 20 meters of depth for the first 300 meters beginning at ten meters, and less frequently from 300 to 500 meters. To obtain an average salinity value corresponding to the geostrophic velocity computed between adjacent stations, an arithmetic mean was used. Specifically, to obtain an average salinity value at ten meters' depth between stations A and B, an arithmetic mean was computed using the surface, 10 and 20 meter salinity values at both adjacent stations A and B. This procedure was used to obtain a representative salinity value between adjacent stations, and to avoid using anomalous values of salinity in the salt transport calculations. The other variable, density, was considered constant over the entire vertical column due to its insignificant effect on the computations. A constant value of 1.026 gm/cm^3 was used for density.

IV. DISCUSSION AND RESULTS

A. THE GEOSTROPHIC CURRENT AND ITS LEVEL OF NO MOTION

The computation of geostrophic currents by the dynamic method has been discussed extensively in physical oceanography texts such as Neumann and Pierson [1966], and Stommel [1965]. The computation scheme is based on an equation derived by Sandström and Helland-Hansen [1903] from Bjerknes Circulation Theorem [1900]. In Oceanography, the equation is widely referred to as the Helland-Hansen equation, and has been extensively used to compute the relative field of currents from the observed field of mass. The equation may be written in terms of the horizontal pressure gradient of the geopotential between two levels P_1 and P_2 ,

$$V_2 - V_1 = \frac{\int_{P_1}^{P_2} \alpha_A dP - \int_{P_1}^{P_2} \alpha_B dP}{f \Delta X} \quad (3)$$

where

$f = 2\omega \sin \phi$, the coriolis parameter (1/sec)

ω = the angular velocity of the earth (radians/sec)

ϕ = the geographic latitude (degrees)

ΔX = the distance between stations A and B (kilometers)

α = specific volume (cm^3/gm); subscripts A and B refer to stations A and B

P = pressure (decibars)

$V_2 - V_1$ = the component of horizontal velocity normal to ΔX at P_1 relative to that at P_2 (cm/sec)

Equation (3) may be evaluated to obtain the mean geostrophic flow normal to a horizontal line joining stations A and B.

This method permits only the computation of relative velocities.

In order to arrive at the absolute currents, either the absolute pressure field or the absolute velocity must be known at least at one level between adjacent stations [Neumann and Pierson, 1966]. The absolute velocity may be found by determining the level or depth at which the currents become zero. In Oceanography, this depth is referred to as the 'level of no motion'. Some methods for estimating this reference level are given in the textbook, The Oceans, by Sverdrup, Johnson and Fleming, 1942, pp. 456-457. However, it is common practice to assume a depth where the currents become zero or to infer it from considerations of continuity.

An obvious way would be to determine the 'level of no motion' by direct measurements. However, this method has limitations due to the presence of other disturbances such as tidal currents, and the difficulty in sensing accurately relatively weak currents. Consequently, several investigators have attempted to corroborate their geostrophic current values, and indirectly their choice of reference level, by independent measurements of the current field by use of parachute drogues. For example, in a study of the California Current System off Baja, California, Reid, Swartzlose and Brown [1963] showed that geostrophic currents computed with respect to a 500 db reference level compared favorably with surface currents independently measured by drogues. On the other hand, other

investigators have found that they agree only roughly. Wickham [1975] in "Observations of the California Countercurrent" found that the local geostrophic current speeds agreed only roughly with the parachute drogue speeds. There are good reasons to expect differences between the actual flow and the results of geostrophy. First, there are obvious non-geostrophic components shown in the drogue speed values; and second, in the investigation area especially near the Monterey Canyon there are large internal waves known to exist, and finally, deformations of the reference isobaric surface (500 db) also must contribute to the difference between actual flow and the results of geostrophy [Wickham, 1975].

For this study, a reference level of 500 db was chosen as the 'level of no motion'. This choice was precipitated by the vertical extent (525 m) of the data in most cases and the success of earlier studies which found the 500 db reference to be suitable for the area.

During the months, January and August 1974, and October through December 1973, STD data were obtained to approximately 735 meters of depth at several stations. These deep station observations permitted geostrophic current calculations using the 700 db, 600 db and the 500 db levels as the reference level of no motion. Tables II through X are the resultant geostrophic currents from the surface to 475 meters relative to the three reference levels, and the velocity shears between the reference levels. To clarify the results contained in Tables II through X, the following variables are defined,

TABLE II

LEVEL OF NO MOTION ANALYSIS

OCTOBER 1973 - STATIONS 317-307

DEPTH	VEL.7,Z	VEL.6,Z	VEL.5,Z	VEL.7,5	VEL.7,6	VEL.6,5
(METERS)	---	---	---	---	---	---
Z	---	---	---	---	---	---
0.	1.87	2.56	2.95	-1.08	-0.69	-0.39
10.	1.07	1.76	2.15	-1.08	-0.69	-0.39
20.	-0.20	0.48	0.87	-1.07	-0.68	-0.39
30.	-1.39	-0.71	-0.32	-1.07	-0.68	-0.39
40.	-2.17	-1.49	-1.10	-1.08	-0.69	-0.39
50.	-2.98	-2.29	-1.90	-1.07	-0.68	-0.39
60.	-3.74	-3.06	-2.67	-1.08	-0.69	-0.39
70.	-4.33	-3.64	-3.25	-1.08	-0.69	-0.39
80.	-4.87	-4.13	-3.79	-1.08	-0.69	-0.39
90.	-5.23	-4.54	-4.15	-1.08	-0.69	-0.39
100.	-5.44	-4.75	-4.36	-1.08	-0.69	-0.39
110.	-5.55	-4.86	-4.47	-1.07	-0.68	-0.39
120.	-5.61	-4.93	-4.54	-1.08	-0.69	-0.39
130.	-5.67	-4.98	-4.59	-1.07	-0.68	-0.39
140.	-5.63	-4.95	-4.55	-1.07	-0.68	-0.39
150.	-5.56	-4.88	-4.49	-1.07	-0.68	-0.39
160.	-5.46	-4.78	-4.39	-1.07	-0.68	-0.39
170.	-5.35	-4.67	-4.28	-1.07	-0.68	-0.39
180.	-5.22	-4.54	-4.15	-1.08	-0.69	-0.39
190.	-5.05	-4.36	-3.97	-1.08	-0.69	-0.39
200.	-4.83	-4.14	-3.75	-1.07	-0.68	-0.39
210.	-4.58	-3.90	-3.51	-1.07	-0.68	-0.39
220.	-4.32	-3.64	-3.25	-1.07	-0.68	-0.39
230.	-4.06	-3.38	-2.99	-1.08	-0.69	-0.39
240.	-3.81	-3.12	-2.73	-1.08	-0.69	-0.39
250.	-3.56	-2.87	-2.48	-1.07	-0.68	-0.39
260.	-3.32	-2.64	-2.25	-1.07	-0.68	-0.39
270.	-3.10	-2.42	-2.03	-1.07	-0.68	-0.39
280.	-2.90	-2.22	-1.83	-1.08	-0.69	-0.39
290.	-2.71	-2.02	-1.63	-1.08	-0.69	-0.39
300.	-2.53	-1.84	-1.45	-1.08	-0.69	-0.39
310.	-2.36	-1.67	-1.28	-1.07	-0.68	-0.39
320.	-2.21	-1.52	-1.13	-1.07	-0.68	-0.39
330.	-2.06	-1.37	-0.98	-1.08	-0.69	-0.39
340.	-1.92	-1.23	-0.84	-1.08	-0.69	-0.39
350.	-1.79	-1.10	-0.71	-1.08	-0.69	-0.39
360.	-1.67	-0.98	-0.59	-1.08	-0.69	-0.39
370.	-1.56	-0.87	-0.48	-1.08	-0.69	-0.39
380.	-1.46	-0.77	-0.38	-1.08	-0.69	-0.39
390.	-1.37	-0.68	-0.29	-1.08	-0.69	-0.39
400.	-1.29	-0.60	-0.21	-1.08	-0.69	-0.39
410.	-1.22	-0.53	-0.14	-1.08	-0.69	-0.39
420.	-1.15	-0.46	-0.07	-1.08	-0.69	-0.39
430.	-1.09	-0.40	-0.01	-1.08	-0.69	-0.39
440.	-1.03	-0.34	0.05	-1.08	-0.69	-0.39
450.	-0.97	-0.28	0.11	-1.08	-0.69	-0.39
460.	-0.91	-0.22	0.17	-1.08	-0.69	-0.39
470.	-0.85	-0.16	0.23	-1.08	-0.69	-0.39
480.	-0.79	-0.10	0.29	-1.08	-0.69	-0.39
490.	-0.73	-0.04	0.35	-1.08	-0.69	-0.39
500.	-0.67	0.02	0.41	-1.08	-0.69	-0.39
510.	-0.61	0.08	0.47	-1.08	-0.69	-0.39
520.	-0.55	0.14	0.53	-1.08	-0.69	-0.39
530.	-0.49	0.20	0.59	-1.08	-0.69	-0.39
540.	-0.43	0.26	0.65	-1.08	-0.69	-0.39
550.	-0.37	0.32	0.71	-1.08	-0.69	-0.39
560.	-0.31	0.38	0.77	-1.08	-0.69	-0.39
570.	-0.25	0.44	0.83	-1.08	-0.69	-0.39
580.	-0.19	0.50	0.89	-1.08	-0.69	-0.39
590.	-0.13	0.56	0.95	-1.08	-0.69	-0.39
600.	-0.07	0.62	1.01	-1.08	-0.69	-0.39
610.	-0.01	0.68	1.07	-1.08	-0.69	-0.39
620.	0.05	0.74	1.13	-1.08	-0.69	-0.39
630.	0.11	0.80	1.19	-1.08	-0.69	-0.39
640.	0.17	0.86	1.25	-1.08	-0.69	-0.39
650.	0.23	0.92	1.31	-1.08	-0.69	-0.39
660.	0.29	0.98	1.37	-1.08	-0.69	-0.39
670.	0.35	1.04	1.43	-1.08	-0.69	-0.39
680.	0.41	1.10	1.49	-1.08	-0.69	-0.39
690.	0.47	1.16	1.55	-1.08	-0.69	-0.39
700.	0.53	1.22	1.61	-1.08	-0.69	-0.39
710.	0.59	1.28	1.67	-1.08	-0.69	-0.39
720.	0.65	1.34	1.73	-1.08	-0.69	-0.39
730.	0.71	1.40	1.79	-1.08	-0.69	-0.39
740.	0.77	1.46	1.85	-1.08	-0.69	-0.39
750.	0.83	1.52	1.91	-1.08	-0.69	-0.39
760.	0.89	1.58	1.97	-1.08	-0.69	-0.39
770.	0.95	1.64	2.03	-1.08	-0.69	-0.39
780.	1.01	1.70	2.09	-1.08	-0.69	-0.39
790.	1.07	1.76	2.15	-1.08	-0.69	-0.39
800.	1.13	1.82	2.21	-1.08	-0.69	-0.39
810.	1.19	1.88	2.27	-1.08	-0.69	-0.39
820.	1.25	1.94	2.33	-1.08	-0.69	-0.39
830.	1.31	2.00	2.39	-1.08	-0.69	-0.39
840.	1.37	2.06	2.45	-1.08	-0.69	-0.39
850.	1.43	2.12	2.51	-1.08	-0.69	-0.39
860.	1.49	2.18	2.57	-1.08	-0.69	-0.39
870.	1.55	2.24	2.63	-1.08	-0.69	-0.39
880.	1.61	2.30	2.69	-1.08	-0.69	-0.39
890.	1.67	2.36	2.75	-1.08	-0.69	-0.39
900.	1.73	2.42	2.81	-1.08	-0.69	-0.39
910.	1.79	2.48	2.87	-1.08	-0.69	-0.39
920.	1.85	2.54	2.93	-1.08	-0.69	-0.39
930.	1.91	2.60	2.99	-1.08	-0.69	-0.39
940.	1.97	2.66	3.05	-1.08	-0.69	-0.39
950.	2.03	2.72	3.11	-1.08	-0.69	-0.39
960.	2.09	2.78	3.17	-1.08	-0.69	-0.39
970.	2.15	2.84	3.23	-1.08	-0.69	-0.39
980.	2.21	2.90	3.29	-1.08	-0.69	-0.39
990.	2.27	2.96	3.35	-1.08	-0.69	-0.39
1000.	2.33	3.02	3.41	-1.08	-0.69	-0.39

TABLE III

LEVEL OF NO MOTION ANALYSIS

OCTOBER 1973 - STATIONS 307-303

DEPTH	VEL.7,Z	VEL.6,Z	VEL.5,Z	VEL.7,5	VEL.7,6	VEL.6,5
(METERS)	---	---	---	---	---	---
Z	---	---	---	---	---	---
0.	0.75	0.95	1.62	-0.87	-0.20	-0.67
10.	-0.20	0.0	0.67	-0.87	-0.20	-0.67
20.	-0.29	0.09	0.58	-0.87	-0.20	-0.67
30.	-0.73	-0.53	0.14	-0.87	-0.20	-0.67
40.	-1.47	-1.27	-0.60	-0.87	-0.20	-0.67
50.	-2.02	-1.82	-1.15	-0.87	-0.20	-0.67
60.	-2.28	-2.08	-1.41	-0.87	-0.20	-0.67
70.	-2.53	-2.33	-1.66	-0.87	-0.20	-0.67
80.	-2.60	-2.40	-1.73	-0.87	-0.20	-0.67
90.	-2.70	-2.49	-1.82	-0.88	-0.21	-0.67
100.	-2.75	-2.55	-1.88	-0.87	-0.20	-0.67
110.	-2.72	-2.51	-1.84	-0.88	-0.21	-0.67
120.	-2.62	-2.43	-1.74	-0.88	-0.21	-0.67
130.	-2.51	-2.30	-1.63	-0.88	-0.21	-0.67
140.	-2.38	-2.18	-1.51	-0.87	-0.20	-0.67
150.	-2.26	-2.06	-1.39	-0.87	-0.20	-0.67
160.	-2.16	-1.96	-1.29	-0.87	-0.20	-0.67
170.	-2.05	-1.85	-1.18	-0.87	-0.20	-0.67
180.	-1.88	-1.68	-1.01	-0.87	-0.20	-0.67
190.	-1.77	-1.57	-0.90	-0.87	-0.20	-0.67
200.	-1.71	-1.51	-0.84	-0.87	-0.20	-0.67
210.	-1.72	-1.52	-0.85	-0.87	-0.20	-0.67
220.	-1.77	-1.57	-0.90	-0.87	-0.20	-0.67
230.	-1.86	-1.65	-0.98	-0.88	-0.21	-0.67
240.	-1.94	-1.74	-1.07	-0.87	-0.20	-0.67
250.	-1.96	-1.76	-1.09	-0.87	-0.20	-0.67
260.	-1.96	-1.76	-1.08	-0.88	-0.21	-0.67
270.	-1.92	-1.72	-1.05	-0.87	-0.20	-0.67
280.	-1.89	-1.69	-1.02	-0.87	-0.20	-0.67
290.	-1.85	-1.65	-0.98	-0.87	-0.20	-0.67
300.	-2.35	-2.14	-1.47	-0.87	-0.21	-0.67
330.	-2.35	-2.14	-1.47	-0.87	-0.21	-0.67
340.	-2.35	-2.14	-1.47	-0.87	-0.21	-0.67
375.	-2.12	-1.92	-1.25	-0.87	-0.20	-0.67
425.	-2.12	-1.92	-1.25	-0.87	-0.20	-0.67
475.	-1.28	-1.07	-0.40	-0.88	-0.21	-0.67

T A B L E I V
L E V E L O F N O M O T I O N A N A L Y S I S
N O V E M B E R 1 9 7 3 - S T A T I O N S 3 1 7 - 3 0 7

DEPTH (METERS)	VEL.7,Z	VEL.6,Z	VEL.5,Z	VEL.7,5	VEL.7,6	VEL.6,5
0.	-9.86	-9.54	-8.44	-1.42	-0.32	-1.10
10.	-10.22	-9.89	-8.79	-1.43	-0.33	-1.10
20.	-10.58	-10.25	-9.15	-1.43	-0.33	-1.10
30.	-10.79	-10.46	-9.36	-1.43	-0.33	-1.10
40.	-10.60	-10.28	-9.18	-1.42	-0.32	-1.10
50.	-10.69	-10.36	-9.26	-1.43	-0.33	-1.10
60.	-10.80	-10.47	-9.37	-1.43	-0.33	-1.10
70.	-10.74	-10.41	-9.31	-1.43	-0.33	-1.10
80.	-10.49	-10.16	-9.06	-1.43	-0.33	-1.10
90.	-10.23	-9.90	-8.80	-1.43	-0.33	-1.10
100.	-10.00	-9.68	-8.57	-1.42	-0.32	-1.11
110.	-9.79	-9.47	-8.37	-1.43	-0.33	-1.10
120.	-9.64	-9.31	-8.21	-1.43	-0.33	-1.10
130.	-9.45	-9.12	-8.02	-1.43	-0.33	-1.10
140.	-9.25	-8.92	-7.82	-1.42	-0.32	-1.10
150.	-9.06	-8.74	-7.64	-1.42	-0.32	-1.10
160.	-8.89	-8.57	-7.47	-1.43	-0.33	-1.10
170.	-8.73	-8.40	-7.30	-1.43	-0.33	-1.10
180.	-8.54	-8.21	-7.11	-1.43	-0.33	-1.10
190.	-8.32	-8.00	-6.90	-1.43	-0.32	-1.11
200.	-8.13	-7.81	-6.70	-1.43	-0.32	-1.11
210.	-7.91	-7.59	-6.48	-1.42	-0.32	-1.10
220.	-7.67	-7.35	-6.25	-1.43	-0.32	-1.10
230.	-7.43	-7.11	-6.00	-1.42	-0.32	-1.10
240.	-7.17	-6.85	-5.75	-1.43	-0.32	-1.10
250.	-6.92	-6.60	-5.50	-1.43	-0.33	-1.10
260.	-6.66	-6.33	-5.23	-1.42	-0.32	-1.10
270.	-6.37	-6.05	-4.95	-1.43	-0.33	-1.10
280.	-6.09	-5.76	-4.66	-1.43	-0.33	-1.10
290.	-5.87	-5.54	-4.44	-1.42	-0.32	-1.10
300.	-5.63	-5.31	-4.21	-1.43	-0.33	-1.10
330.	-4.59	-4.27	-3.16	-1.42	-0.32	-1.10
340.	-4.77	-4.45	-3.35	-1.43	-0.33	-1.10
375.	-2.74	-2.42	-1.33	-1.43	-0.32	-1.10
475.	-1.82	-1.50	-0.39	-1.43	-0.32	-1.11

T A B L E V

L E V E L O F N O M O T I O N A N A L Y S I S

N O V E M B E R 1 9 7 3 - S T A T I O N S 3 0 7 - 3 0 3

DEPTH	VEL.7,Z	VEL.6,Z	VEL.5,Z	VEL.7,5	VEL.7,6	VEL.6,5
(METERS)	VEL.7,Z	VEL.6,Z	VEL.5,Z	VEL.7,5	VEL.7,6	VEL.6,5
0.	6.20	5.23	3.41	2.79	0.97	1.82
10.	6.37	5.40	3.57	2.80	0.97	1.83
20.	6.57	5.60	3.77	2.80	0.97	1.83
30.	6.81	5.84	4.01	2.79	0.97	1.82
40.	7.25	6.28	4.46	2.79	0.97	1.82
50.	8.17	7.20	5.38	2.80	0.97	1.83
60.	8.57	7.60	5.77	2.79	0.97	1.82
70.	8.76	7.79	5.97	2.79	0.97	1.83
80.	8.81	7.85	6.02	2.79	0.96	1.83
90.	8.76	7.79	5.96	2.80	0.97	1.83
100.	8.79	7.82	5.99	2.80	0.97	1.83
110.	8.76	7.79	5.96	2.79	0.97	1.82
120.	8.73	7.76	5.94	2.79	0.97	1.82
130.	8.55	7.58	5.76	2.79	0.97	1.82
140.	8.52	7.55	5.72	2.80	0.97	1.83
150.	8.51	7.55	5.72	2.79	0.96	1.83
160.	8.61	7.64	5.82	2.79	0.97	1.82
170.	8.76	7.79	5.96	2.80	0.97	1.83
180.	8.94	7.97	6.14	2.80	0.97	1.83
190.	8.96	7.97	6.14	2.80	0.97	1.83
200.	9.16	8.19	6.37	2.79	0.97	1.82
210.	9.34	8.37	6.54	2.80	0.97	1.83
220.	9.49	8.46	6.64	2.79	0.97	1.82
230.	9.55	8.52	6.70	2.79	0.97	1.82
240.	9.61	8.58	6.75	2.80	0.97	1.83
250.	9.68	8.64	6.81	2.80	0.97	1.83
260.	9.67	8.71	6.88	2.80	0.97	1.83
270.	9.48	8.70	6.87	2.80	0.97	1.83
280.	9.39	8.51	6.69	2.79	0.97	1.82
290.	9.17	8.42	6.60	2.79	0.97	1.82
300.	7.66	8.20	6.37	2.80	0.97	1.83
340.	6.76	6.69	4.86	2.80	0.97	1.83
375.	6.76	5.79	3.97	2.79	0.97	1.82
425.	5.10	4.13	2.31	2.79	0.97	1.82
475.	3.44	2.47	0.64	2.80	0.97	1.83

T A B L E V I L E V E L O F N O M O T I O N A N A L Y S I S

DECEMBER 1973 - STATIONS 307-303

DEPTH	VEL.7,Z	VEL.6,Z	VEL.5,Z	VEL.7,5	VEL.7,6	VEL.6,5
(METERS)	---	---	---	---	---	---
Z	---	---	---	---	---	---
0.	-8.21	-6.17	-5.22	-2.99	-2.04	-0.95
10.	-7.92	-5.89	-4.93	-2.99	-2.03	-0.96
20.	-7.57	-5.54	-4.58	-2.99	-2.03	-0.96
30.	-7.01	-4.97	-4.01	-3.00	-2.04	-0.96
40.	-6.06	-4.02	-3.06	-3.00	-2.04	-0.96
50.	-4.75	-2.71	-1.75	-3.00	-2.04	-0.96
60.	-3.91	-1.87	-0.92	-3.00	-2.04	-0.95
70.	-3.35	-1.31	-0.35	-3.00	-2.04	-0.96
80.	-2.93	-0.89	0.07	-3.00	-2.04	-0.96
90.	-2.51	-0.47	0.49	-3.00	-2.04	-0.96
100.	-1.84	0.20	1.16	-3.00	-2.04	-0.96
110.	-1.20	0.84	1.80	-3.00	-2.04	-0.96
120.	-0.82	1.22	2.18	-3.00	-2.04	-0.96
130.	-0.48	1.56	2.52	-3.00	-2.04	-0.96
140.	-0.16	1.87	2.83	-2.99	-2.03	-0.96
150.	0.18	2.22	3.18	-3.00	-2.04	-0.96
160.	0.54	2.58	3.54	-3.00	-2.03	-0.96
170.	0.80	2.85	3.79	-2.99	-2.04	-0.96
180.	0.81	2.85	3.81	-3.00	-2.04	-0.96
190.	0.65	2.69	3.65	-3.00	-2.04	-0.95
200.	0.42	2.46	3.42	-3.00	-2.04	-0.96
210.	0.04	2.08	3.04	-3.00	-2.04	-0.96
220.	0.05	1.91	2.94	-2.99	-2.03	-0.96
230.	-0.12	1.78	2.87	-2.99	-2.03	-0.96
240.	-0.22	1.62	2.73	-3.00	-2.04	-0.96
250.	-0.32	1.45	2.58	-2.99	-2.03	-0.95
260.	-0.41	1.23	2.41	-2.99	-2.03	-0.96
270.	-0.49	1.05	2.25	-2.99	-2.03	-0.96
280.	-0.59	0.85	2.09	-3.00	-2.04	-0.96
290.	-0.71	0.63	1.94	-3.00	-2.04	-0.96
300.	-0.99	0.33	1.70	-2.99	-2.04	-0.95
340.	-1.19	0.05	1.48	-2.99	-2.04	-0.95
375.	-1.91	0.85	1.08	-2.99	-2.03	-0.96
425.	-2.85	-0.81	0.15	-3.00	-2.04	-0.96

T A B L E V I I L E V E L O F N O M O T I O N A N A L Y S I S J A N U A R Y 1 9 7 4 - S T A T I O N S 3 1 7 - 3 0 7

DEPTH	V E L O C I T I E S									
(METERS)	-(C M./ S E C.)									
Z	VEL.7,Z	VEL.6,Z	VEL.5,Z	VEL.7,5	VEL.7,6	VEL.6,5				
0.	-13.66	-13.63	-13.63	-0.03	-0.03	0.0				
10.	-14.41	-14.38	-14.38	-0.03	-0.03	0.0				
20.	-15.22	-15.20	-15.19	-0.03	-0.02	-0.01				
30.	-16.03	-16.01	-16.00	-0.03	-0.02	-0.01				
40.	-16.45	-16.42	-16.42	-0.03	-0.03	0.0				
50.	-16.98	-16.96	-16.95	-0.03	-0.02	-0.01				
60.	-15.29	-15.27	-15.27	-0.02	-0.02	0.0				
70.	-14.42	-14.39	-14.39	-0.03	-0.03	0.0				
80.	-13.52	-13.50	-13.49	-0.03	-0.02	-0.01				
90.	-12.58	-12.56	-12.55	-0.03	-0.02	-0.01				
100.	-11.65	-11.63	-11.62	-0.03	-0.02	-0.01				
110.	-10.80	-10.78	-10.77	-0.03	-0.02	0.0				
120.	-9.01	-9.98	-9.98	-0.03	-0.03	0.0				
130.	-8.36	-8.34	-8.33	-0.03	-0.02	-0.01				
140.	-7.57	-7.54	-7.54	-0.03	-0.03	0.0				
150.	-6.78	-6.75	-6.75	-0.03	-0.03	0.0				
160.	-6.06	-6.04	-6.03	-0.03	-0.02	-0.01				
170.	-5.41	-5.39	-5.39	-0.02	-0.02	0.0				
180.	-4.82	-4.79	-4.79	-0.03	-0.03	0.0				
190.	-4.26	-4.24	-4.23	-0.03	-0.02	-0.01				
200.	-3.75	-3.73	-3.72	-0.03	-0.03	0.0				
210.	-3.30	-3.27	-3.27	-0.03	-0.02	-0.01				
220.	-2.93	-2.91	-2.90	-0.03	-0.03	0.0				
230.	-2.67	-2.64	-2.64	-0.03	-0.02	-0.01				
240.	-2.44	-2.41	-2.41	-0.03	-0.03	0.0				
250.	-2.23	-2.20	-2.20	-0.03	-0.03	0.0				
260.	-2.04	-2.02	-2.01	-0.03	-0.02	-0.01				
270.	-1.86	-1.83	-1.83	-0.03	-0.03	0.0				
280.	-1.67	-1.65	-1.64	-0.03	-0.02	-0.01				
290.	-1.45	-1.43	-1.42	-0.03	-0.02	0.0				
300.	-1.23	-1.20	-1.19	-0.03	-0.02	-0.01				
340.	-0.82	-0.80	-0.79	-0.03	-0.02	0.0				
375.	-0.48	-0.45	-0.45	-0.03	-0.02	-0.01				
425.	-0.18	-0.16	-0.15	-0.03	-0.02	0.0				
475.	-0.04	-0.02	-0.01	-0.03	-0.02	-0.01				

T A B L E V I I I L E V E L O F N O M O T I O N A N A L Y S I S J A N U A R Y 1 9 7 4 - S T A T I O N S 3 0 7 - 3 0 3

DEPTH	VEL.7,Z	VEL.6,Z	VEL.5,Z	VEL.7,5	VEL.7,6	VEL.6,5
(METERS)	---	---	---	---	---	---
Z	---	---	---	---	---	---
0.	8.06	9.28	9.55	-1.49	-1.22	-0.27
10.	9.21	10.43	10.70	-1.49	-1.22	-0.27
20.	9.93	11.15	11.42	-1.49	-1.22	-0.27
30.	10.28	11.51	11.77	-1.49	-1.23	-0.27
40.	10.50	11.73	12.00	-1.50	-1.23	-0.27
50.	10.69	11.92	12.19	-1.50	-1.22	-0.27
60.	10.82	12.04	12.31	-1.49	-1.22	-0.27
70.	10.86	12.08	12.35	-1.49	-1.22	-0.27
80.	11.09	12.32	12.59	-1.50	-1.22	-0.27
90.	11.56	12.78	13.05	-1.49	-1.22	-0.27
100.	12.00	13.22	13.49	-1.49	-1.22	-0.27
110.	12.48	13.70	13.97	-1.49	-1.22	-0.27
120.	12.89	14.11	14.38	-1.50	-1.22	-0.27
130.	12.92	14.15	14.42	-1.50	-1.22	-0.27
140.	12.39	13.61	13.88	-1.49	-1.22	-0.27
150.	11.48	12.70	12.97	-1.49	-1.22	-0.27
160.	10.21	11.44	11.71	-1.50	-1.23	-0.27
170.	8.97	10.20	10.47	-1.50	-1.23	-0.27
180.	7.79	9.02	9.29	-1.50	-1.23	-0.27
190.	6.60	7.83	8.10	-1.50	-1.23	-0.27
200.	5.45	6.68	6.95	-1.50	-1.23	-0.27
210.	4.28	5.50	5.77	-1.49	-1.22	-0.27
220.	3.15	4.37	4.64	-1.49	-1.22	-0.27
230.	2.26	3.48	3.75	-1.49	-1.22	-0.27
240.	1.61	2.84	3.10	-1.50	-1.23	-0.26
250.	1.09	2.32	2.59	-1.50	-1.23	-0.27
260.	0.60	1.83	2.10	-1.49	-1.22	-0.27
270.	0.18	1.40	1.67	-1.49	-1.22	-0.27
280.	-0.25	0.97	1.24	-1.49	-1.22	-0.27
290.	-0.65	0.57	0.84	-1.49	-1.22	-0.27
300.	-1.06	0.16	0.43	-1.49	-1.22	-0.27
340.	-1.72	-0.50	-0.23	-1.49	-1.22	-0.27
375.	-1.91	-0.68	-0.42	-1.49	-1.22	-0.27
425.	-1.77	-0.55	-0.28	-1.49	-1.22	-0.27
475.	-1.60	-0.38	-0.11	-1.49	-1.22	-0.27

T A B L E I X L E V E L O F N O M O T I O N A N A L Y S I S

AUGUST 1974 - STATIONS 317-307

DEPTH (METERS)	VEL. 7,Z	VEL. 6,Z	VEL. 5,Z	VEL. 7,5	VEL. 7,6	VEL. 6,5
0.	-2.22	-1.33	-0.28	-1.94	-0.89	-1.05
10.	-2.30	-1.42	-0.36	-1.94	-0.88	-1.06
20.	-2.40	-1.51	-0.46	-1.94	-0.89	-1.05
30.	-2.78	-1.89	-0.84	-1.94	-0.88	-1.05
40.	-3.41	-2.53	-1.48	-1.93	-0.89	-1.05
50.	-3.76	-2.87	-1.82	-1.94	-0.89	-1.05
60.	-4.11	-3.22	-2.17	-1.94	-0.89	-1.05
70.	-4.34	-3.45	-2.40	-1.94	-0.88	-1.05
80.	-4.48	-3.60	-2.55	-1.94	-0.88	-1.06
90.	-4.56	-3.68	-2.62	-1.94	-0.88	-1.06
100.	-4.50	-3.62	-2.56	-1.94	-0.88	-1.05
110.	-4.39	-3.51	-2.46	-1.93	-0.88	-1.05
120.	-4.35	-3.47	-2.42	-1.93	-0.88	-1.05
130.	-4.32	-3.43	-2.38	-1.94	-0.88	-1.06
140.	-4.26	-3.38	-2.32	-1.94	-0.88	-1.06
150.	-4.23	-3.35	-2.30	-1.94	-0.88	-1.05
160.	-4.22	-3.34	-2.28	-1.93	-0.88	-1.06
170.	-4.22	-3.33	-2.28	-1.94	-0.89	-1.05
180.	-4.20	-3.33	-2.27	-1.93	-0.88	-1.05
190.	-4.17	-3.29	-2.24	-1.93	-0.88	-1.05
200.	-4.15	-3.26	-2.21	-1.94	-0.88	-1.05
210.	-4.12	-3.24	-2.19	-1.93	-0.88	-1.05
220.	-4.12	-3.23	-2.18	-1.93	-0.89	-1.05
230.	-4.11	-3.23	-2.18	-1.94	-0.88	-1.05
240.	-4.12	-3.24	-2.19	-1.93	-0.88	-1.05
250.	-4.12	-3.24	-2.19	-1.94	-0.88	-1.06
260.	-4.13	-3.25	-2.17	-1.94	-0.88	-1.06
270.	-4.11	-3.23	-2.17	-1.94	-0.88	-1.06
280.	-4.08	-3.23	-2.14	-1.94	-0.88	-1.05
290.	-4.04	-3.19	-2.11	-1.93	-0.88	-1.05
300.	-3.79	-3.16	-1.85	-1.94	-0.88	-1.06
340.	-3.47	-2.91	-1.54	-1.93	-0.88	-1.05
375.	-3.83	-2.59	-1.89	-1.94	-0.89	-1.05
425.	-2.83	-1.94	-0.28	-1.94	-0.89	-1.05
475.	-2.22	-1.33	-0.28	-1.94	-0.89	-1.05

TABLE X

LEVEL OF NO MOTION ANALYSIS

AUGUST 1974 - STATIONS 307-303

DEPTH (METERS)	VEL. 7,Z	VEL. 6,Z	VEL. 5,Z	VEL. 7,5	VEL. 7,6	VEL. 6,5
0.	-18.97	-15.56	-11.88	-7.09	-3.41	-3.68
10.	-19.03	-15.61	-11.93	-7.10	-3.42	-3.68
20.	-19.16	-15.75	-12.06	-7.10	-3.41	-3.69
30.	-19.22	-15.80	-12.12	-7.10	-3.42	-3.68
40.	-19.12	-15.70	-12.02	-7.10	-3.42	-3.68
50.	-19.15	-15.74	-12.06	-7.09	-3.41	-3.68
60.	-18.82	-15.41	-11.73	-7.09	-3.42	-3.68
70.	-18.41	-14.99	-11.31	-7.10	-3.42	-3.68
80.	-17.98	-14.56	-10.88	-7.10	-3.42	-3.68
90.	-17.84	-14.42	-10.74	-7.10	-3.42	-3.68
100.	-17.70	-14.29	-10.60	-7.10	-3.42	-3.69
110.	-17.49	-14.07	-10.39	-7.09	-3.41	-3.68
120.	-17.19	-13.78	-10.10	-7.09	-3.41	-3.68
130.	-16.86	-13.45	-9.77	-7.10	-3.42	-3.68
140.	-16.63	-13.21	-9.53	-7.10	-3.42	-3.68
150.	-16.47	-13.05	-9.37	-7.10	-3.42	-3.68
160.	-16.22	-12.80	-9.12	-7.10	-3.42	-3.68
170.	-16.00	-12.58	-8.90	-7.10	-3.42	-3.68
180.	-15.78	-12.36	-8.68	-7.10	-3.42	-3.68
190.	-15.51	-12.10	-8.42	-7.09	-3.41	-3.68
200.	-15.23	-11.81	-8.13	-7.10	-3.42	-3.69
210.	-14.72	-11.54	-7.85	-7.10	-3.42	-3.68
220.	-14.49	-11.30	-7.62	-7.10	-3.42	-3.68
230.	-14.27	-11.08	-7.40	-7.09	-3.41	-3.68
240.	-13.97	-10.86	-7.17	-7.10	-3.41	-3.69
250.	-13.65	-10.56	-6.87	-7.10	-3.42	-3.68
260.	-13.33	-10.23	-6.55	-7.10	-3.42	-3.68
270.	-12.99	-9.91	-6.23	-7.10	-3.42	-3.68
280.	-12.65	-9.57	-5.89	-7.10	-3.42	-3.68
290.	-12.32	-9.23	-5.55	-7.09	-3.41	-3.68
300.	-11.99	-8.81	-5.23	-7.10	-3.42	-3.68
340.	-11.03	-7.91	-4.13	-7.10	-3.42	-3.69
375.	-10.32	-6.91	-3.22	-7.10	-3.42	-3.68
425.	-9.17	-5.75	-2.07	-7.10	-3.42	-3.68
475.	-7.84	-4.43	-0.75	-7.09	-3.41	-3.68

Z = depth (m)

VEL.Z = absolute velocity at Z (cm/sec).¹

VEL.7 = absolute velocity at Z = 700 m (cm/sec)

VEL.5 = absolute velocity at Z = 500 m (cm/sec)

VEL.7,Z = velocity at Z relative to 700 m (cm/sec)

VEL.5,Z = velocity at Z relative to 500 m (cm/sec)

VEL.7,5 = velocity at 500 m relative to velocity at
700 m or the velocity shear between Z = 500 m
and Z = 700 m

VEL.6,5 = velocity at 500 m relative to velocity at
600 m or the velocity shear between Z = 500 m
and Z = 600 m

The preceding variables are related to each other in that the absolute velocity at any depth, Z, is equal to the absolute velocity at Z = 700 m plus the velocity at Z relative to 700 m, or symbolically,

$$\text{VEL.Z} = \text{VEL.7} + \text{VEL.7,Z} \quad (4)$$

similarly,

$$\text{VEL.Z} = \text{VEL.6} + \text{VEL.6,Z} \quad (5)$$

$$\text{VEL.Z} = \text{VEL.5} + \text{VEL.5,Z} \quad (6)$$

subtracting equation (6) from (4),

$$0 = \text{VEL.7} - \text{VEL.5} + \text{VEL.7,Z} - \text{VEL.5,Z}$$

or,

$$\text{VEL.5} - \text{VEL.7} = \text{VEL.7,Z} - \text{VEL.5,Z} \quad (7)$$

¹ In fact, velocities are defined on isobaric surfaces where the pressure in db is roughly the same numerically as the given depth in meters. Negative velocities indicate flow to the north in Tables II through X.

but the left-hand side of equation (7) is the velocity shear between $Z = 500$ m and $Z = 700$ m or,

$$VEL.7,5 = VEL.7,Z - VEL.5,Z$$

The velocities at Z relative to 700 db, 600 db and 500 db are known from dynamic method computations. Thus the velocity shears which provide quantitative differences between the two levels are known. Now, assuming that the 500 db level is the reference level which provides velocities which nearly approximate the actual flow, then comparison of the velocity shears, $VEL.7,5$ and $VEL.6,5$, to the velocity at Z relative to 500 m, $VEL.5,Z$, respectively, provides a velocity error percentage. For example, Table II shows that if one chose 700 db as a reference level instead of 500 db, the assumed correct level, the calculated surface currents would differ by 37 percent. As expected, the difference percentage tends to increase with greater depths.

In summary, Tables II through X show quantitatively that there are considerable differences in current speeds obtained from geostrophy using 500 db, 600 db, and 700 db as the reference levels. Consequently, if the objective of a study is to obtain current speeds which are correct in magnitude, the selection of a 'level of no motion' should not be a matter of choice but of direct measurement, and of data corroboration via independent measurements. The apparent influence of bottom topography on the flow (see subsection B in Discussion and Results) also suggests that motion persists rather deeper than 500 db and that there may be no simple 'level of no motion'.

B. PATTERNS OF CURRENT FLOW AND THEIR STRUCTURE WITH DEPTH

The patterns of current flow are inferred from geostrophy with respect to the 500 db surface. To obtain a pictorial representation of the current flow and its structure with depth, dynamic heights for data stations along three constant latitude lines, $36^{\circ} 20'N$, $36^{\circ} 30'N$ and $36^{\circ} 40'N$, were plotted and height contours drawn for the isobaric surface, 50 db, 100 db, 200 db, 300 db, 375 db and the 425 db surfaces during August 1973. These dynamic height contours of the various surfaces above are shown in figures 3 through 9. The contour lines are labeled with their respective dynamic height values in dynamic centimeters. The contour intervals for each of figures 3 through 9 are different. Consequently, caution should be exercised when interpreting the figures for speed. For example, the closely spaced contours in figures 8 and 9 do not indicate an intense circulation.

Unfortunately, this analysis could not be accomplished for data months other than August 1973 since data observations were made predominantly along one constant latitude line, $36^{\circ} 40'N$, during months September 1973 through August 1974. However, the contours clearly reveal some interesting features of the patterns of the current flow and their structure with depth during August 1973.

The prominent features depicted in figures 3 through 9 are,

- (1) The flow branches into a northwesterly and an east-southeasterly component just north of $36^{\circ} 30'N$ at all seven depths from the surface to 425 meters.
- (2) The general pattern of current flow is similar for all depths from the surface to 375 meters.

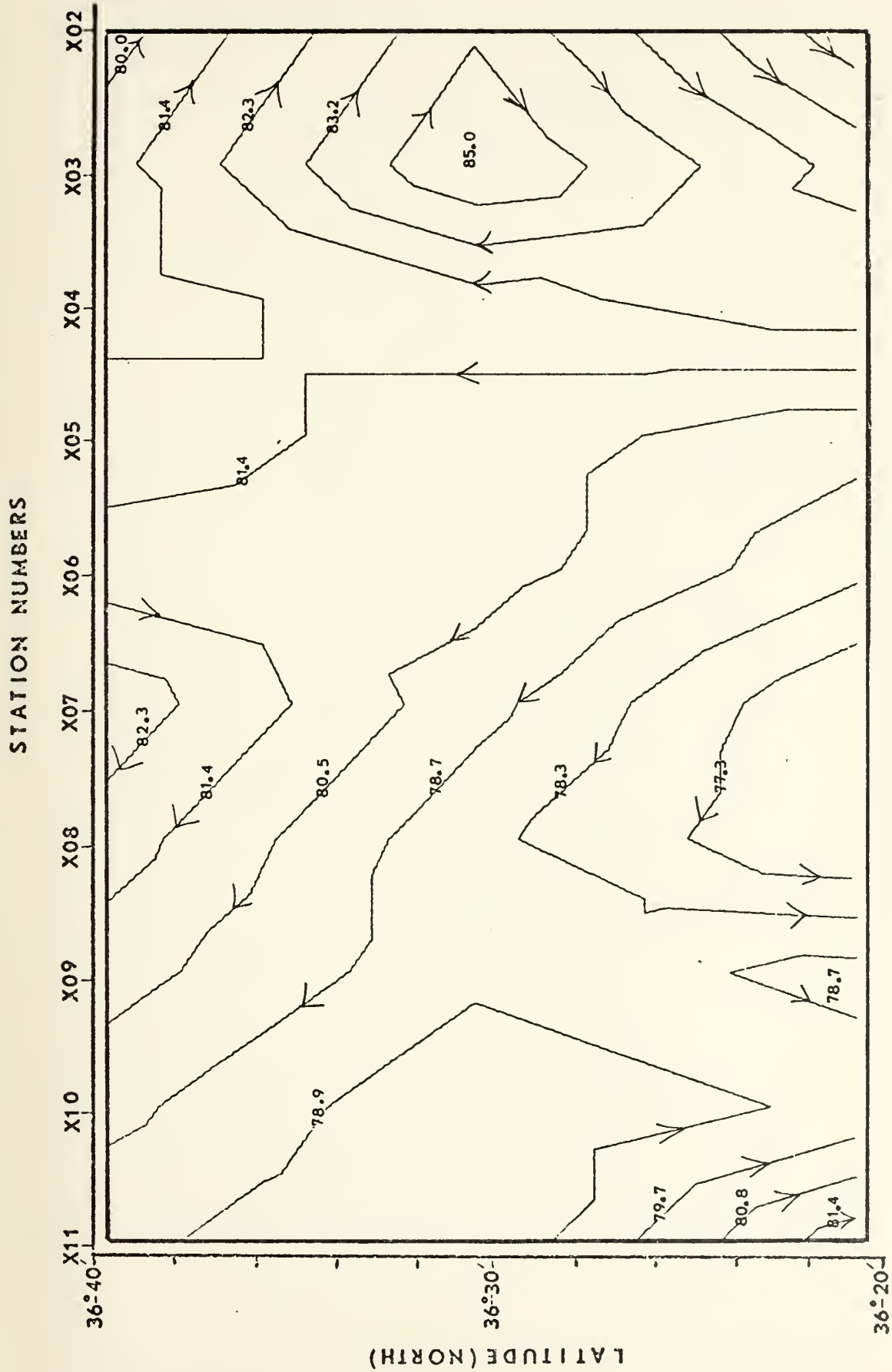


Fig. 3. Dynamic Height Contours at the Surface during August 1973.
(Dynamic heights are in dynamic centimeters, relative to 500 db.)

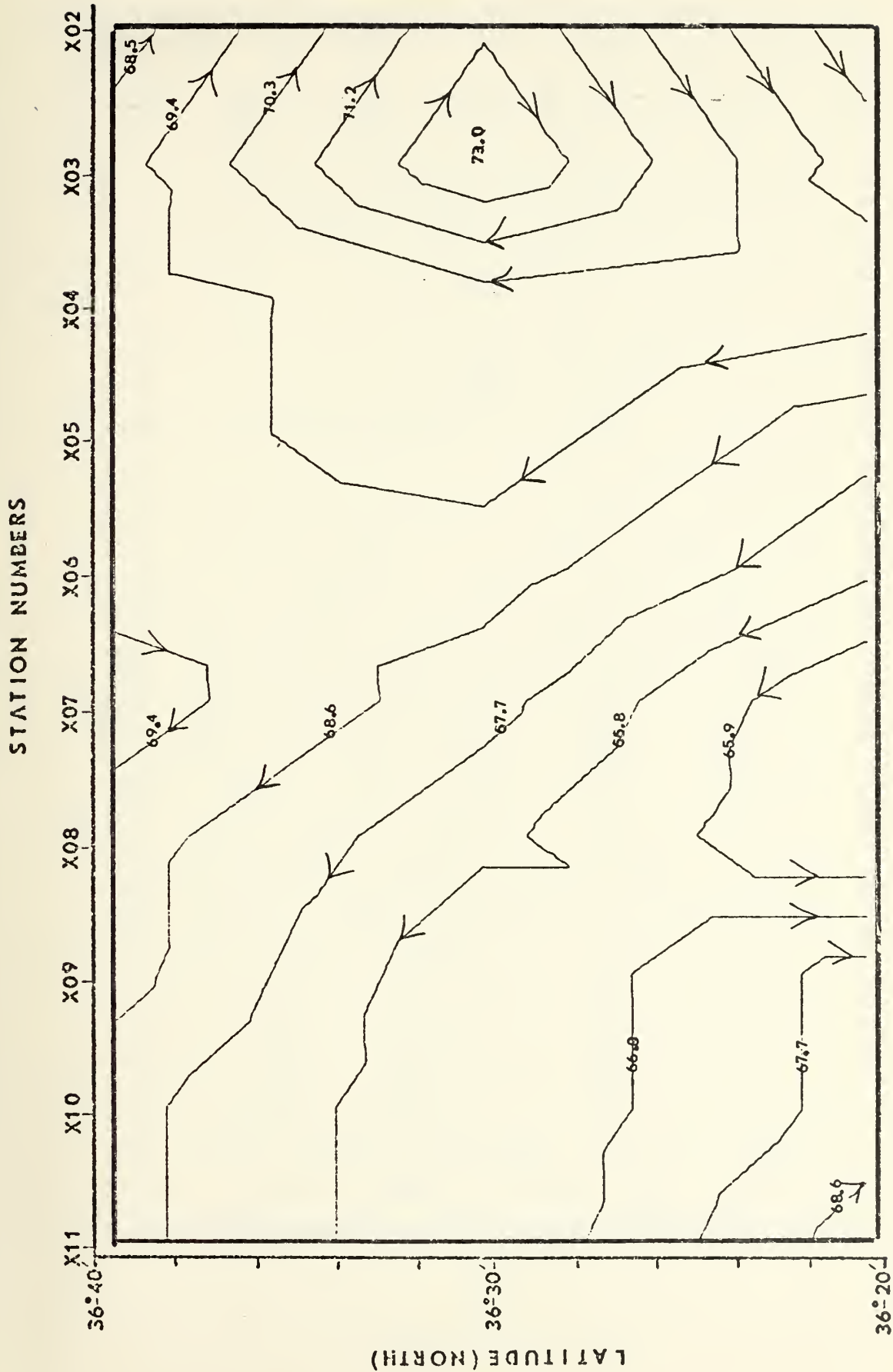


Fig. 4. Dynamic Height Contours of the 50 db Surface during August 1973.
(Dynamic heights are in dynamic centimeters, relative to 500 db.)

STATION NUMBERS

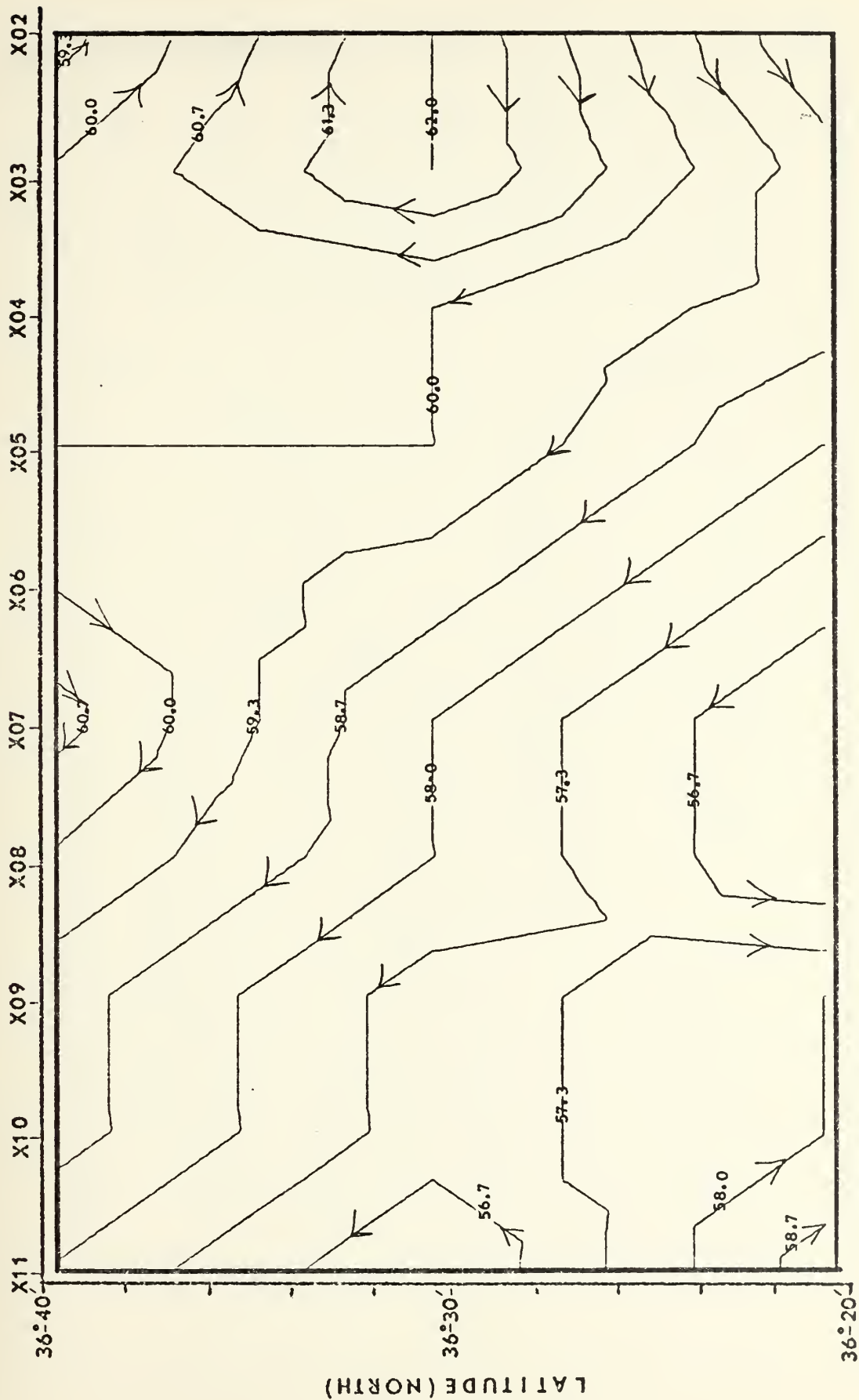


Fig. 5. Dynamic Height Contours of the 100 db Surface during August 1973.
(Dynamic heights are in dynamic centimeters, relative to 500 db.)

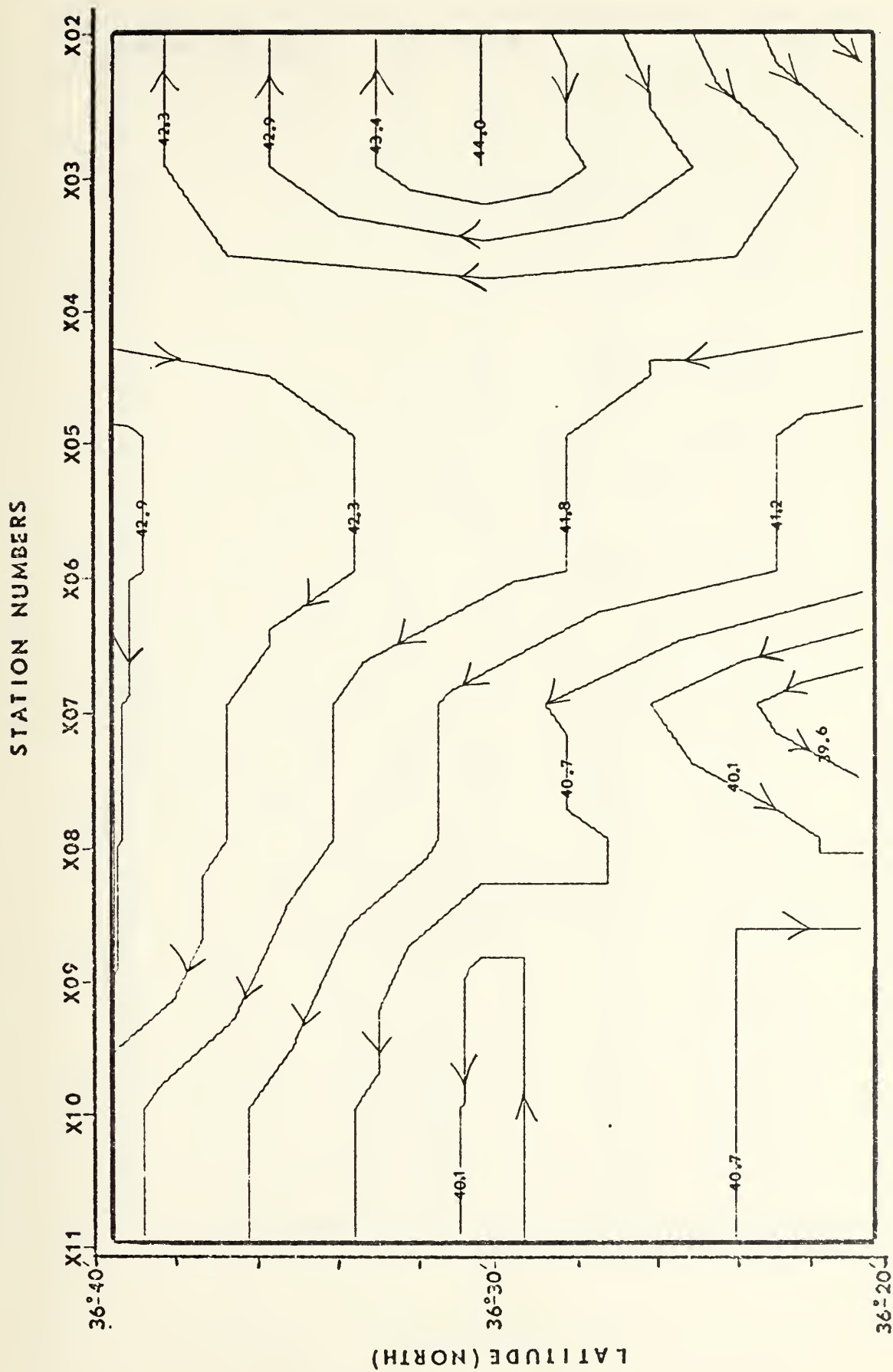


Fig. 6. Dynamic Height Contours of the 200 db Surface during August 1973.
(Dynamic heights are in dynamic centimeters, relative to 500 db.)

STATION NUMBERS

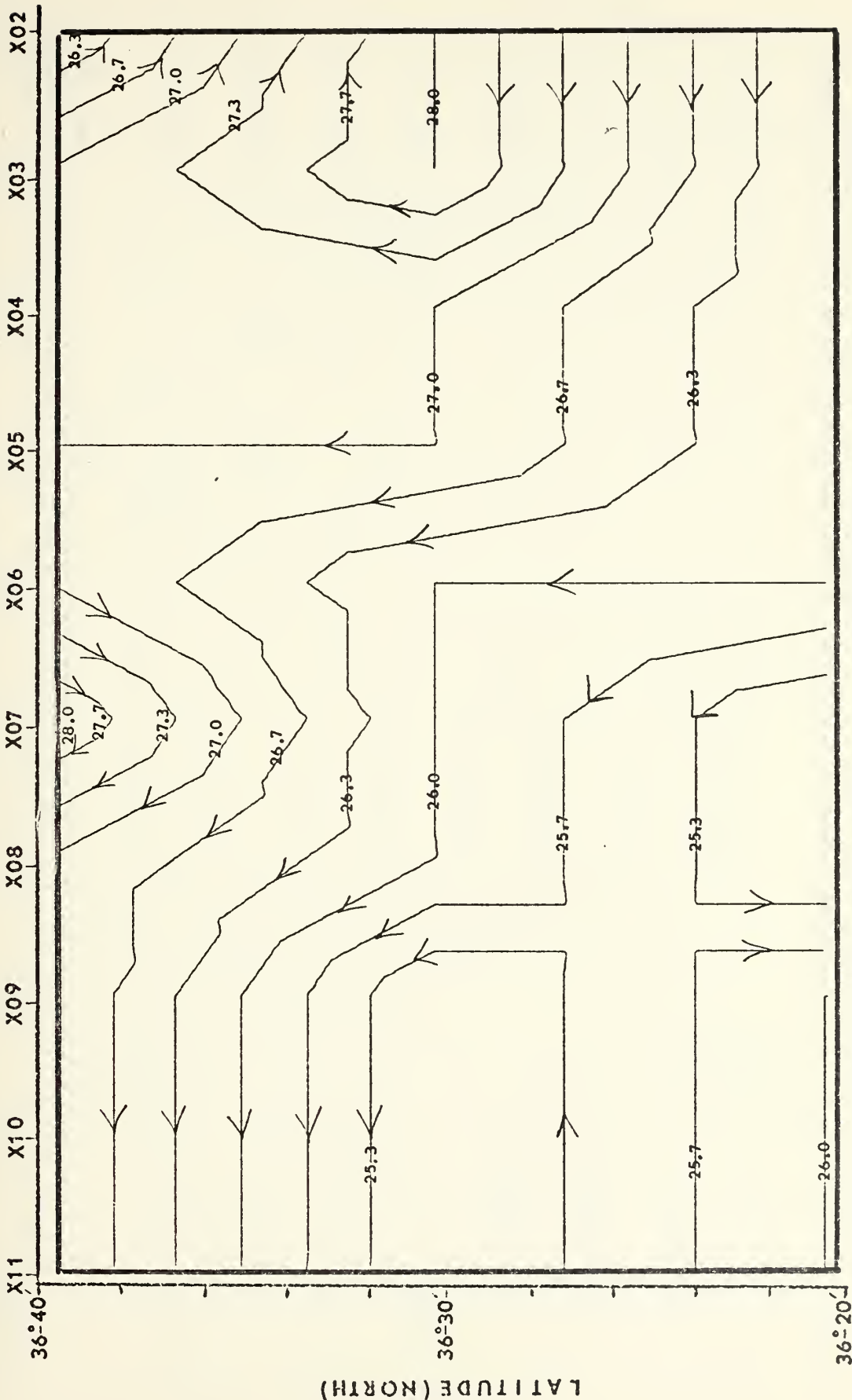


Fig. 7. Dynamic Height Contours of the 300 db Surface during August 1973.
(Dynamic heights are in dynamic centimeters, relative to 500 db.)

STATION NUMBERS

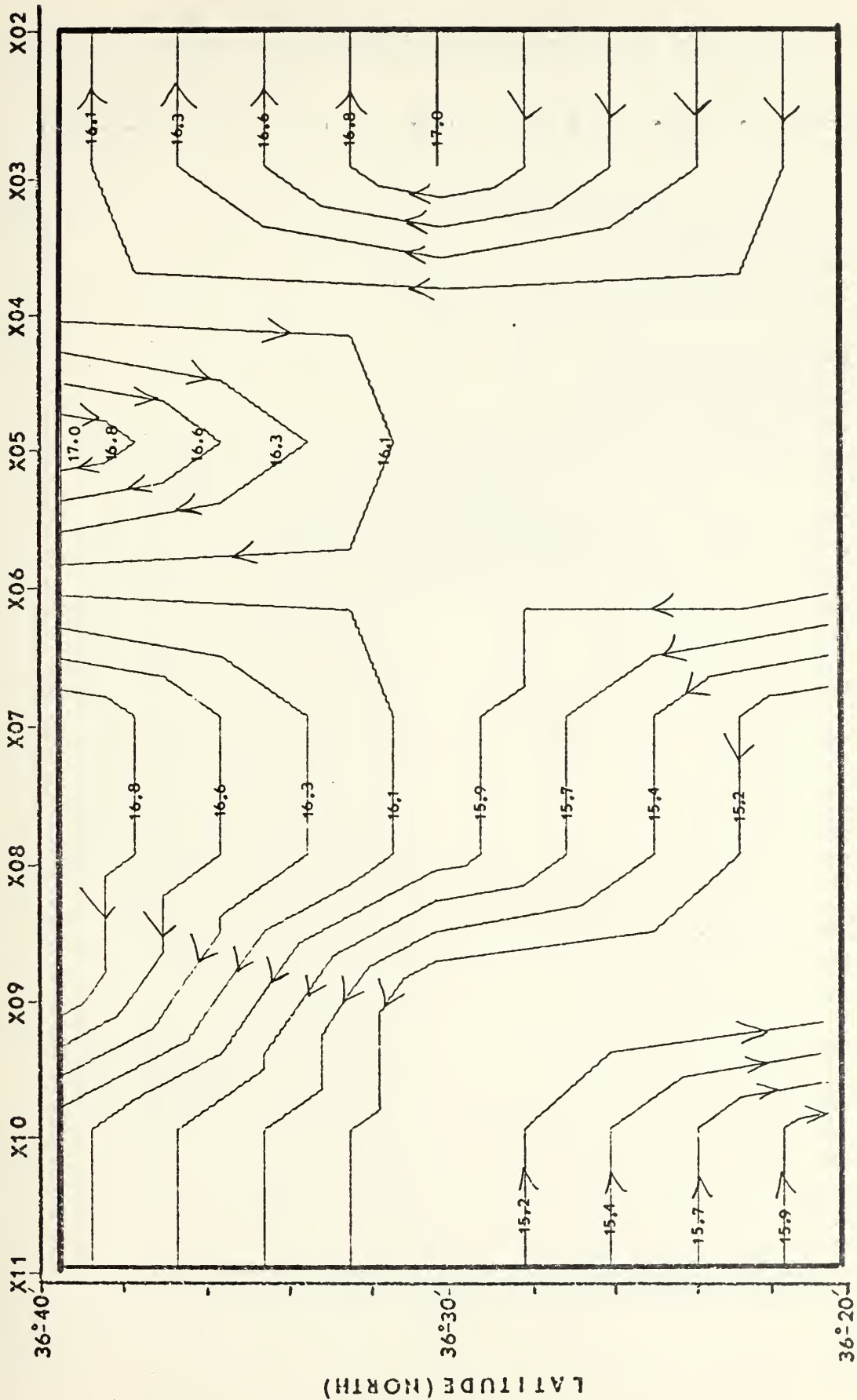


Fig. 8. Dynamic Height Contours of the 375 db Surface during August 1973.
(Dynamic heights are in dynamic centimeters, relative to 500 db.)

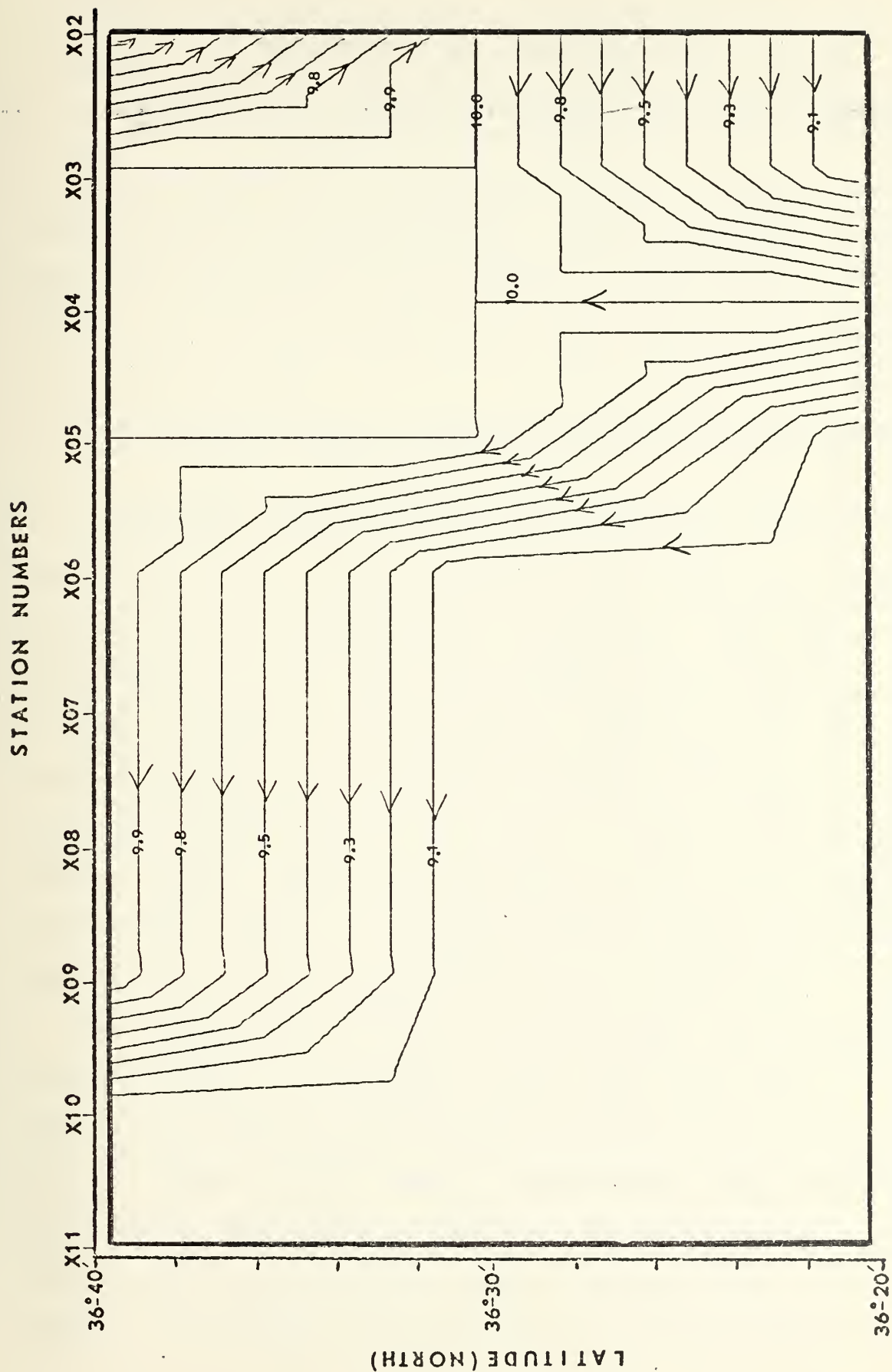


Fig. 9. Dynamic Height Contours of the 425 db Surface during August 1973.
(Dynamic heights are in dynamic centimeters, relative to 500 db.)

- (3) The flow is more intense south of latitude $36^{\circ} 30'N$ as evidenced by the dynamic height contour spacing.
- (4) The narrow band of poleward flow in the vicinity of longitude $122^{\circ} 18'W$, near stations 106 and 206, appears to be topographically controlled.

Figure 10 depicts the general pattern of current flow relative to the local bathymetry. Figures 3 through 10 suggest that the course of the currents in this area is controlled in part by the local bottom topography. This is evidenced in the following ways,

- (1) The flow follows the general north-south topographical orientation south of $36^{\circ} 30'N$.
- (2) The flow branches north of $36^{\circ} 30'N$, and follows the generally east-west bathymetric contours.

Furthermore, the currents in the northwest sector of the area appear not to be topographically controlled. This can be explained by the fact that the current speed for the most part is small near 500 m, and it would be difficult to see how bottom topography at depths greater than 1,000 fathoms could influence the currents in this sector. However, in the northeastern sector, where depth decreases toward the coastline, the currents appear to be topographically controlled and follow the principle of conservation of potential vorticity.

Now consider the validity of the current flow inferred from geostrophy. Independent current flow measurements were made using parachute drogues during August 1972 and August 1973 by Wickham [1975]. Drogue trajectories, especially in 1972, confirm that the flow branches into two components, and there appears to be a narrow band of poleward flow in the vicinity of longitude $122^{\circ} 18'W$; and the drogue paths in

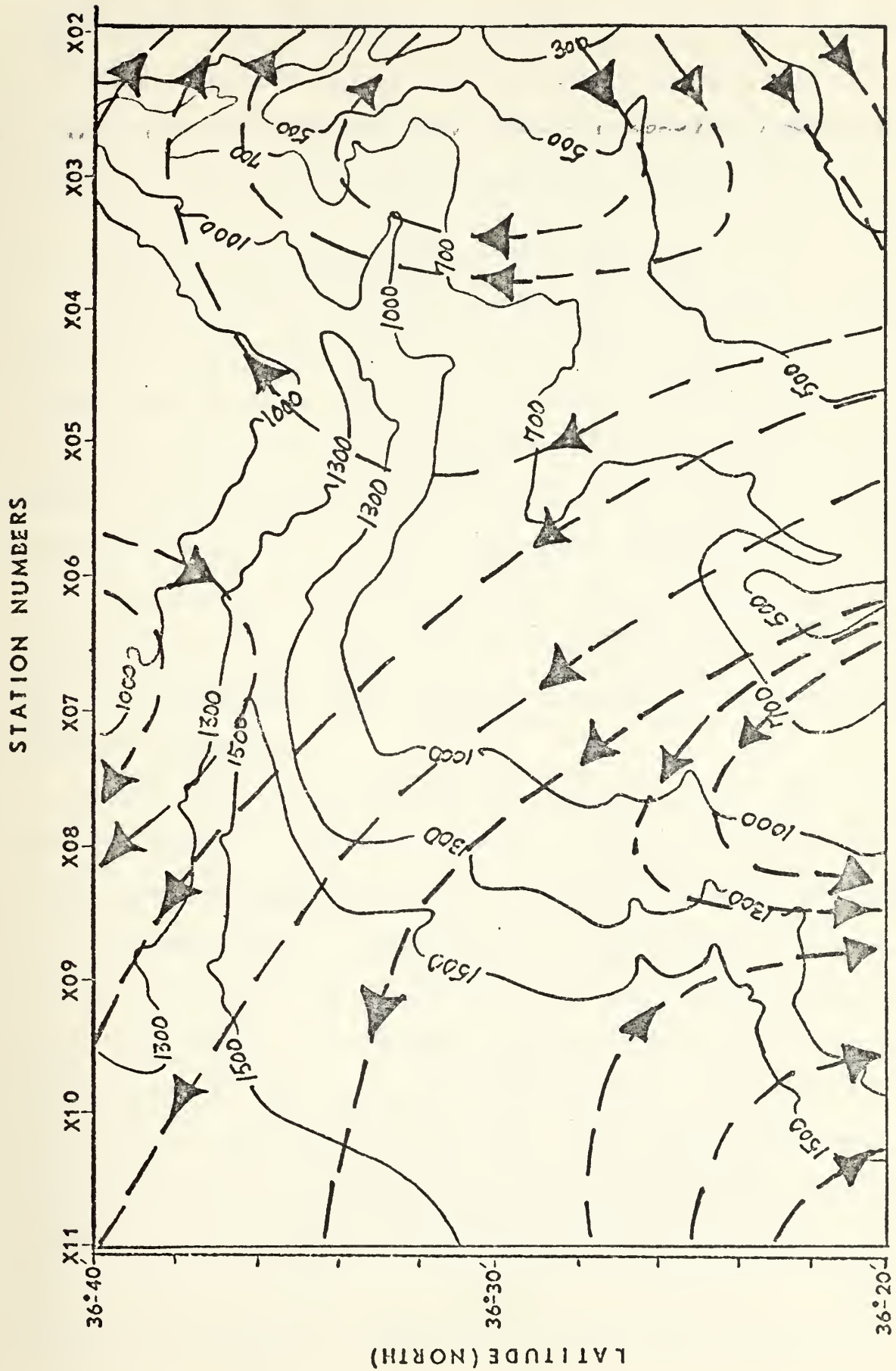


Fig. 10. General Pattern of Geostrophic Current Flow during August 1973.

August 1973 tend to confirm a broader poleward flow towards the west. There is also indication in the drogue paths in August 1972 of a strong shear zone and a cyclonic eddy of a similar scale to that shown by geostrophy in 1973.

C. TEMPORAL VARIATION OF THE GEOSTROPHIC FLOW

The variation of the geostrophic flow with time is inferred from geostrophic calculations with respect to the 500 db surface. Specifically, dynamic heights were calculated for stations along constant latitude line, $36^{\circ} 40'N$, during each month. These dynamic heights were used to generate a two-dimensional array with the abscissa and ordinate axes specified as station numbers and time, respectively. Dynamic height contours were then constructed for several isobaric surfaces and the geostrophic flow normal to the station line inferred from the contours.

Originally, the dynamic height contours with time were to depict temporal variations over the entire observation period, August 1973 through August 1974. However, the time period had to be divided into two segments due to programming constraints of the program routine, CONTUR. Specifically, the program will contour only the dynamic height values of data months which have an equal number of data stations. Consequently, data months February, June and July 1974, which have dynamic height calculations based on only three Nansen data stations, (vice 16 STD stations for the other months) prohibited depicting variation of flow over the entire time period. Therefore figures 11 through 16, which were constructed from dynamic

STATION NUMBERS

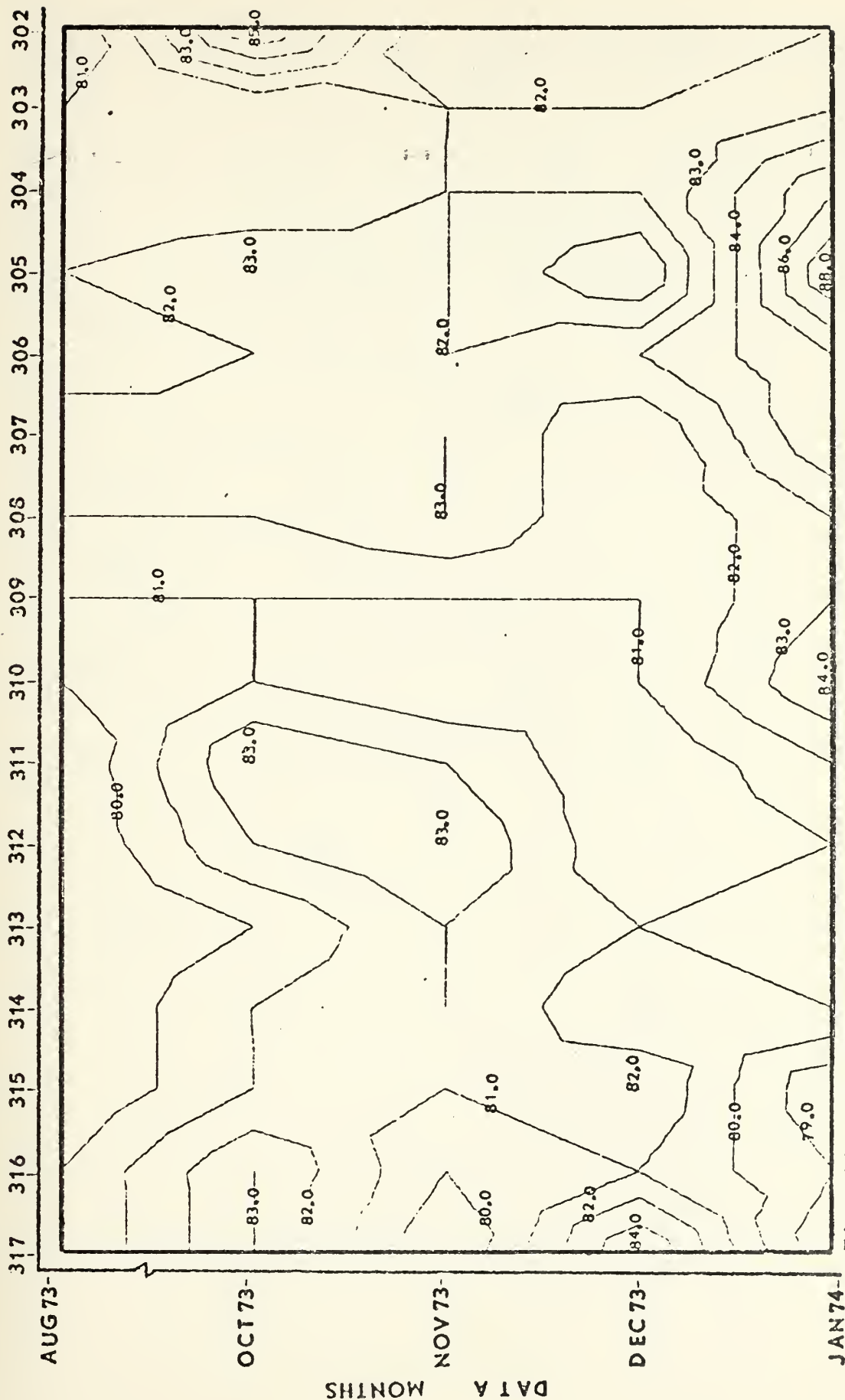


Fig. 11. Temporal Variation of Dynamic Height Contours at the Surface for August 1973 through January 1974. (Dynamic heights are in dynamic centimeters, relative to 500 db.)

STATION NUMBERS

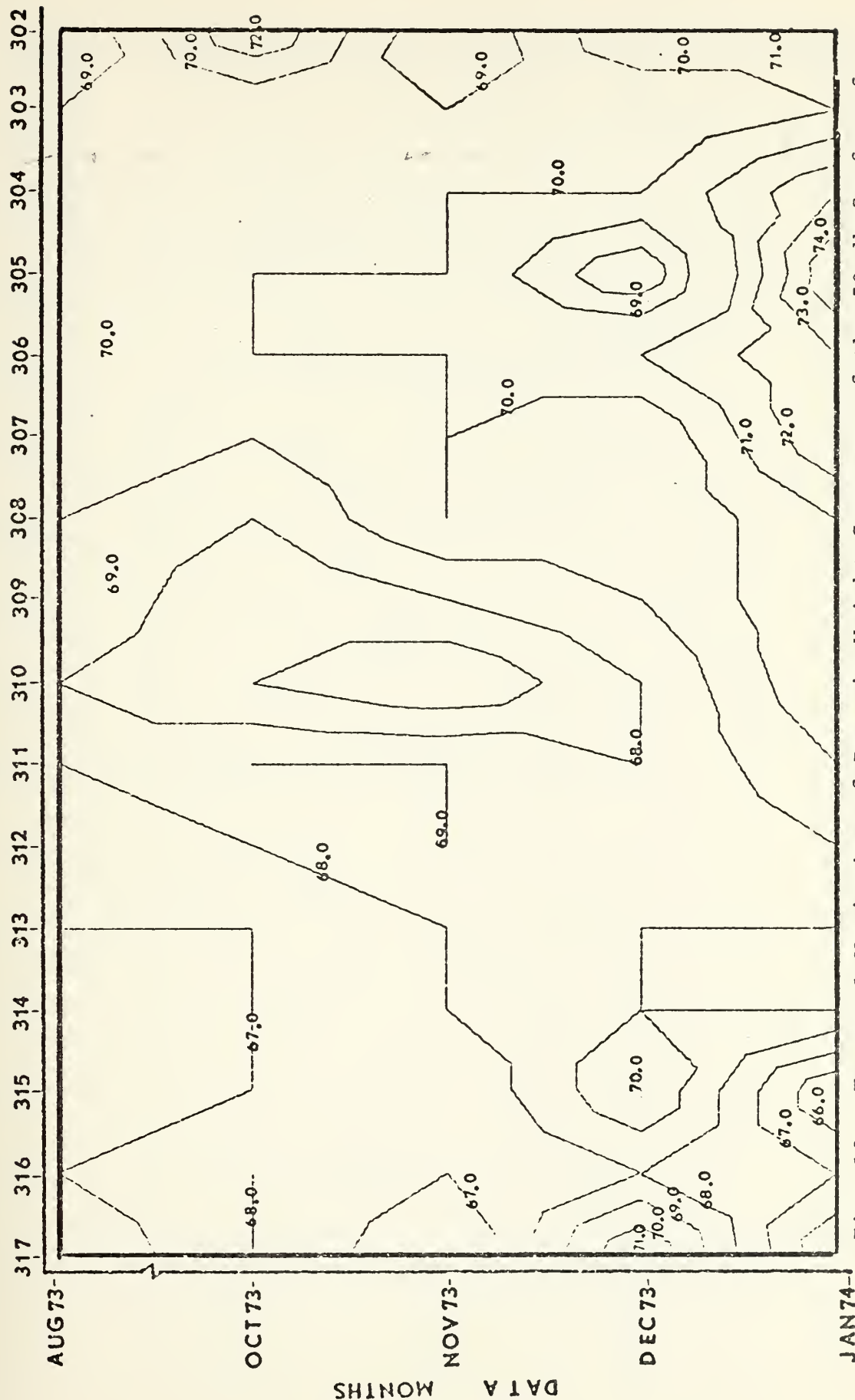


Fig. 12. Temporal Variation of Dynamic Height Contours of the 50 db Surface for August 1973 through January 1974. (Dynamic heights are in dynamic centimeters, relative to 500 db.)

STATION NUMBERS

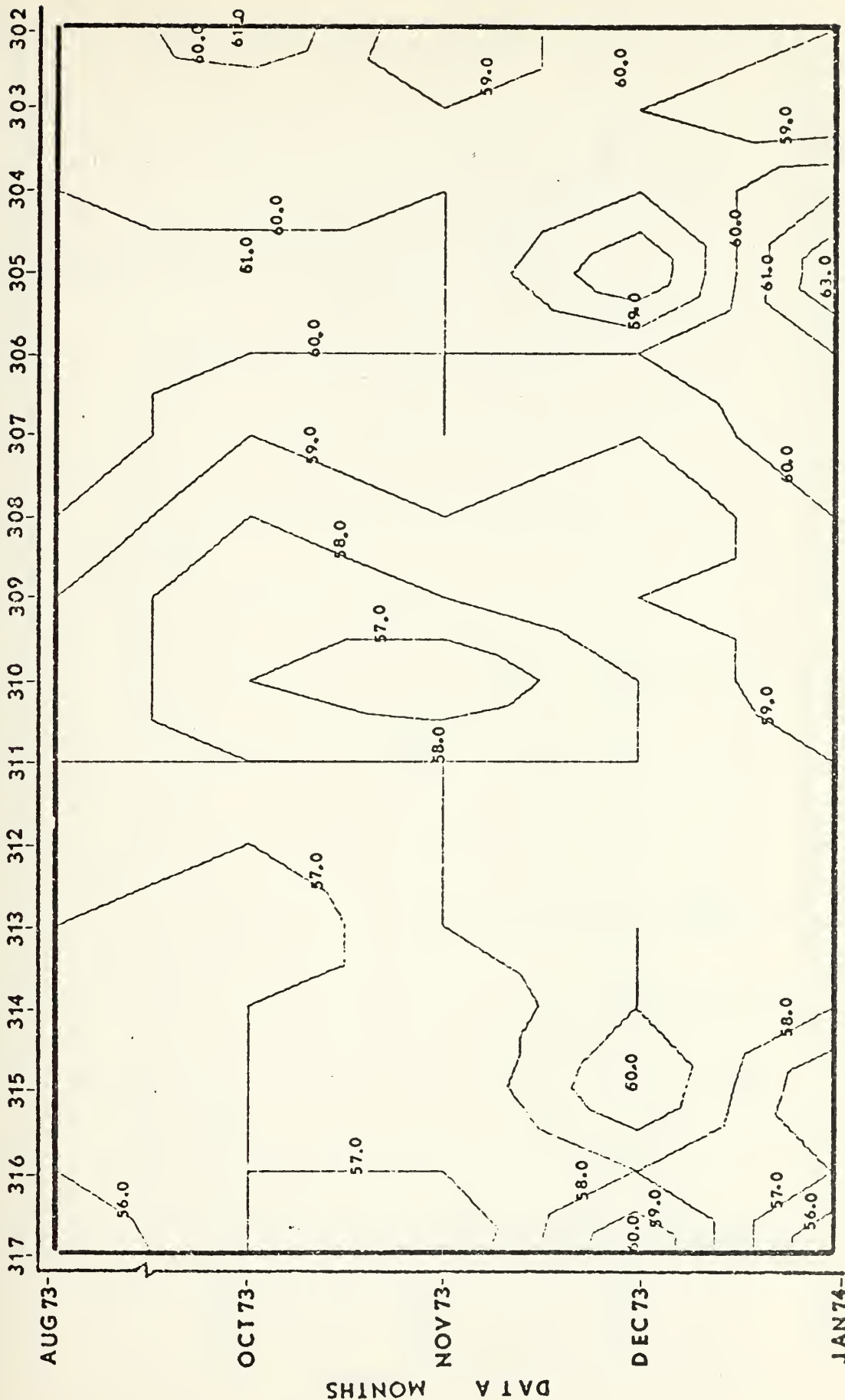


Fig. 13. Temporal Variation of Dynamic Height Contours of the 100 db Surface for August 1973 through January 1974. (Dynamic heights are in dynamic centimeters, relative to 500 db.)

STATION NUMBERS

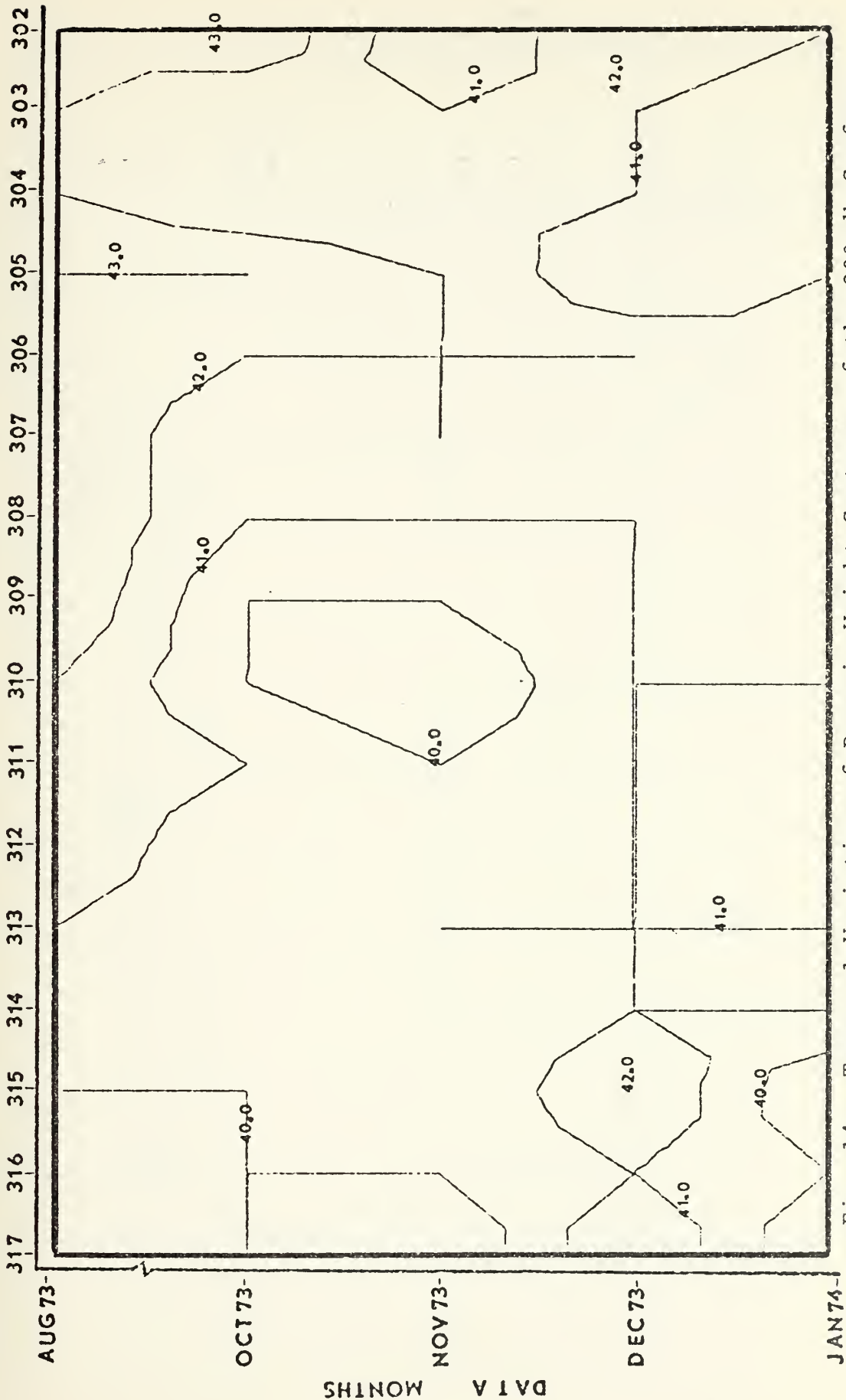


Fig. 14. Temporal Variation of Dynamic Height Contours of the 200 db Surface for August 1973 through January 1974. (Dynamic heights are in dynamic centimeters, relative to 500 db.)

STATION NUMBERS

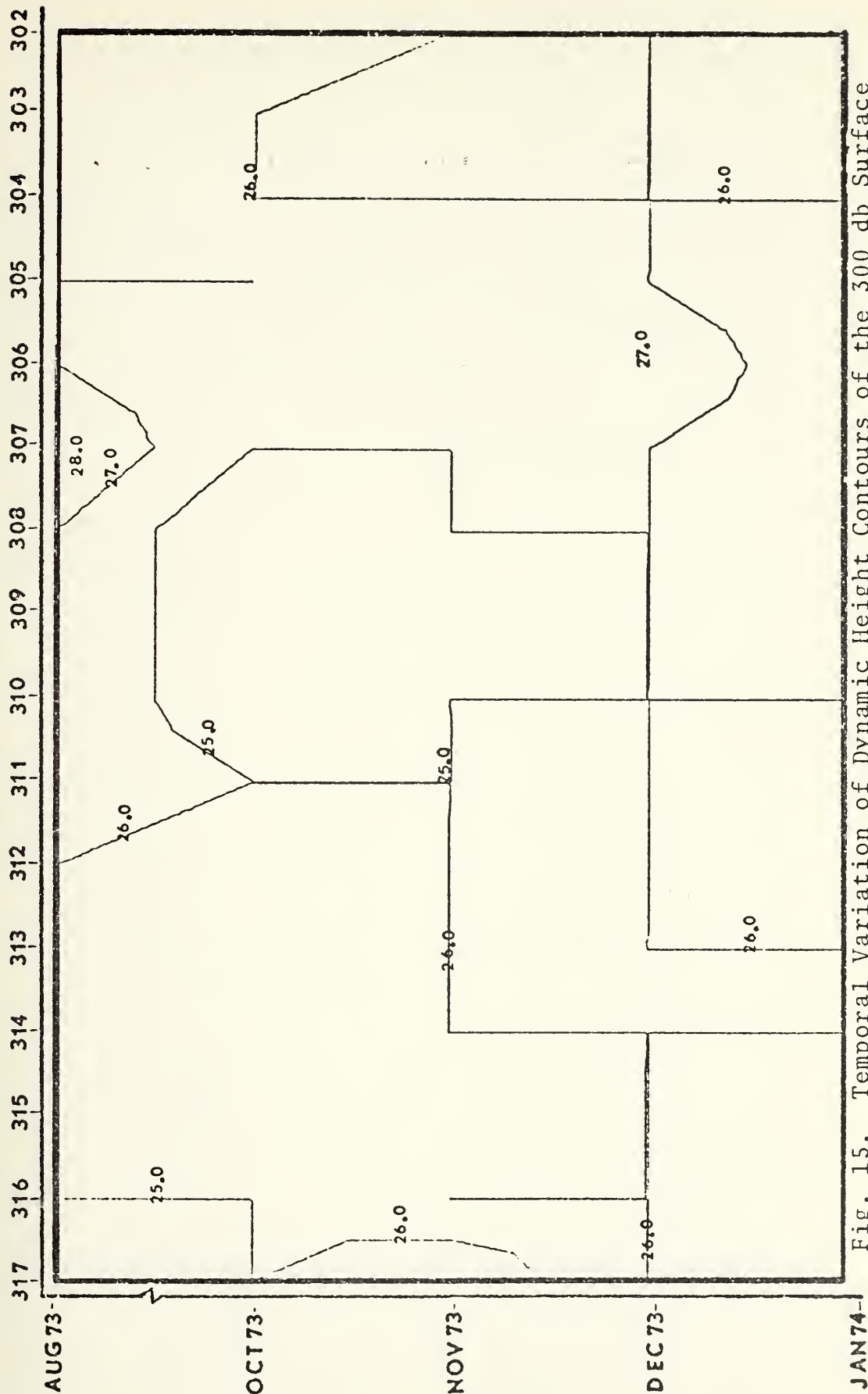


Fig. 15. Temporal Variation of Dynamic Height Contours of the 300 db Surface for August 1973 through January 1974. (Dynamic heights are in dynamic centimeters, relative to 500 db.)

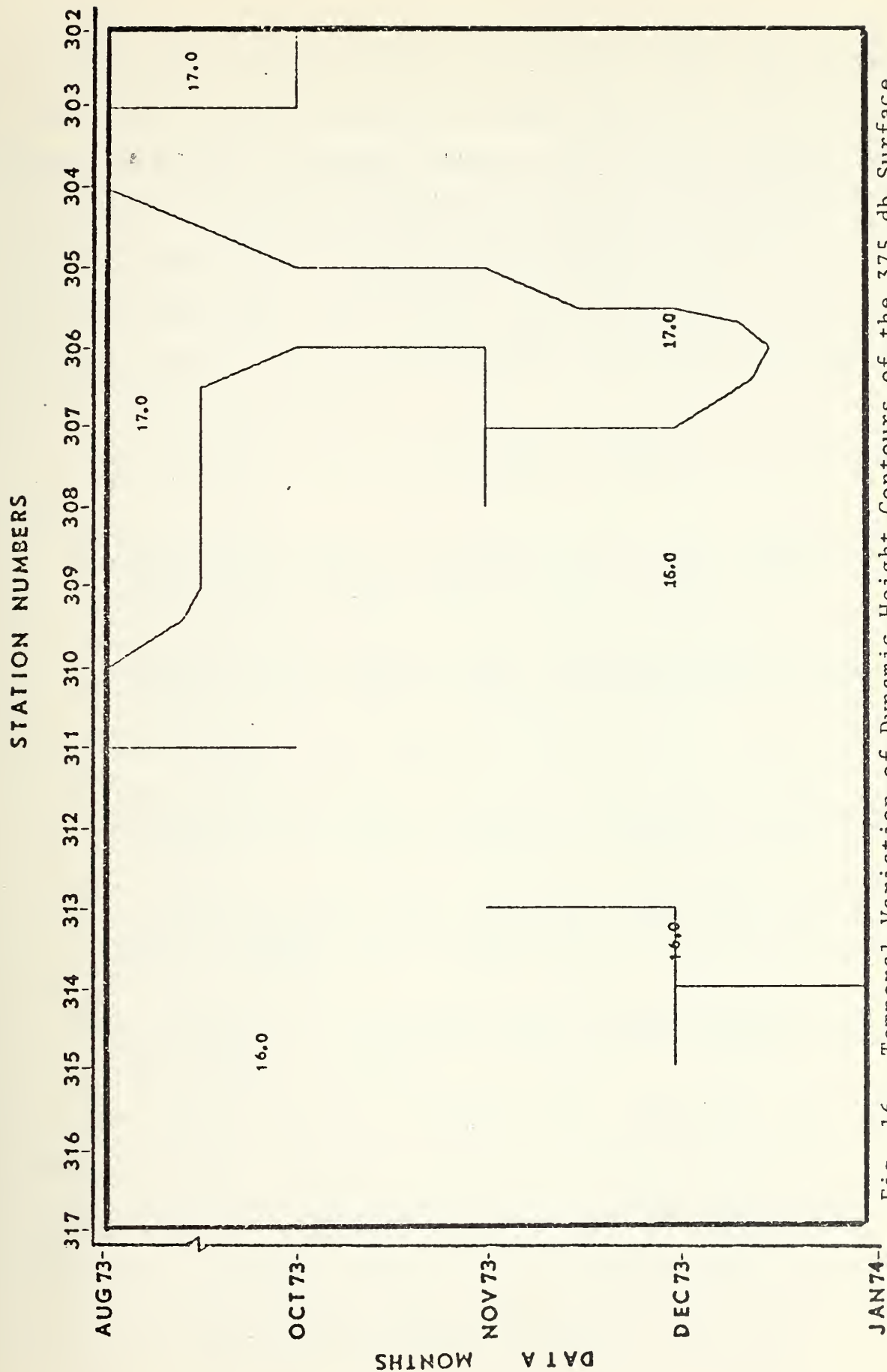


Fig. 16. Temporal Variation of Dynamic Height Contours of the 375 db Surface for August 1973 through January 1974. (Dynamic heights are in dynamic centimeters, relative to 500 db.)

height values based on 16 STD stations per data cruise month, depict the temporal variation of geostrophic flow at several depths for only the period, August 1973 through January 1974. Figures 17 through 21, which were constructed from dynamic height values based on either STD or Nansen data at three data stations per data cruise month, depict the temporal variation of geostrophic flow at several depths over the period January 1974 through August 1974.

The prominent features depicted in figures 11 through 16 are,

- (1) The general surface flow pattern over the time period, August 1973 through January 1974, is very similar to those found at 50 m, 100 m, 200 m and 300 m.
- (2) The geostrophic flow is more intense during the period November 1973 through January 1974 than during August through October 1973 in the upper 200 meters of depth.
- (3) The poleward flow appears to shift to the west with time.
- (4) The equatorward flow, east of station number 309, during December 1973 through January 1974 appears to be more intense in the upper 200 meters than the poleward flow.
- (5) A reversal in the flow direction is depicted in the vicinity of station 305 such that the predominant flow east of station 305 is equatorward, and poleward west of the station.
- (6) A narrow band of poleward flow located between stations 306 and 309 is apparent throughout the period, and from the surface to 375 m.

Now consider figures 17 through 21. Obviously, the small scale structure revealed in figures 11 through 16 cannot be seen in figures 17 through 21 due to the data observation grid size. However, there are a few features that are apparent.

- (1) The flow is more intense during January, June and August 1974 than during February, March and July 1974.

STATION NUMBERS

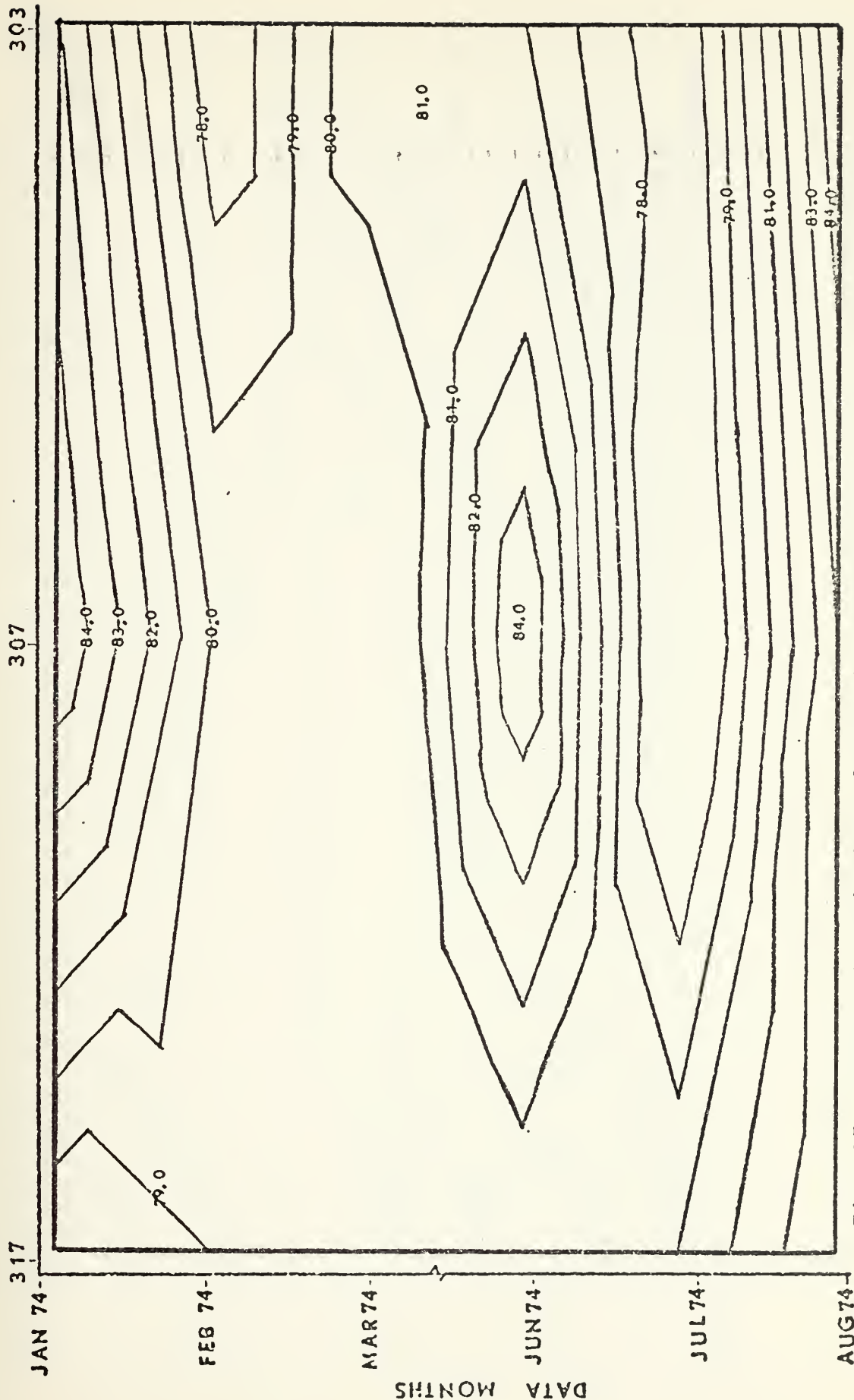


Fig. 17. Temporal Variation of Dynamic Height Contours at the Surface for January 1974 through August 1974. (Dynamic heights are in dynamic centimeters, relative to 500 db.)

STATION NUMBERS

303

307

317

JAN 74-

FEB 74-

MAR 74-

JUN 74-

JUL 74-

AUG 74-

DATA MONTHS

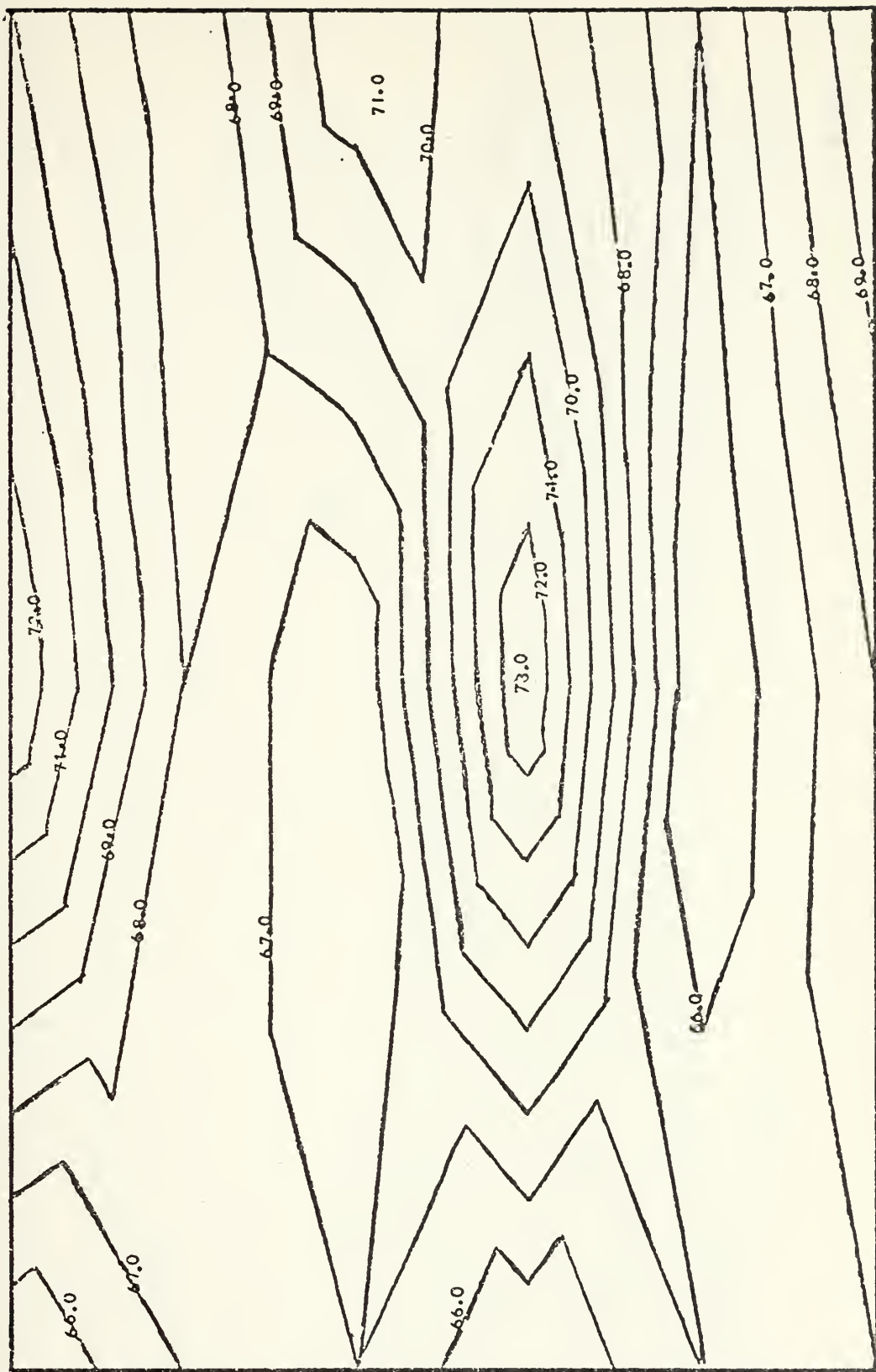


Fig. 18. Temporal Variation of Dynamic Height Contours of the 50 db Surface for January 1974 through August 1974. (Dynamic heights are in dynamic centimeters, relative to 500 db.)

STATION NUMBERS

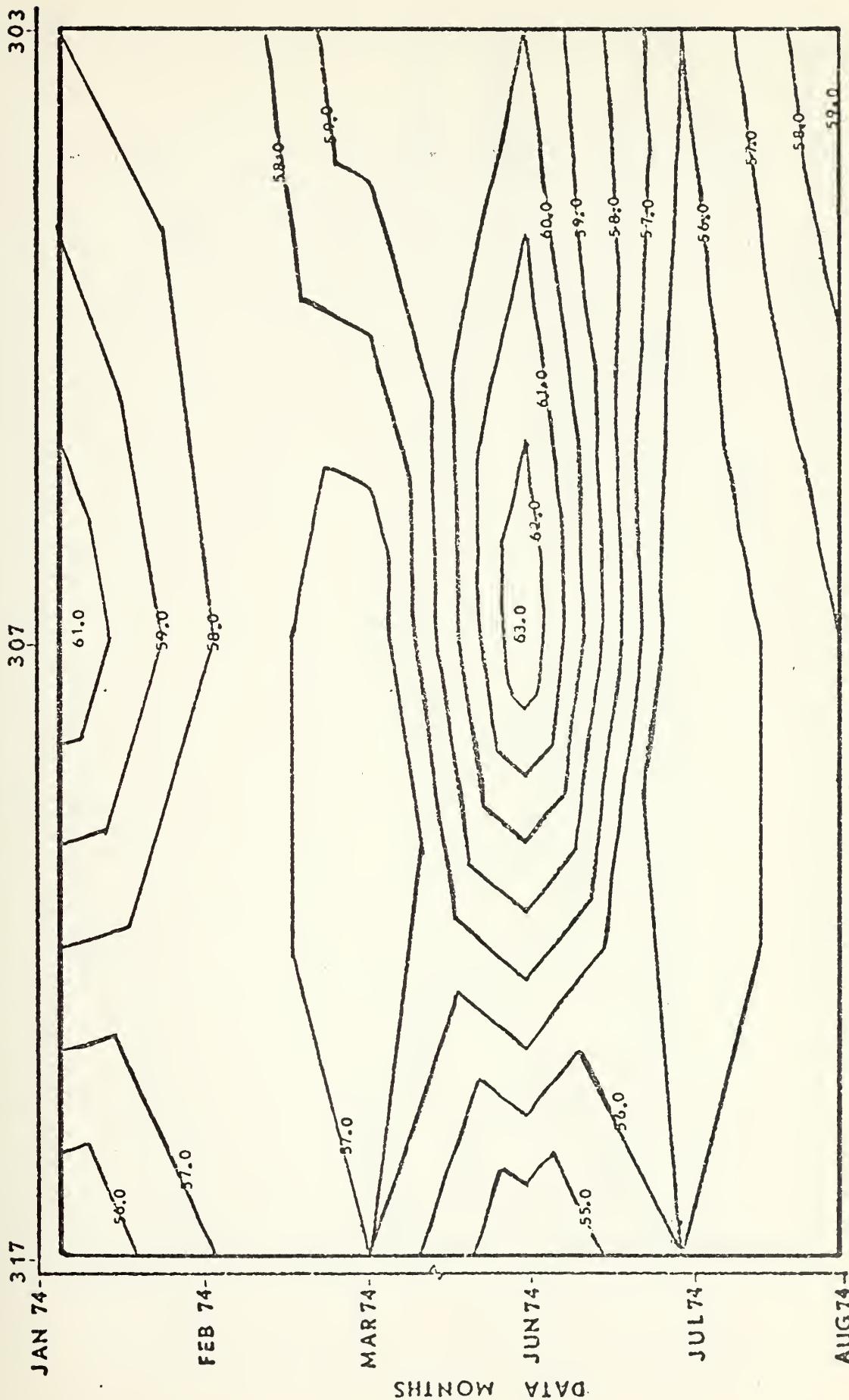


Fig. 19. Temporal Variation of Dynamic Height Contours of the 100 db Surface for January 1974 through August 1974. (Dynamic heights are in dynamic centimeters, relative to 500 db.)

STATION NUMBERS

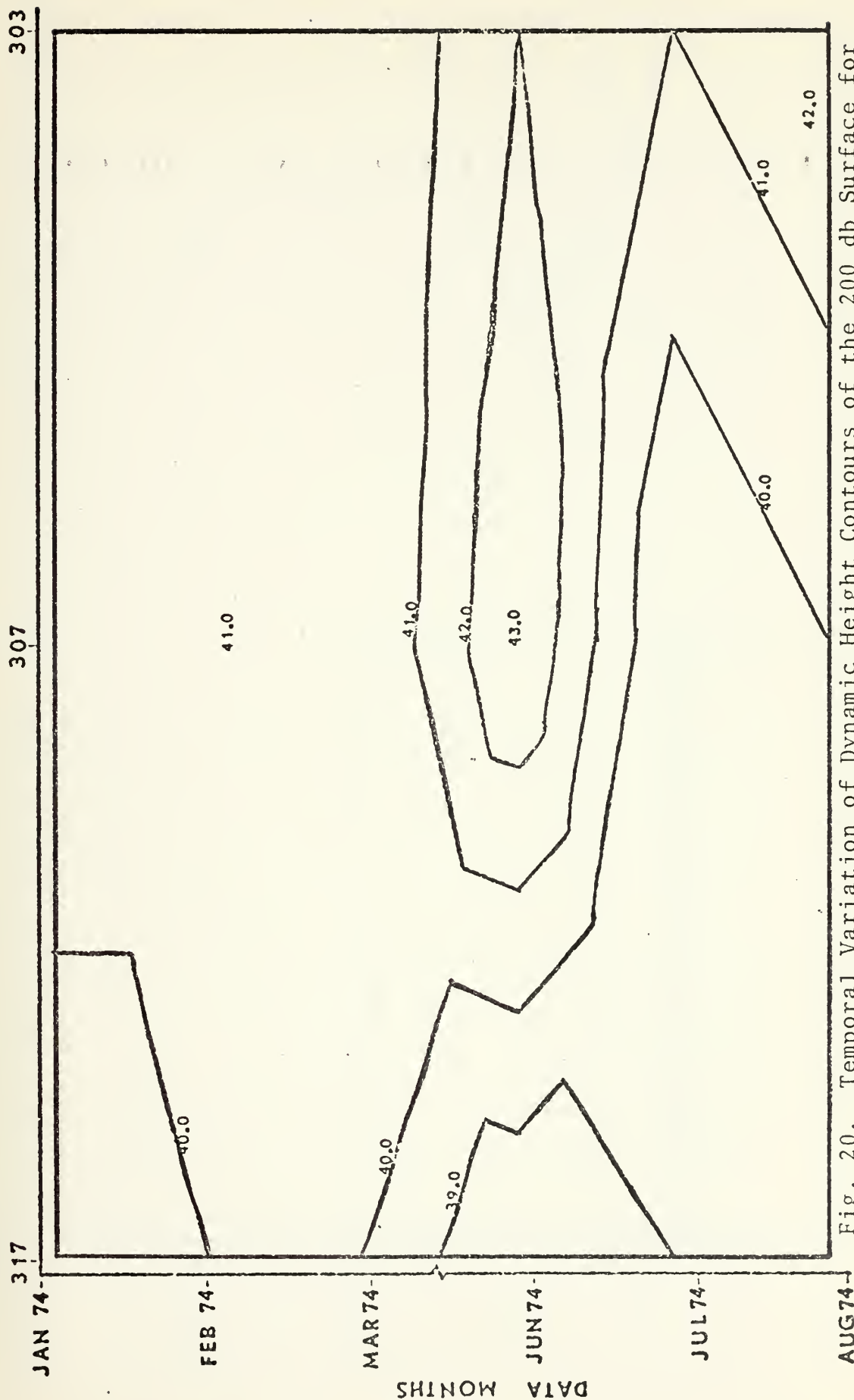


Fig. 20. Temporal Variation of Dynamic Height Contours of the 200 db Surface for January 1974 through August 1974. (Dynamic heights are in dynamic centimeters, relative to 500 db.)

STATION NUMBERS

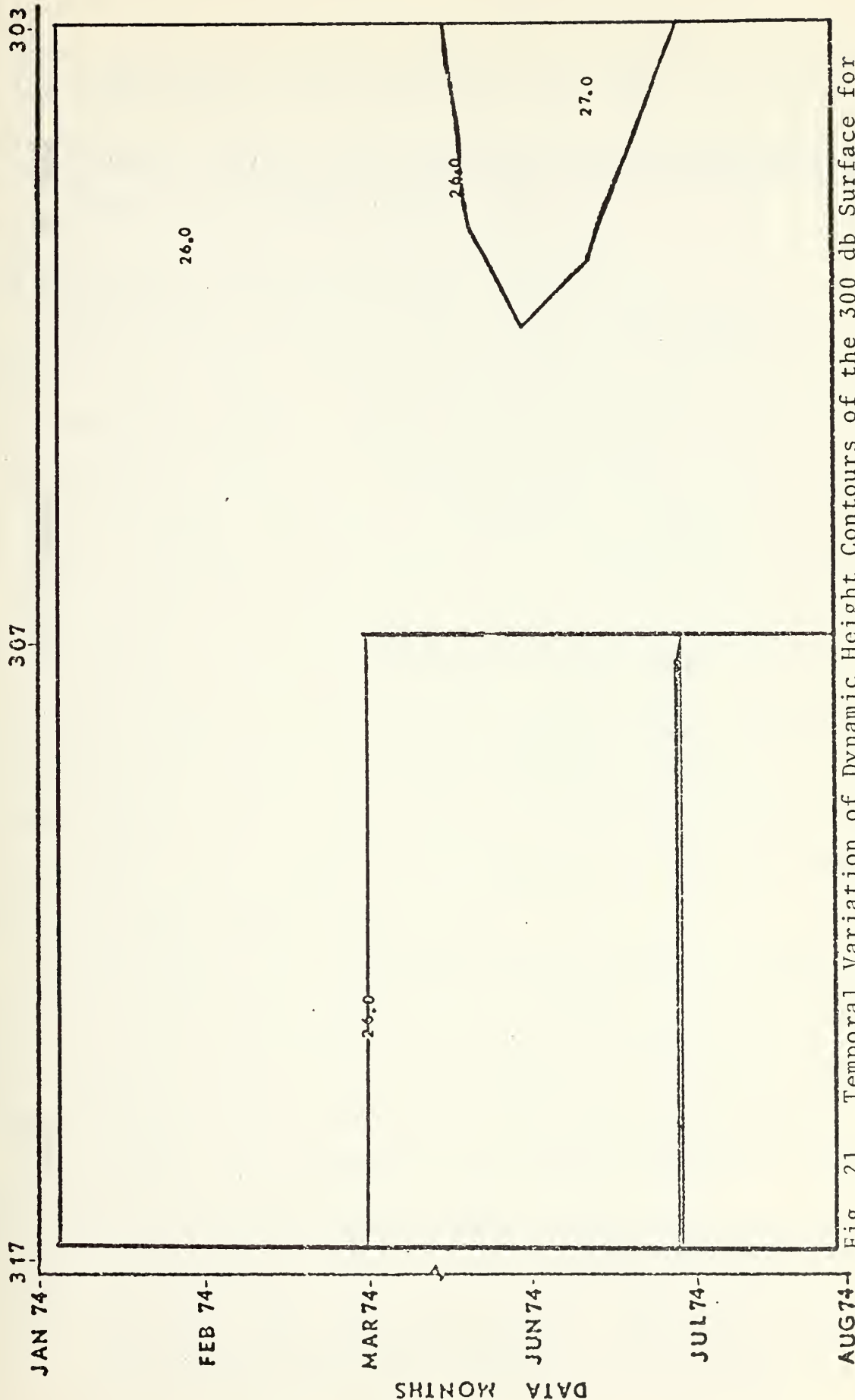


Fig. 21. Temporal Variation of Dynamic Height Contours of the 300 db Surface for January 1974 through August 1974. (Dynamic heights are in dynamic centimeters, relative to 500 db.)

- (2) A reversal in flow direction in the upper 200 meters occurs between June and July 1974.
- (3) Current speeds at depth during January through August 1974 are significantly less than speeds at depth during August 1973 through January 1974.

D. GEOSTROPHIC CURRENTS AND SALT TRANSPORT

The vertical structure of geostrophic flow normal to a section at latitude $36^{\circ} 40'N$ with respect to the 500 db surface is depicted by monthly vertical cross sections of geostrophic salt transport contours. Initially, both vertical cross sections of salt transport contours, and geostrophic isotachs were constructed. However, with exception of magnitude and dimensional units, the isotachs were nearly identical to the vertical contours of geostrophic salt transport. Consequently, the figures depicting vertical cross sections of geostrophic isotachs have been omitted in favor of the salt transport contours. Accordingly, figures 22 through 33 depict the vertical structure of geostrophic salt transport during August 1973 through February 1974, and June through August 1974.

In the discussion and presentation of results in this section, each monthly vertical cross section will be discussed in terms of its general flow and transport characteristics, its direction and current speeds, and the nature of the water.

To clarify the information presented in figures 22 through 33, the following comments are made,

- (1) The dimensional units of salt transport are (gm/sec-cm²).
- (2) Generally, every other contour has been labeled according to its particular transport value. Negative values (hatched area) indicate transport to the north, and positive values indicate transport to the south.

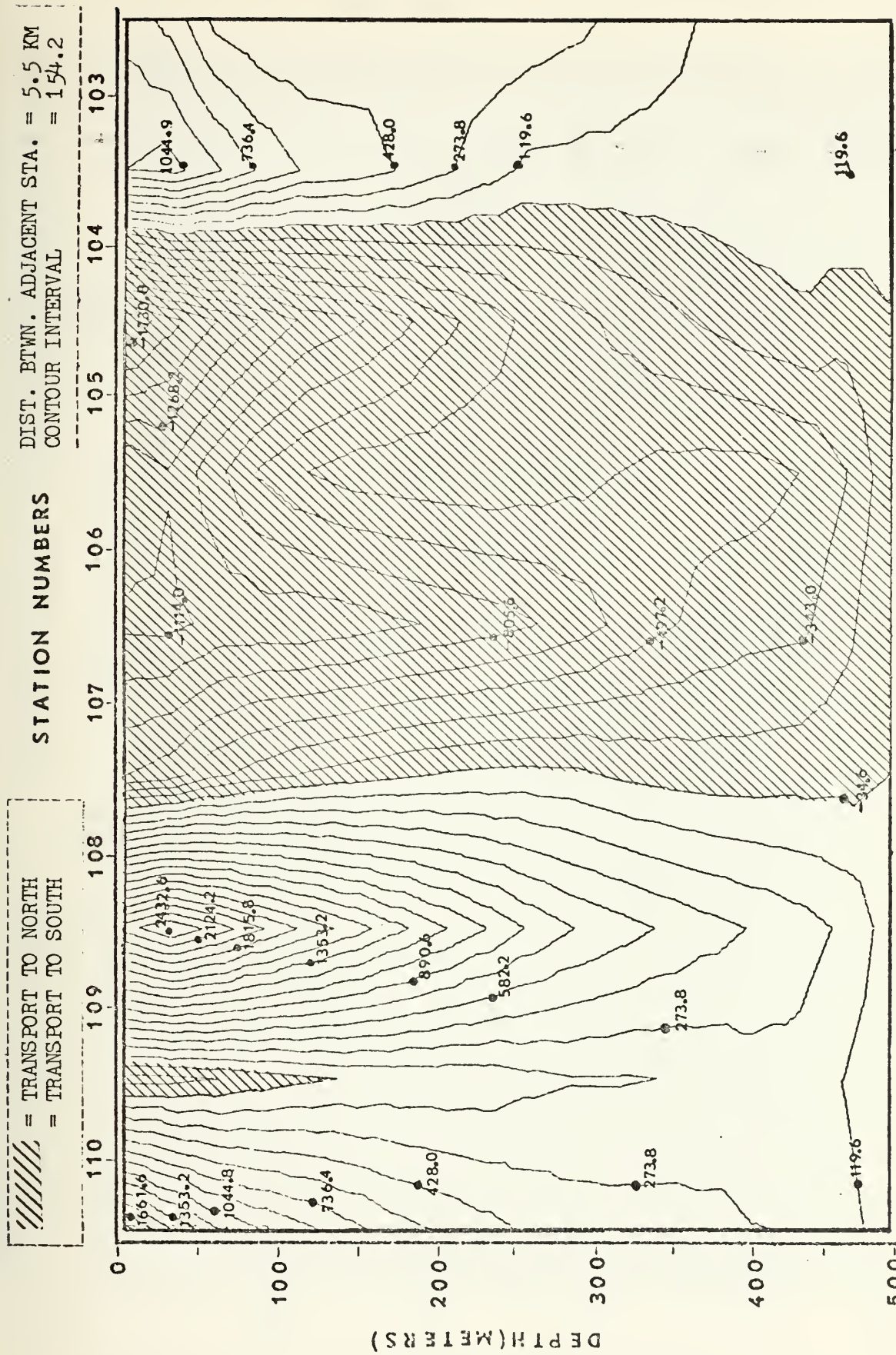


Fig. 22. Vertical Cross Section of Geostrophic Salt Transport Contours for Stations 111-102 during August 1973. (Negative transport values (hatched area) in (gm/sec-cm²) indicate transport to North.)

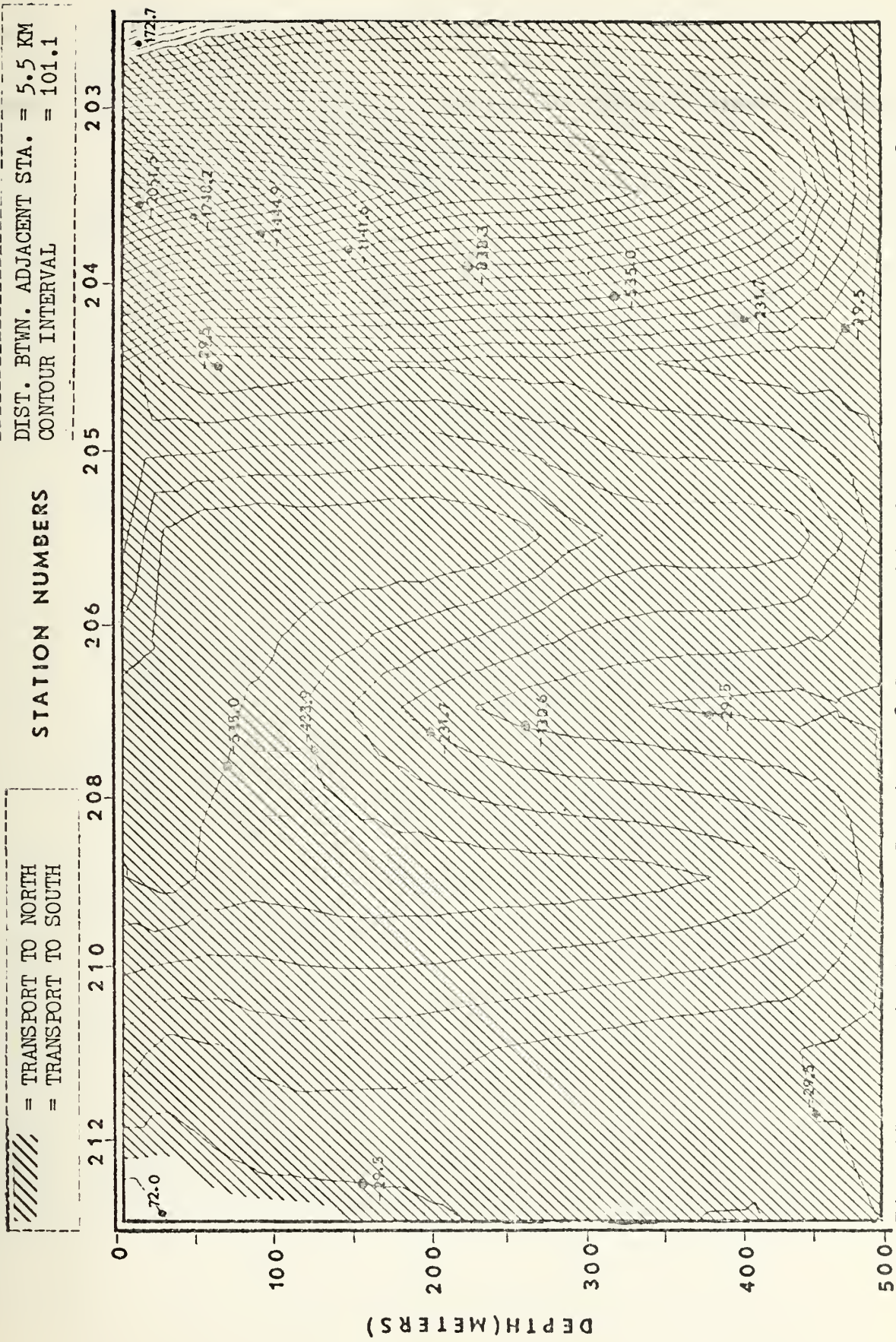


Fig. 23. Vertical Cross Section of Geostrophic Salt Transport Contours for Stations 214-202 during August 1973. (Negative transport values (hatched area) in gm/sec-cm^2) indicate transport to North.)

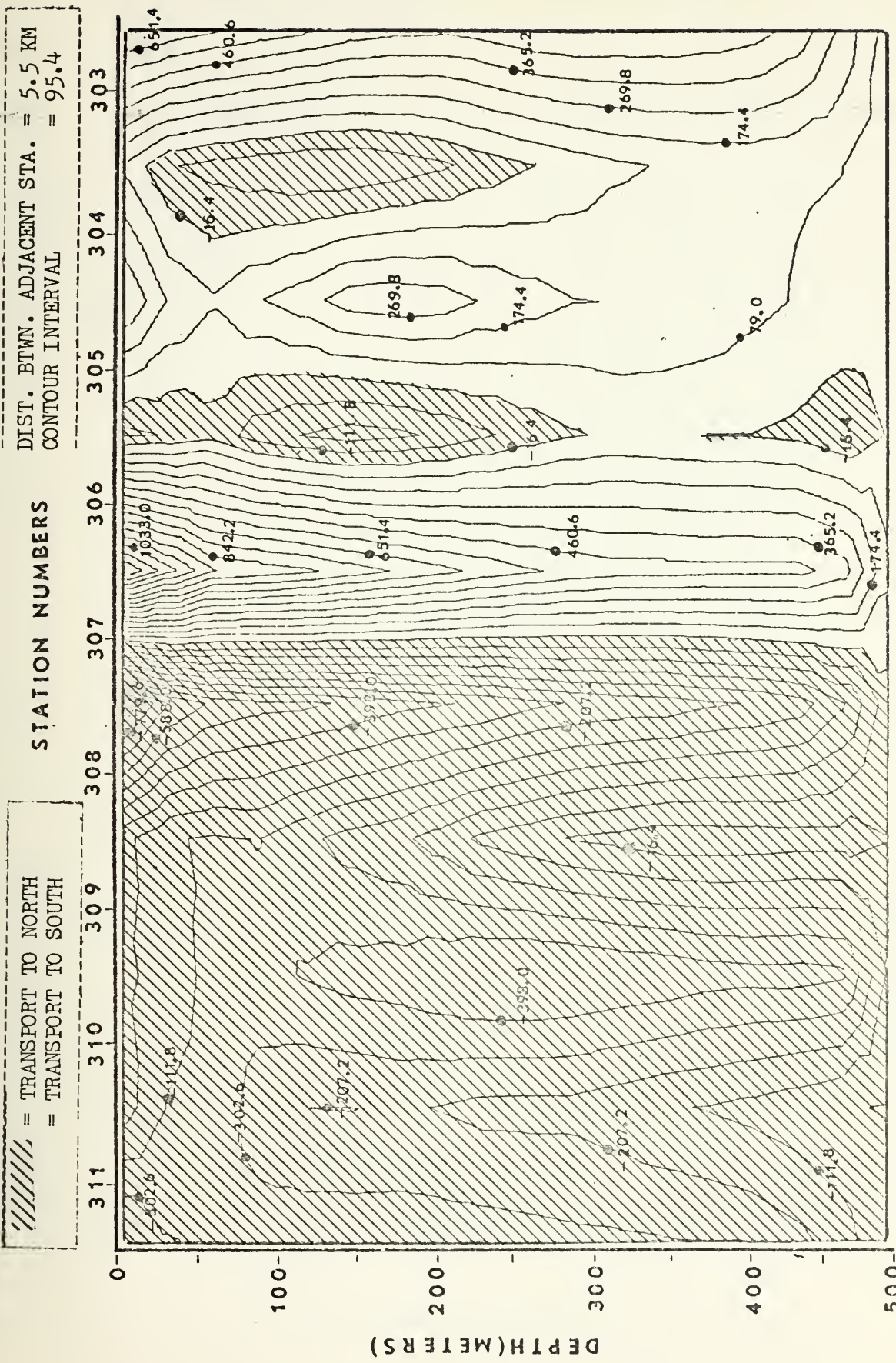
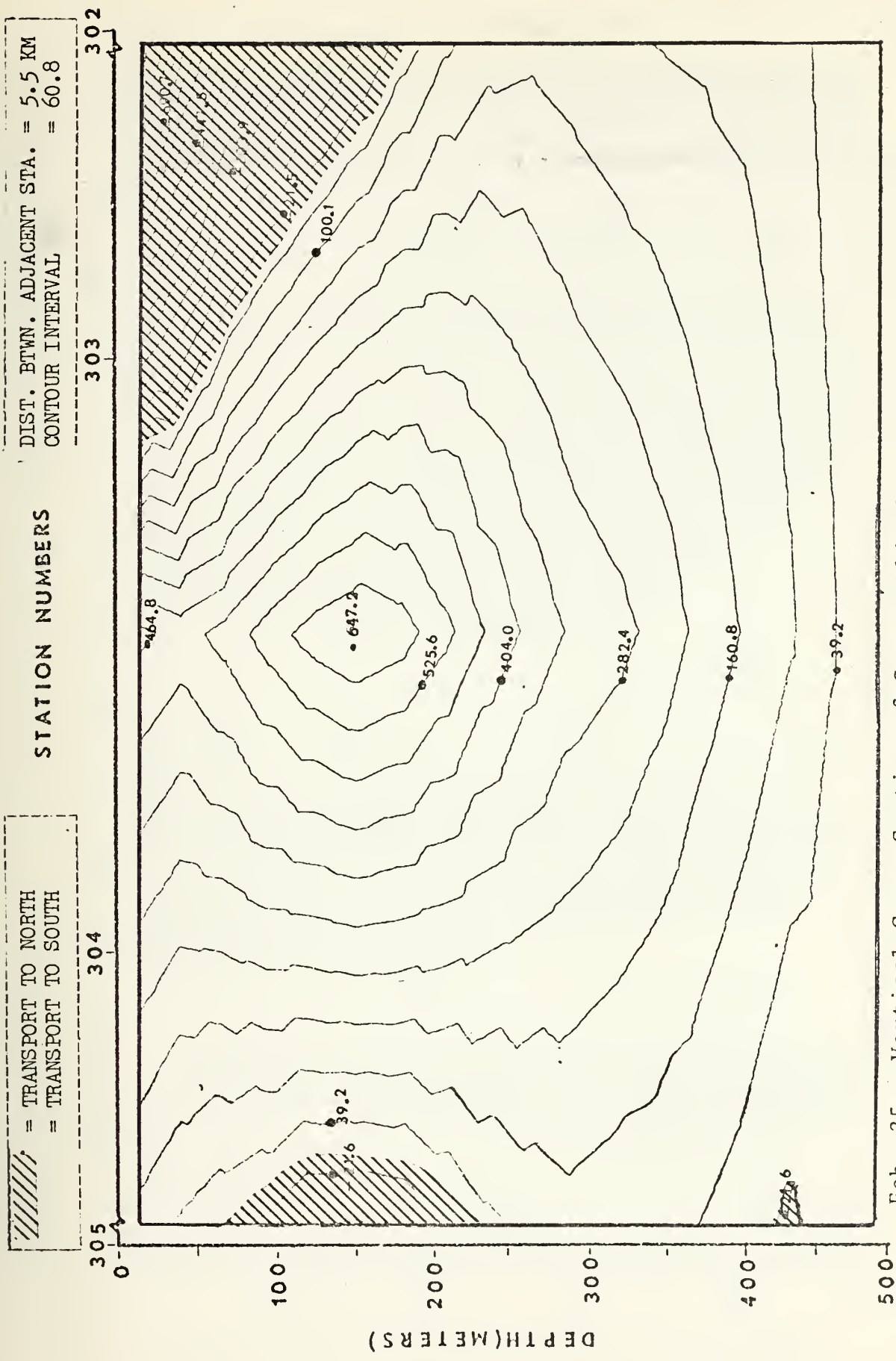
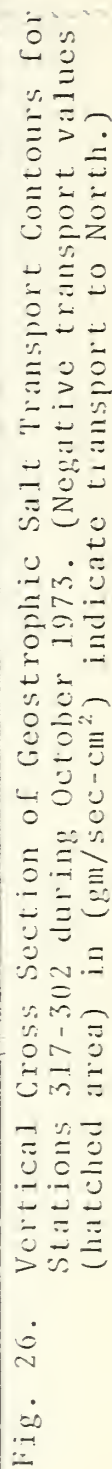


Fig. 24. Vertical Cross Section of Geostrophic Salt Transport Contours for Stations 315-302 during August 1973. (Negative transport values (hatched area) in (gm/sec-cm²) indicate transport to North.)



Feb. 25. Vertical Cross Section of Geostrophic Salt Transport Contours for Stations 317-302 during September 1973. (Negative transport values (hatched area) in (gm/sec-cm²) indicate transport to North.)

— TRANSPORT TO NORTH
— TRANSPORT TO SOUTH



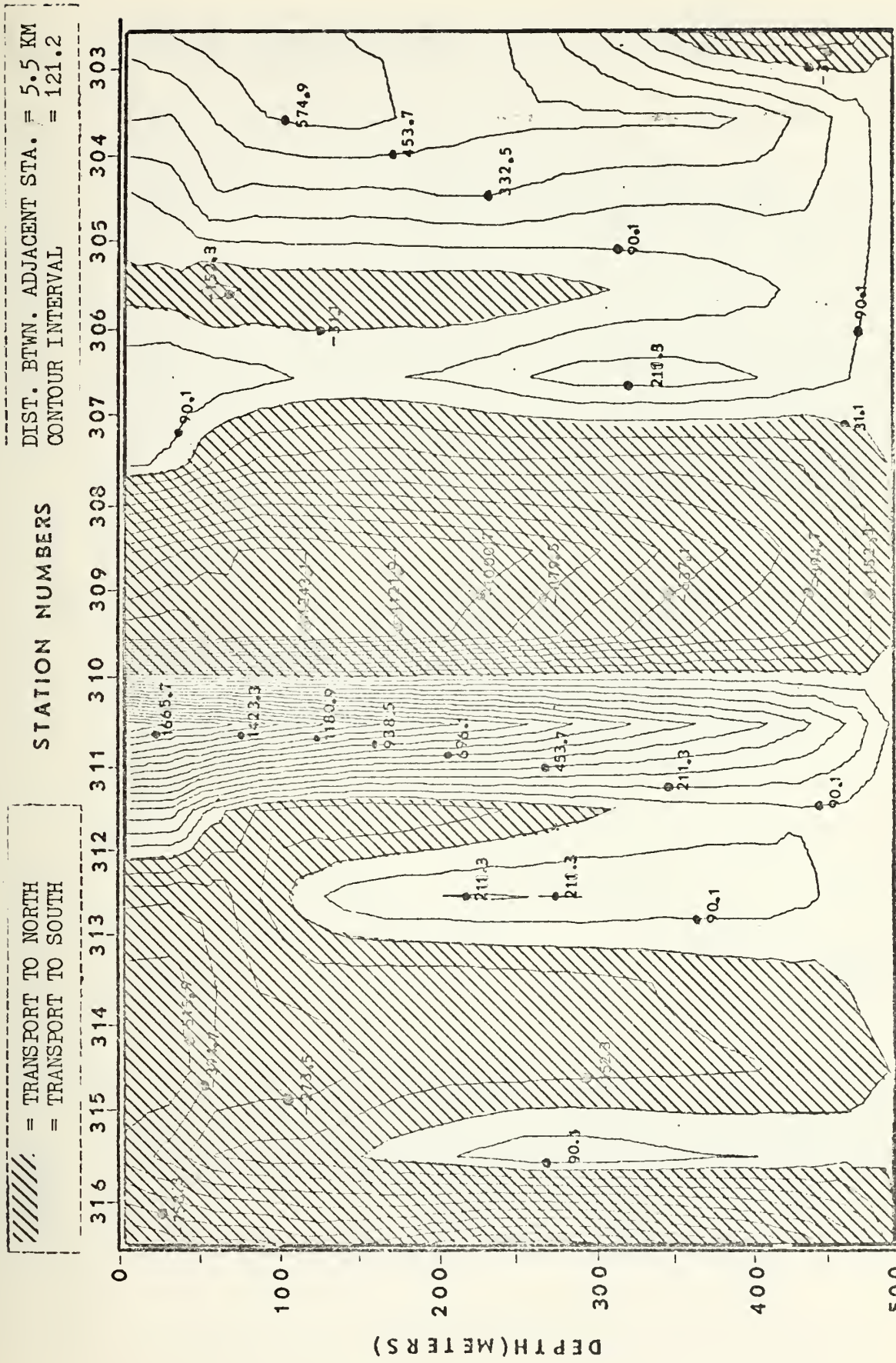
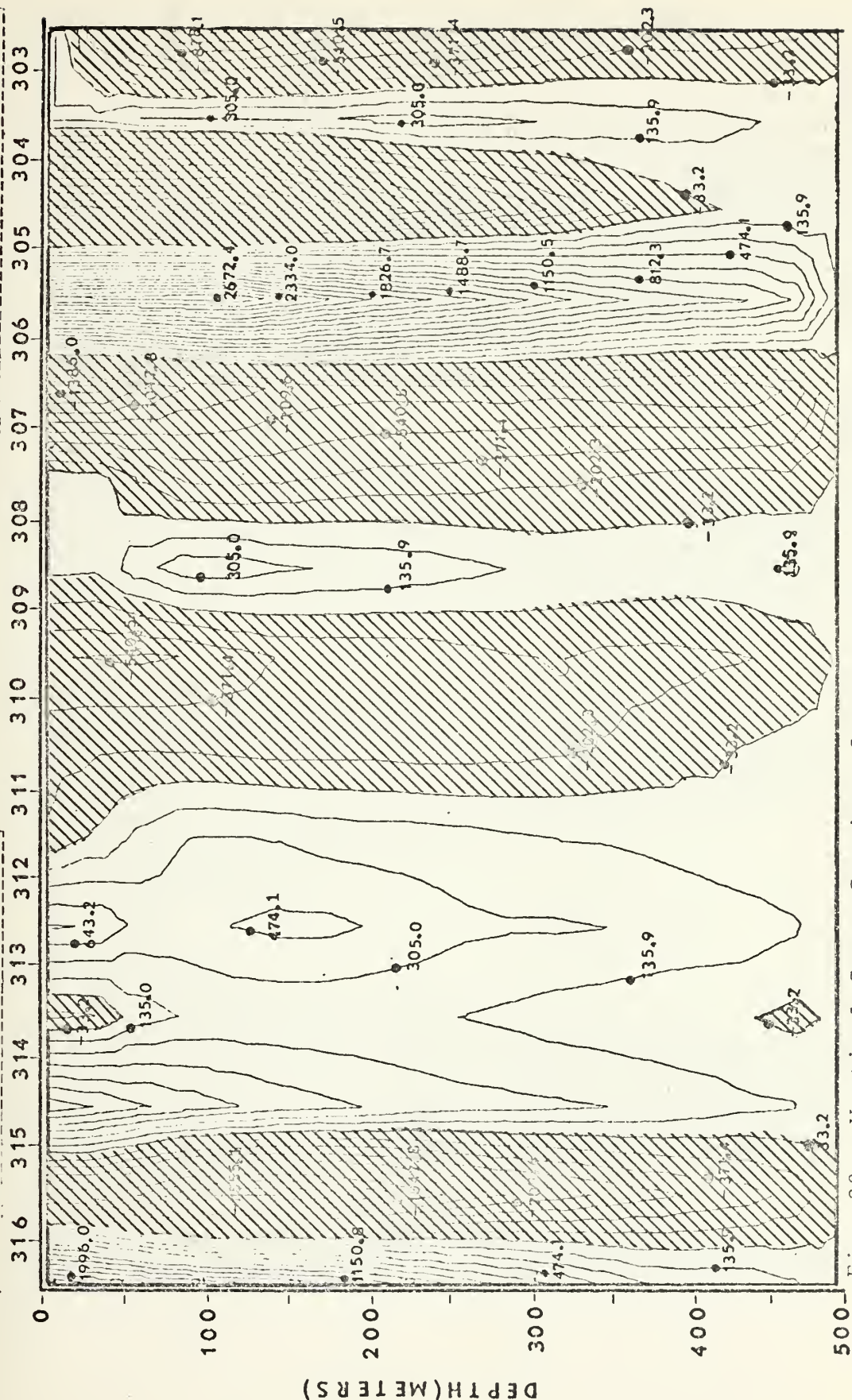
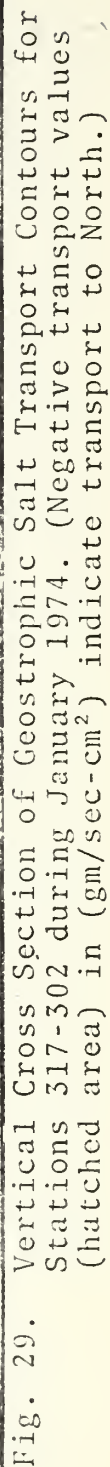


Fig. 27. Vertical Cross Section of Geostrophic Salt Transport Contours for Stations 317-302 during November 1973. (Negative transport values (hatched area) in (gm/sec-cm²) indicate transport to North.)

— TRANSPORT TO NORTH
— TRANSPORT TO SOUTH



= TRANSPORT TO NORTH
= TRANSPORT TO SOUTH



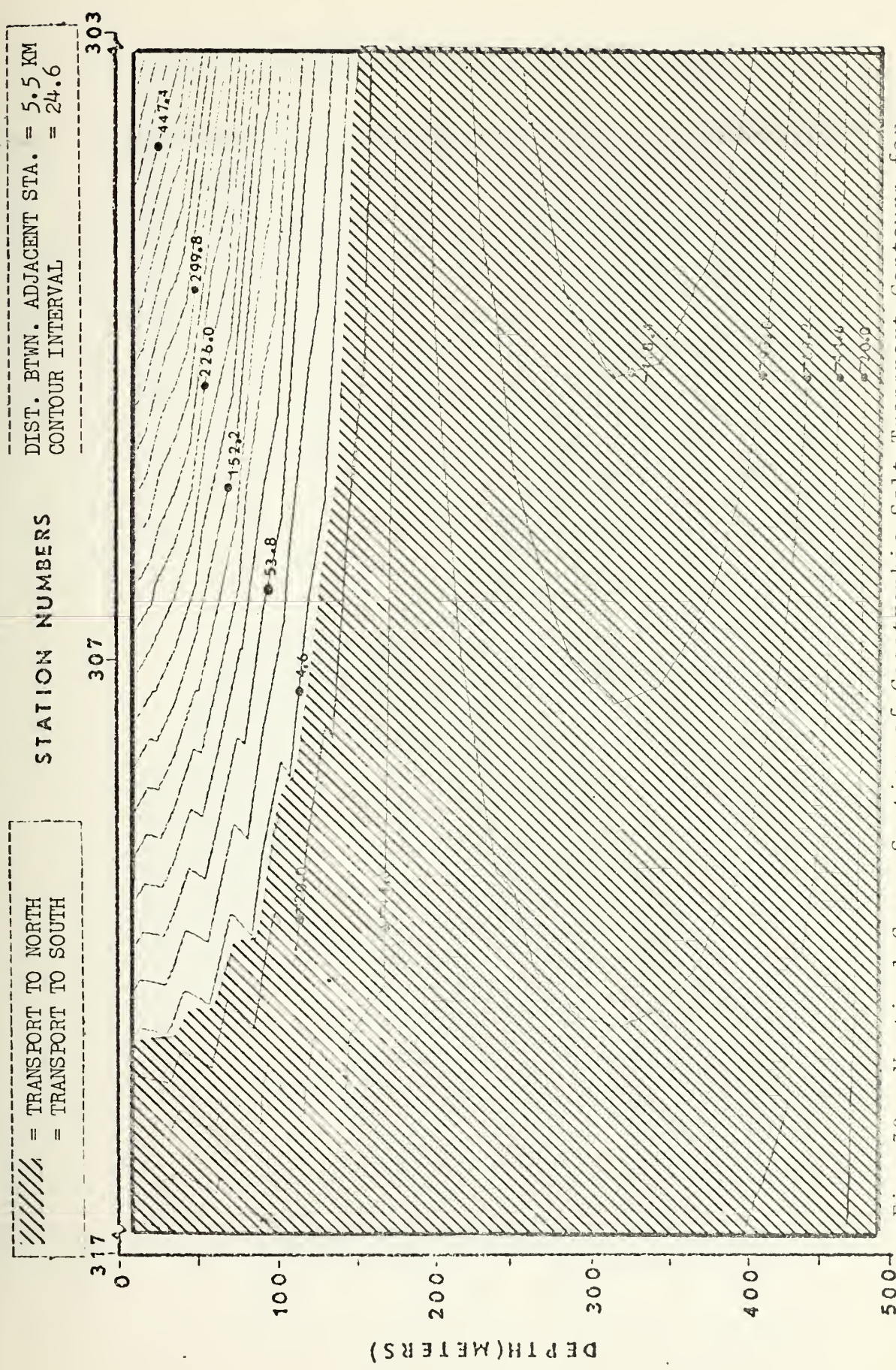


Fig. 30. Vertical Cross Section of Geostrophic Salt Transport Contours for Stations 317, 307, and 303 during February 1974. (Negative transport values (hatched area) in (gm/sec-cm²) indicate transport to North.)

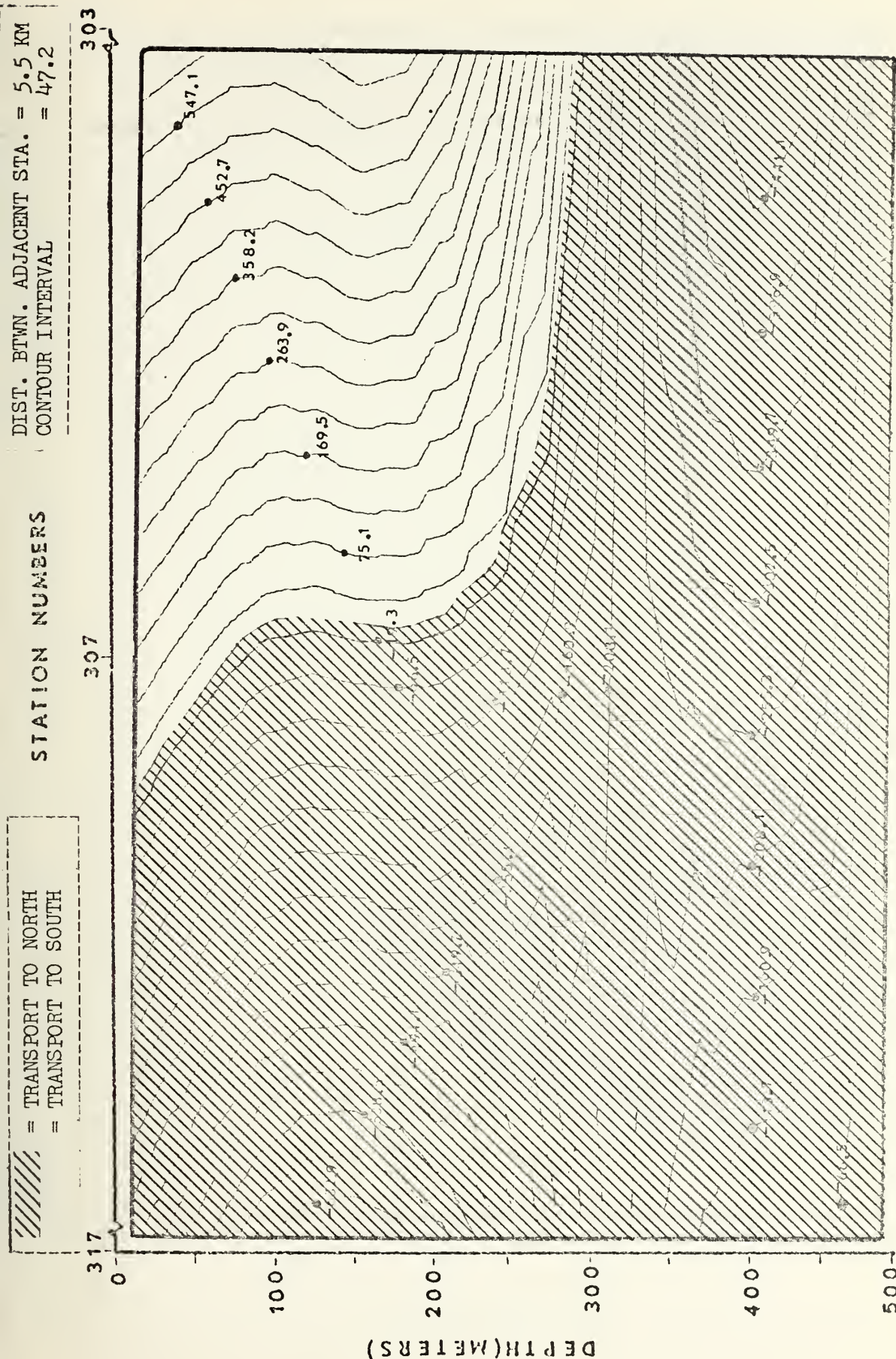


Fig. 31. Vertical Cross Section of Geostrophic Salt Transport Contours for Stations 317, 307, and 303 during June 1974. (Negative transport values (hatched area) in gm/sec-cm^2) indicate transport to North.)

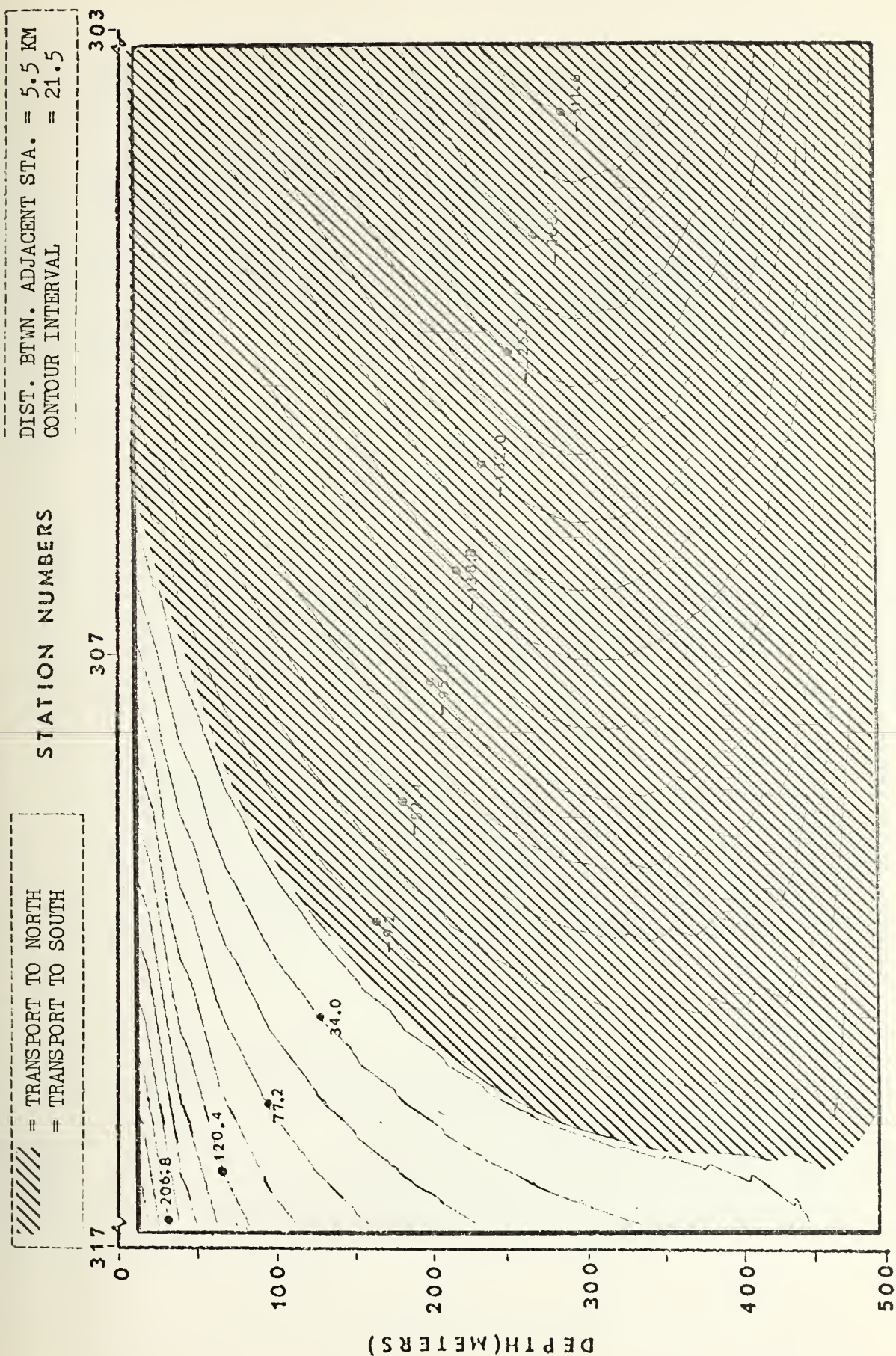


Fig. 32. Vertical Cross Section of Geostrophic Salt Transport Contours for Stations 317, 307, and 303 during July 1974. (Negative transport values (hatched area) in (gm/sec-cm²) indicate transport to North.)

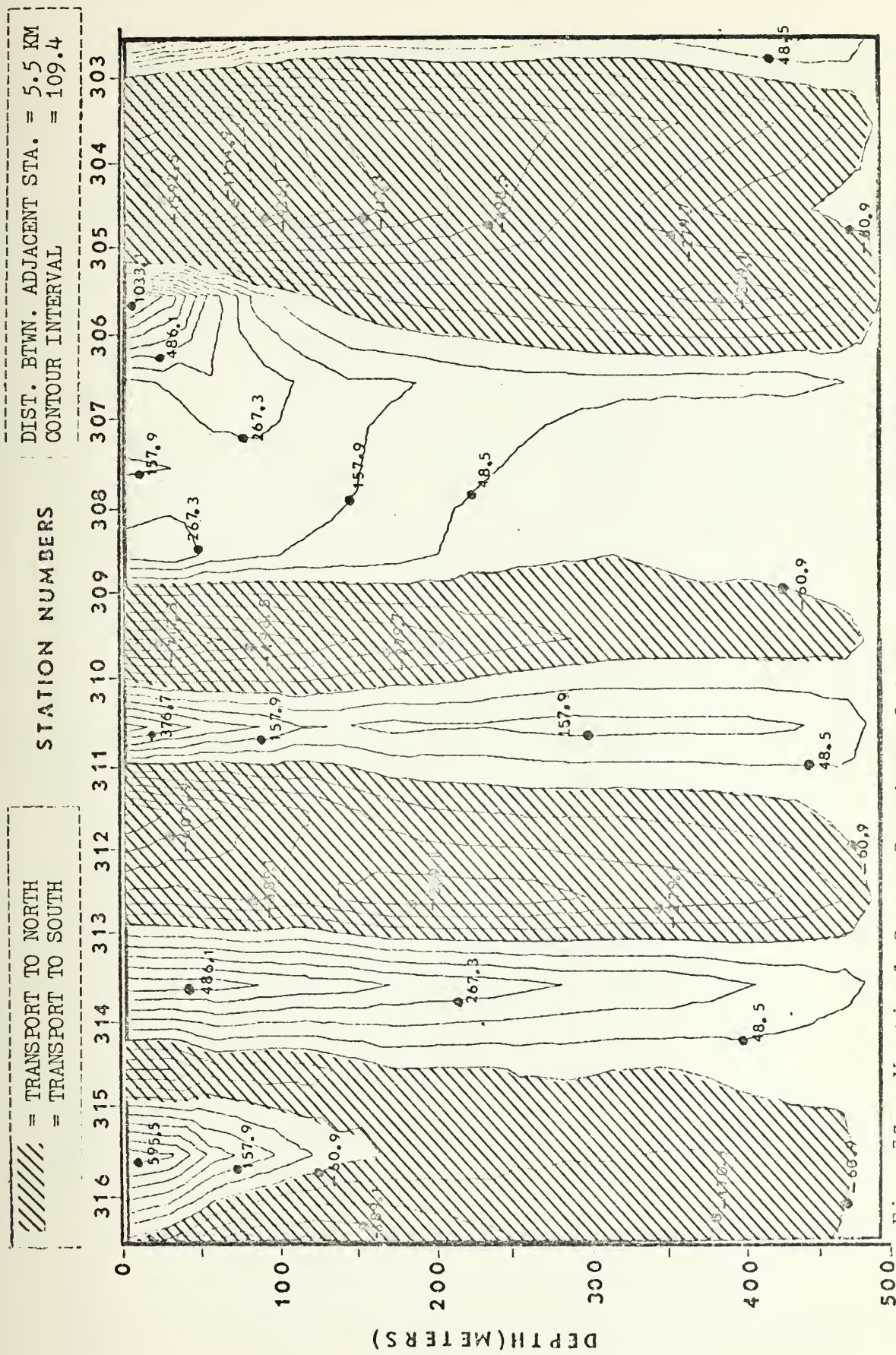


Fig. 33. Vertical Cross Section of Geostrophic Salt Transport Contours for Stations 317-302 during August 1974. (Negative transport values (hatched area) in (gm/sec-cm²) indicate transport to North.)

- (3) The exact contour interval is specified in units, (gm/sec-cm^2), at the upper right-hand corner of each figure.
- (4) The black dots adjacent to the individual transport values identify the corresponding contour line.
- (5) Distance between consecutively numbered adjacent stations is approximately 5.5 km. Note for figures 30 through 32, the distances between stations 303 and 307, and 307 and 317 are approximately 22 km and 55 km, respectively.

Consider the vertical structure of geostrophic flow during August 1973. Figures 22 through 24 depict the vertical structure of geostrophic salt transport contours during August 1973 for stations 111-102, 214-202 and 315-302, respectively. Examine, first, stations 111-102 along the $36^{\circ} 20'$ parallel of latitude depicted in figure 22. Poleward transport (shown by hatched area) located west of longitude $122^{\circ} 11'W$ is approximately 20 km in width and extends from the surface to 500 m. A maximum speed and salt transport of approximately 50 cm/sec and 1730 gm/sec-cm^2 , respectively, are indicated at the surface between stations 104 and 105. However, current speeds and salt transport values range generally from 30 cm/sec and 1114 gm/sec-cm^2 at the surface to 20 cm/sec and 736 gm/sec-cm^2 at 300 m. To the west of the poleward flow, geostrophy indicates an intense equatorward jet (maximum speed 70 cm/sec) at about longitude $122^{\circ} 27'W$. Farther west the flow is towards the equator with a maximum surface speed of 56 cm/sec decreasing with depth to less than 10 cm/sec at 300 m.

Figure 23 depicts the vertical structure in August 1973 along the $36^{\circ} 30'N$ parallel of latitude. Along the entire length of the station line, poleward transport is indicated

by geostrophy with a maximum surface speed of 62 cm/sec decreasing to 15 cm/sec at 300 m in the vicinity of longitude $122^{\circ} 09'W$. Farther to the west the poleward flow is characterized by speed and salt transport surface values of 15 cm/sec and 535.0 gm/sec-cm², respectively.

The vertical structure along the $36^{\circ} 40'N$ parallel of latitude during August is depicted by figure 24. East of longitude $122^{\circ} 22'W$ the flow is predominantly towards the equator while towards the west the flow is poleward. Maximum current speed and transport surface values are 40 cm/sec and 1320 gm/sec-cm², respectively, towards the equator. While the poleward flow to the west is approximately 35 cm/sec at the surface, it decreases to 10 cm/sec at 300 m.

There is some evidence that the equatorward and poleward jets indicated in figures 22 and 23 are realistic; the author refers to a concurrent study, examining the water mass characteristics by Blumberg [1975]. His findings indicate a sharp front-like water mass boundary along both jet axes. These water mass boundaries are indicated by large angles between isopycnal and isothermal surfaces from the near-surface to approximately 450 m. Additionally, there is theoretical basis for an equatorward jet in a dynamical model for eastern boundary flows [McNider and O'Brien, 1973], and drogue drifts [Wickham, 1975] in the same area also show large shears. These factors tend to support the view that the flow details are real; it should be noted, however, that mass distributions consistent with the calculated dynamic heights could also be produced by internal waves of amplitude 50 m.

Now consider the relation between the flow and structure. The current patterns indicated by both drogues and geostrophy tend to confirm an analysis of the structure which has elongated filaments of southern water flowing poleward in narrow bands, particularly near the coast [Wickham, 1975]. Specifically, drogue paths at 200 m in August 1973 tend to show this tendency.

The vertical structure of geostrophic flow in September 1973 is depicted in figure 25. Unfortunately, only the far eastern sector, stations 302 to 305, of the investigation area is shown. As in the preceding month, the flow in the eastern sector is predominantly to the south. There are maximum speed and salt transports of approximately 20 cm/sec and 650 gm/sec-cm² at 150 m. Towards the coastline there is a poleward flow contained in the upper 150 meters with a maximum current speed of 30 cm/sec at the surface.

Figure 26 depicts the vertical structure of geostrophic flow in October 1973. The flow structure consists of elements of several tens of kilometers in width extending from the surface to 500 m. Poleward flow dominates the first 20 km west of station 305, longitude 122° 15'W, with some indications that it is an undercurrent, since a maximum current speed and transport of approximately 20 cm/sec and 790 gm/sec-cm², respectively, lie below the surface from 100 to 200 meters. To the west of station 309 the flow appears to be alternating narrow bands of equatorward and poleward flow. The elements are typically 10 km wide, and extend from the surface to 500 m.

The vertical structure of geostrophic flow in November 1973 is depicted in figure 27. The flow is generally poleward

west of station 307 with a maximum salt transport of approximately 1370 gm/sec-cm^2 , and current speed of approximately 40 cm/sec at the surface. Upon comparing October and November 1973 vertical cross sections, there are indications that the equatorward flow east of station 307 is becoming weaker with current speeds less than 10 cm/sec at the surface. This is evidence that the onset of the Davidson Current period has taken place. The equatorward jet (maximum speed 55 cm/sec) axis located between stations 310 and 311 (longitude $122^{\circ} 33' \text{W}$) lies in a region with "northern" characteristics; i.e., it is anomalously cold for its density [Blumberg, 1975].

Figure 28 depicts the vertical structure of geostrophic flow in December 1973. The flow is predominantly poleward east of station 311 with the exception of a narrow-banded intense equator jet (maximum speed 77 cm/sec) located between stations 305 and 306 (longitude $122^{\circ} 15' \text{W}$). In this case, the intense equatorward jet axis does not clearly correspond to water of "northern" characteristics. West of station 311 the flow is generally more to the south but weaker than the narrow band of poleward flow. Maximum current speed and salt transport for the narrow band of poleward flow are 30 cm/sec and 1555 gm/sec-cm^2 . Whereas, with few exceptions, equatorward current speeds of less than 20 cm/sec characterize the flow within the upper 300 m.

The vertical structure of geostrophic flow in January 1974 is depicted in figure 29. Typical of the Davidson Current period, the general flow is towards the north. Poleward current

speeds vary from approximately 10 to 30 cm/sec in the upper 300 m. Two narrow jets, poleward and equatorward, have axes which are not unambiguously related to the water mass structure. The poleward jet reaches a maximum speed of 75 cm/sec while the equatorward jet reaches a maximum of 58 cm/sec. West of station 306 the flow structure is complex with regions of weak narrow band equatorward flow interspersed among a predominantly poleward flow.

Figure 30 depicts the flow in February 1974. The geostrophic salt transport contours shown in figure 30 as well as figures 31 and 32 are based on data obtained from three Nansen data stations. Consequently, the small-scale detail seen in previous figures is not recognizable. However, the general flow structure between January and February are similar. From concurrent analysis of water mass characteristics during this month there are indications that upwelling has begun along the coast. Figure 30 also tends to corroborate the onset of upwelling in that the poleward California countercurrent has disappeared, for the most part, above 200 m due to the onset of north-northwesterly winds, and is now in evidence as an undercurrent with a maximum current speed (this being a mean over 20 km) of approximately 4 cm/sec at 300 m. The flow above 100 m is predominantly equatorward with a maximum speed and salt transport of approximately 16 cm/sec and 520 gm/sec-cm², respectively.

The vertical structure of geostrophic flow in June 1974 is depicted in figure 31. The California undercurrent is well

defined and confined below 200 m in the eastern part of the investigation area during June. Maximum current speed (14 cm/sec) and salt transport (490 gm/sec-cm^2) occur at 400 m. Farther west the undercurrent tends to surface as evidenced by the maximum speed and transport values occurring between 100 and 200 meters.

Figure 32 depicts the vertical flow structure in July 1974. The undercurrent has pushed closer to the coast, and shows signs of its ascent to the surface. The maximum poleward current speed (9 cm/sec) and salt transport (312 gm/sec-cm^2) are located at 300 m. Concurrent analyses of the water mass characteristics indicate that upwelling was not present along the station line at $36^{\circ} 40' \text{N}$ but was possibly present along the $36^{\circ} 30' \text{N}$ parallel line. This is not surprising since upwelling tends to be a localized phenomenon. The flow depicted in figure 32 appears to agree with the seasonal period of the California Current System.

The vertical structure of geostrophic flow in August 1974 is depicted in figure 33. The ascending undercurrent depicted in figure 32 has now surfaced with a maximum poleward current speed and salt transport of 53 cm/sec and 1810 gm/sec-cm^2 , respectively, at the surface. The major northward flow between stations 303 and 306 coincides with southern water in a separate analysis [Blumberg, 1975]. Typical of the California Current during transition to the oceanic period, the flow is becoming more equatorward. However, west of station 309 the flow is apparently complex and characterized by narrow bands (less than 10 km wide) of weak poleward and equatorward flow.

From figures 22 through 33, it is apparent that the flow and structure in this area of the California Current System are highly complex. The vertical structure, in many cases, is characterized by what appears to be narrow bands of flow less than 10 km in width and by water mass elements of similar scale. Accordingly, only in surveys with sampling grid lengths less than 10 km could the complex structure and flow be realistically depicted. Of course, there still remains the question whether the results depicted here by geostrophy are correct in regards to the small-scale features. However, a sampling grid length of this order in the construction of a data base, in addition to extensive independent measurements of the current system, seems to be required if the behavior of the southern water and its associated current system are to be described.

V. SUMMARY AND CONCLUSIONS

A. GENERAL

The oceanic region just west of the continental shelf off Monterey Bay was examined in detail during the period August 1973 through August 1974. Observations were made on a horizontal grid much finer than is traditionally used in oceanographic surveys in order to permit horizontal definition of narrow bands of flow, and a continuous STD profiler was used to provide high density vertical sampling. Accordingly, the analyses of the data base over the 13-month period provided a description of the mesoscale components of the apparent geostrophic flow and its temporal and spatial variability in the California Current System. Some of the more interesting features of the flow and its structure with depth are provided below.

B. PATTERNS OF CURRENT FLOW AND THEIR STRUCTURE WITH DEPTH

Patterns of current flow inferred from geostrophy with respect to the 500 db surface in August 1973 showed the surface current flow patterns to be similar to those found at depths from the surface to 375 m. The area studied was characterized by narrow bands of interlacing poleward and equatorward flow. Generally, the flow in this area tended to follow bathymetric contours, and there was evidence that the bottom topography influenced the direction of flow within the 1,000 fathom curve. Additionally, independent current flow

measurements made using parachute drogues during August 1972 and August 1973 by Wickham [1975] confirm the general flow patterns inferred from geostrophy.

C. TEMPORAL VARIATION OF THE GEOSTROPHIC FLOW

The variation of the geostrophic flow with time inferred from geostrophy with respect to the 500 db surface showed that the general surface flow patterns over the time period, August 1973 through January 1974, are similar to those found at depths from the surface to 300 m. The geostrophic flow was more intense during the period November 1973 through January 1974 than during August 1973 through October 1973 in the upper 200 m. What appear to be narrow bands of poleward and equatorward flow, which could result from transient effects due to the redistribution of mass by internal waves, characterized the study area. Additionally, the equatorward flow in the eastern sector of the area appeared to be more intense in the upper 200 m during December 1973 and January 1974 than the poleward flow. Finally, the time history showed the poleward flow to shift to the west with time.

The variation of the geostrophic flow with time over the period January 1974 through August 1974 showed the flow to be more intense during January, June and August 1974 than during February, March and July 1974. Additionally, current speeds at depth during January through August 1974 were significantly less than speeds at depth during August 1973 through January 1974. And a reversal in flow direction in the upper 200 m was revealed between June and July 1974.

D. GEOSTROPHIC CURRENT AND SALT TRANSPORT

The vertical structure of geostrophic flow, depicted by monthly vertical cross sections of geostrophic salt transport contours, showed three distinct oceanographic seasons, and were consistent with Skogsberg's [1936] annual cycle of the California Current System. The flow and structure inferred from geostrophy in the area appeared highly complex with interlacing narrow bands (many times less than 10 km in width) of poleward and equatorward flow. Additionally, equatorward and poleward jets (speeds up to 77 cm/sec) were found to have axes corresponding to sharp water mass boundaries indicated by large angles between the isopycnal and isothermal surfaces.

A P P E N D I X A

TITLE	DIGISTD
PROGRAMMERS	R.E.GREER,R.E.BLUMBERG,AND J.G.HUGHES EXTENSIVELY MODIFIED AN ORIGINAL PROGRAM,MIZ2, BY R.G.PAQUETTE.
DOCUMENTATION	R.E.GREER
DATE	26 JUNE 1975
PURPOSE	PROGRAM READS, CONVERTS, AND PROCESSES DIGITIZED SALINITY, TEMPERATURE, AND DEPTH DATA FROM A CALMA DIGITIZER 7-TRACK TAPE. DATA ARE COMPUTED AND STORED EVERY 0.01 INCHES OF DEPTH FOR OUTPUT TO PRINTER, PUNCHED CARD, OR 9-TRACK TAPE. PROGRAM CONVERTS DEPTH, TEMPERATURE, SALINITY AND COMPUTES SOUND VELOCITY AND SIGMA-T FOR EACH INDIVIDUAL OCEANOGRAPHIC STATION AND PRINTS THE DATA IN A STATION DATA SUMMARY.
SEQUENCE	<p>THE PROGRAM PERFORMS ALL FUNCTIONS IN THE FOLLOWING SEQUENCE OF OPERATIONS:</p> <ul style="list-style-type: none"> (A) INITIALIZES ALL ARRAYS AND VARIABLES. (B) COMPUTES TABLE OF SALINITY AND TEMPERATURE SCALE CONVERSION FACTORS. (C) SKIPS XXX NUMBER OF RECORDS IF NSKP VARIABLE SET OTHER THAN ZERO ON CONTROL DATA CARD. (D) READS PAIR OF DATA CARDS (LABEL AND DAT) FOR RECORD BEING PROCESSED. (E) TERMINATES PROGRAM IF ISTOP=1 OR AT THE END OF PROCESSING THE NN-TH RECORD. (F) SKIPS UNREADABLE OR BAD RECORDS IF NRCSKP VARIABLE SET TO INDIVIDUAL RECORD NUMBER. (G) READS USEABLE DATA RECORD INTO A-ARRAY. (H) MOVES BYTES OF A-ARRAY INTO 4-BYTE WORDS OF B-ARRAY TO ALLOW PROCESSING BY STANDARD FORTRAN. (I) PROCESSES RAW B-ARRAY. <ul style="list-style-type: none"> (1) IF HEADER RECORD, PROGRAM DECODES HEADER LABEL AND COMPARES TO LABEL SUPPLIED BY DATA CARD. (2) IF TRACER RECORD, PROGRAM ADDS AND STORES CUMULATIVE SUMS OF X AND Y DISTANCE TRAVEL. (J) INDEXES THE VALUES OF CUMULATIVE DISTANCE BY INCREASING DEPTH UNITS; INTERPOLATES TO FILL GAPS IN THE FINAL ARRAY WHICH MAY OCCUR AT THE POINTS OF SCALE CHANGES IN THE SEGMENTED RECORD. (K) INSERTS MANUALLY ENTERED SURFACE AND NEAR SURFACE DATA

VALUES VIA DATA CARD.
 (L) INCREMENTS RECORD COUNT AND REPEATS STEPS (D) THRU (K)
 UNTIL ALL RECORDS PROCESSED FOR PARTICULAR STATION.
 (M) ADJUSTS ALL FINAL DATA ARRAYS TO THE LENGTH OF THE
 SHORTEST.
 (O) COMPUTES SOUND VELOCITY.
 (P) COMPUTES SIGMA-T.
 (Q) COMPUTES CONSECUTIVE RECORD SERIALIZATION FOR TAPE
 OUTPUT NUMBERING SCHEME.
 (R) CONVERTS LETTER DESIGNATOR MONTH/YEAR CODE, AMONC, TO
 REAL *8 MONTH/YEAR.
 (S) PRINTS OCEANOGRAPHIC DATA STATION SUMMARY.
 (T) WRITES ALL STATION DATA ON TAPE IF TAPE=.TRUE..
 (U) PUNCHES ALL STATION DATA ON CARDS SUITABLE FOR THESIS II
 INPUT IF CARDS=.TRUE..
 (V) PUNCHES DEPTH, TEMPERATURE, AND SALINITY ON CARDS
 SUITABLE FOR INPUT TO HYDROGRAPHIC PROGRAM IF GCARDS=.TRUE..
 (W) INITIALIZES ALL ARRAYS AND VARIABLES FOR PROCESSING
 NEXT STATION DATA.
 (X) REPEATS STEPS (D) THRU (W) UNTIL ALL RECORDS PROCESSED,
 ISTOP=1, OR DESIRED RECORD READ.

FEATURES

PROGRAM CONSISTS OF MANY MARKED PROPERTIES WHICH MAKE IT A
 HIGHLY VERSATILE PROGRAM FOR PROCESSING OCEANOGRAPHIC DATA
 FROM TAPE. SOME OF THESE PROPERTIES ARE LISTED UNDER THE
 FOLLOWING SIX GENERAL CATEGORIES:

- (A) INPUT
 - (1) 7-TRACK CALMA DIGITIZER TAPE IN BCD.
 - (2) TWO DATA CARDS REQUIRED PER TRACE SEGMENT OR HEADER
 LABEL RECORD. EXAMPLE: AN STD TEMPERATURE TRACE
 CONSISTING OF FOUR SEGMENTS OR RECORDS WILL REQUIRE FOUR
 PAIRS OF DATA CARDS.
- (B) SUBROUTINES
 - (1) TPRD - AN ASSEMBLER LANGUAGE SUBROUTINE FOR READING
 MAGNETIC TAPE WHICH CANNOT BE READ BY STANDARD METHODS.
 NOTE: TPRD ALLOWS USER TO SKIP BAD RECORDS WHILE TAPRD
 (W. R. CHURCH COMPUTER CENTER SUBROUTINE) DOES NOT.
 - (2) CHMOVE - MOVES BYTES OF A-ARRAY INTO FOUR BYTE WORDS
 OF B-ARRAY TO ALLOW PROCESSING BY STANDARD FORTRAN.
 - (3) CONDNS - CONDENSES, INDEXES, AND CONVERTS THE
 CUMULATIVE DISTANCE X AND Y ARRAYS, BY INCREASING DEPTH
 UNITS, TO TEMPERATURE AND DEPTH OR SALINITY AND DEPTH.
 - (4) OUTI - PRINTS OCEANOGRAPHIC STATION DATA SUMMARY.
 - (5) SVEL - COMPUTES SOUND VELOCITY FROM DEPTH, TEMPERATURE
 AND SALINITY ACCORDING TO WILSON'S EQUATION.
 - (6) SIGMT - COMPUTES SIGMA-T FROM TEMPERATURE AND
 SALINITY ACCORDING TO H.O. 614 P. 91.
- (C) AUTOMATIC DATA PROCESSING/HANDLING

- (1) APPLICABLE TO MULTIPLE DEPTH, TEMPERATURE AND SALINITY SCALES.
- (2) HANDLES OPERATOR MISTAKES MADE IN TRACING STD CURVES ON CALMA DIGITIZER.
- (3) SKIPS AN INITIAL NUMBER OF RECORDS SPECIFIED BY NSKP AND INDIVIDUAL RECORDS (EVEN IF UNREADABLE) SPECIFIED BY THE ARRAY NRC SKP.
- (4) DECODES 7-TRACK TAPE HEADER LABELS AND TRACE RECORDS.
- (5) COMPUTES DATA FOR EVERY 0.01 INCHES DEPTH BUT SELECTABLE FOR GREATER DEPTH INTERVAL.
- (6) ENTERS HAND-ENTERED DATA FOR SURFACE AND NEAR-SURFACE VALUES.
- (7) EDITS OUT ANY UNFILLED ARRAY POSITIONS.
- (8) COMPUTES CONSECUTIVE RECORD SERIALIZATION FOR TAPE OUTPUT NUMBERING SCHEME.
- (9) COMPUTES SOUND VELOCITY AND SIGMA-T.
- (D) (1) WRITES FIRST TWENTY-FIVE VALUES OF B-ARRAY FOR INSPECTION PURPOSES.
- (2) WRITES EVERY TWENTIETH VALUE OF STD ARRAYS FOR DATA INSPECTION PURPOSES.
- (3) WRITES PROGRAM STATEMENT NUMBER IN ADDITION TO MESSAGE WHEN SIGNIFICANT OPERATIONS OCCUR.
- (E) TROUBLE-SHOOTING
- (1) HANDLES MULTIPLE KEYBOARD AND TRACER SYMBOL ENTRIES.
- (2) PROVIDES FOR A MISSED HEADER LABEL OR INCOMPLETE HEADER LABEL.
- (3) HANDLES MISSING INTER-RECORD GAPS.
- (4) HANDLES DELETE RECORD BY INCREMENTING RECORD COUNT AND READING SAME PAIR OF DATA CARDS AGAIN.
- (5) COMPARES CARD HEADER LABEL AGAINST TAPE HEADER LABEL AND ACCEPTS CARD VALUES IF CARD AND TAPE DISAGREE.
- (F) OUTPUT
- (1) PRINTER- TWO PRINTING VARIABLES, PRT1 AND PRT2.
- (A) OCEANOGRAPHIC DATA STATION SUMMARIES.
- (B) PRT2, PROVISION ONLY.
- (2) CARD- TWO CARD PUNCHING ROUTINES, CARDS AND GCARDS.
- (A) PUNCHED DATA CARDS SUITABLE FOR USE WITH THE SISI1.
- (B) PUNCHED DATA CARDS FOR INPUT TO HYDROGRAPHIC PROGRAM.
- (3) TAPE- 9-TRACK TAPE
- (4) PLOTTING- PROVISIONS FOR PLOTTING ROUTINES ACTUATED BY PLOT1 AND PLOT2 ARE NOT PRESENTLY PROGRAMMED.

ARGUMENTS

PROGRAM CONSISTS OF MANY TERMS, ARRAYS AND VARIABLES. THE FOLLOWING IS A BRIEF DESCRIPTION OF THE IMPORTANT ARGUMENTS LISTED ALPHABETICALLY UNDER TWO GENERAL CATEGORIES.

(A) ARRAYS

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(19) IH      THE NEXT STATION.
(20) IHDR    = NUMBER OF HAND-ENTERED SURFACE OR
              NEAR-SURFACE DATA VALUES.
(21) ISTOP   = WHEN SET EQUAL TO 1 PERMITS
              ENTERING MISSING OR FAULTY DIGITIZER
              TAPE HEADER INFO VIA DATA CARD.
              = TERMINATES PROGRAM IF SET EQUAL TO
              1 ON A FINAL &DAT CARD PRECEDED BY
              A LABEL CARD.
(22) JREC    = VARIABLE USED TO COUNT RECORDS FOR
              RECORD SERIALIZATION PURPOSES.
(23) JSKIP   = WHEN SET EQUAL TO 1 ON THE LABEL
              CARD, CAUSES THE PROGRAM TO ACCEPT
              DATA ON AN &CONTRL CARD.
              = THE KEYBOARD SYMBOL ON THE
              DIGITIZER TAPE.
(24) KEY     = NUMBER OF DATA POINTS TO BE PUNCHED
              BY CARDS PUNCHING ROUTINE.
(25) KCRD    = NUMBER OF RECORDS PROCESSED FOR
              PARTICULAR STATION.
(26) KDTA    = HEADER TYPE DATA CARD WHICH
              IDENTIFIES STATION NUMBER AND TYPE
              TRACE, TEMPERATURE OR SALINITY.
(27) LABEL   = NUMBER OF CARDS PUNCHED BY CARDS
              PUNCHING ROUTINE.
(28) NCRDS   = THE INDEX AT THE LAST USEFUL ARRAY
              POSITION OF THE X(DEPTH) ARRAY.
(29) NE      = VARIABLE USED TO INDICATE MISSING
              END OF RECORD GAP ON TAPE.
(30) NGIRG   = NUMBER OF INITIAL RECORDS ON TAPE
              SKIPPED.
(31) NSKP    = SALINITY SCALE CONSTANT.
(32) SCON    = CORRECTION FACTOR ADDED TO SALINITY
              DATA VALUES.
(33) SCOR    = TEMPERATURE SCALE CONSTANT.
(34) TCON    = CORRECTION FACTOR ADDED TO
              TEMPERATURE DATA VALUES.
(35) TCOR    = MONTH AND YEAR
(36) WMONTH

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DATA DECK

THE FOLLOWING IS A SAMPLE DATA DECK REQUIRED BY THIS PROGRAM. SAMPLE BELOW SHOWS DATA CARDS REQUIRED FOR TWO STATIONS, 3070 AND 3080. ALSO SHOWN IS 'STATION END' CARD WITH ISTOP SET EQUAL TO ONE.

```

&CONTRL NN=400,TAPE=F,GCARDS=F,ISQZ=01,NSKP=90,NRCSKP=103,104,105,
106,107,108,109,110,111,112,113,114,115,116,117,118,119,120,121,122,123,
124,125,126,175,176,177,178,179,180,181,182,183,184,185,186,ICSQZ=8,

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IGSQZ=8,TCOR=-0.08,SCOR=0.04,&END
UCM004 INCLUDES STATIONS 3070 THRU 302R MINUS 3080,3090 AND 3140.
STATION 3070 TEMPERATURE HEADER
&DAT ISTA=307,AMONC=0,IDEPTH=99,IDSCL=1,ICODE=0,ITSCL=4,ISCL=3,IP=0,
DH=0.0,IH=11.24,SH=33.40,IH=1,&END
STATION 3070 TEMPERATURE TRACE
&DAT IDEPTH=00&END
STATION 3070 TEMPERATURE HEADER
&DAT IDEPTH=99,ITSCL=3&END
STATION 3070 TEMPERATURE TRACE
&DAT IDEPTH=00&END
STATION 3070 TEMPERATURE HEADER
&DAT IDEPTH=99,IDSCL=2&END
STATION 3070 TEMPERATURE TRACE
&DAT IDEPTH=00&END
STATION 3070 TEMPERATURE HEADER
&DAT IDEPTH=99,ITSCL=2&END
STATION 3070 TEMPERATURE TRACE
&DAT IDEPTH=00&END
STATION 3070 SALINITY HEADER
&DAT IDSCL=1,IDEPTH=99,ICODE=1,ITSCL=4,&END
STATION 3070 SALINITY TRACE
&DAT IDEPTH=00&END
STATION 3070 SALINITY HEADER
&DAT IDSCL=2,IDEPTH=99,IP=1,&END
STATION 3070 SALINITY TRACE
&DAT IDEPTH=00&END
STATION 3080 TEMPERATURE HEADER
&DAT ISTA=308,AMONC=0,IDEPTH=99,IDSCL=1,ICODE=0,ITSCL=4,ISCL=3,IP=0,&END
STATION 3080 TEMPERATURE TRACE
&DAT IDEPTH=00&END
STATION 3080 TEMPERATURE HEADER
&DAT IDEPTH=99,ITSCL=3,&END
STATION 3080 TEMPERATURE TRACE
&DAT IDEPTH=00&END
STATION 3080 TEMPERATURE HEADER
&DAT IDEPTH=99,IDSCL=2&END
STATION 3080 TEMPERATURE TRACE
&DAT IDEPTH=00&END
STATION 3080 TEMPERATURE HEADER
&DAT IDEPTH=99,ITSCL=2&END
STATION 3080 TEMPERATURE TRACE
&DAT IDEPTH=00&END
STATION 3080 SALINITY HEADER
&DAT IDSCL=1,IDEPTH=99,ICODE=1,ITSCL=4,&END
STATION 3080 SALINITY TRACE
&DAT IDEPTH=00&END
STATION 3080 SALINITY HEADER

```



```

&DAT IDSCCL=2, IDEPTH=99, IP=1, &END
STATION 3080 SALINITY TRACE
&DAT IDEPTH=00&END
STATION END
C (END OF FILE)

```

THE FOLLOWING IS AN EXAMPLE OF JOB CONTROL LANGUAGE AND DECK SET-UP REQUIRED TO USE DIGISTD. THIS PARTICULAR DECK SET-UP WAS USED TO WRITE FILE 6 ON 9-TRACK TAPE, NPS-527. THE 9-TRACK TAPE WAS WRITTEN AT 800 BPI WITH A LRECL OF 40 AND BLKSIZE OF 32,520. HINDSIGHT INDICATES THAT IT IS DESIRABLE TO WRITE THE TAPE AT A BLKSIZE OF 8000 VICE 32,520 SINCE IT IS EXTREMELY ADVANTAGEOUS TO KEEP FOLLOW ON TAPE PROCESSING PROGRAMS SMALL (IE LESS THAN 100K).

```

//GUCMSTD6 JOB (2006,0823,0542), RE GREER SMC 1413, TIME=10,
//  TYPRUN=HOLD,
//  MSGCLASS=D
//  EXEC FORTCLG, REGION.FORT=150K, REGION.GO=350K, DEST=0
//FORT.SYSIN DD *
//  ( MAIN SOURCE DECK AND SUBROUTINES)
//GO.FT06F001 DD SPACE=(CYL,(40,03)), SYSOUT=0
//GO.FT07F001 DD DUMMY
//GO.FT08F001 DD UNIT=3400-4, VOL=SER=NPS527, LABEL=(06,SL,OUT),
//  DISP=(NEW,KEEP), DCB=(DEN=2, RECFM=FB, LRECL=40, BLKSIZE=32520),
//  DSN=S2006.UCM7374
//GO.METTAP DD UNIT=2400-1, VOL=SER=UCM004, DISP=OLD, LABEL=(,NL),
//  DCB=(DEN=1, TRTCH=ET)
//GO.SYSIN DD *
//  (DATA DECK)
C (END OF FILE)

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MAIN PROGRAM

***** D I G I S T D *****

DIMENSION X(4001), Y(4001), LABEL(19), SH(50), TH(50), DH(50),
 1INTA(10), INSA(10), NRCSKP(99), DCON(3), CORRST(7),
 2IREC(1801), AMONCA(13), EVENT(13),
 3INTEGER B(8001), ZER, ONE, FLAG, DLTRC, ZER, DLR, BLANK, GCRD,
 4A(2001), TWO, THREE, FOUR, FIVE, SIX, SEVEN, EIGHT, TEN, ELEVEN, AMONT, FG
 LOGICAL PRT1, PRT2, PLT1, PLT2, TAPE, ENDFL, CARDS, SKIP, GCARDS
 COMMON /C1/ I(1801), S(1801), D(1801), SV(1801), SIG(1801),
 1SI(1801), T1(1801), D2(1801), T2(1801)
 REAL *8EVENT, WMONTH
 DATA AMONCA/ 'H', 'I', 'C', 'K', 'L', 'O', 'P', 'Q', 'R', 'U', 'V', 'W', 'Z' /
 DATA EVENT/ 'AUG 1973', 'SEP 1973', 'OCT 1973', 'NOV 1973', 'DEC 1973',
 1, 'JAN 1974', 'FEB 1974', 'MAR 1974', 'APR 1974', 'MAY 1974', 'JUN 1974',
 2, 'JUL 1974', 'AUG 1974' /

NAMELIST /CONTRL/ NN, PRT1, PRT2, PLT1, PLT2, TAPE, ENDFL, CARDS, ISTOP, IP
 1, IH, NRCSKP, NSKP, JSKP, IREQ, ISQZ, ICSQZ, IGSCZ, GCARDS, ICOR, SCOR
 2/DAT/SH, TH, DH, IH, ICODE, ISCL, ITSC, IDSC, IP, IDEPTH, ISCZ, IGSCZ, ICSQZ
 3, SCOR, TCON, IHDR, NDIRG, ISTA, TCON, SCOR, DCUN, CCRD, SKIP, CURRS, CORR,
 4AMONC, TAPE, CARDS, GCARDS

***** DEFINE SYMBOLS *****

DEFINE SYMBOLS, NOTING THAT THE LEFT THREE HEX BYTES IN EACH
 ELEMENT OF B END UP FILLED WITH BLANKS
 DATA DOL/ '\$\$\$', STAR/Z4040405C/, KEY/Z4040405F/, ONE/Z404040F1/,
 1FLAG/Z40404050/, DLTRC/Z40404060/, MINUS/Z40404061/,
 2DLR/Z4040405B/, BLANK/ ' ', ZER/Z404040F0/, TWO/Z404040F2/,
 3THREE/Z404040F3/, FOUR/Z404040F4/, FIVE/Z404040F5/,
 4MTWO/Z404040E2/, MTHREE/Z404040E3/, MFOUR/Z404040E4/, MFIVE/Z404040E5
 5/, SIX/Z404040F6/, SEVEN/Z404040F7/, EIGHT/Z404040F8/, NINE/Z404040F9
 6/, TEN/Z404040F0/, ELEVEN/Z4040407B/

***** DEFINE CONSTANTS *****

THE FOLLOWING CONVERSION FACTORS ARE IN HUNDRETHS OF INCHES PER
 UNIT OF S OR T. THEY MAY BE OVERRIDDEN BY THE DATA CARDS.
 DCON(1) = 3.153
 DCON(2) = 1.261

CCCCCCC


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180 DCON(3) = 0.631
185 TCUN = 189.680
190 SCUN = 474.200

195 *****
200 ***** INITIALIZE ALL TERMS AND VARIABLES *****
205 *****
210 *****
215 *****
220 *****
225 *****
230 *****
235 *****
240 *****
245 *****

DATA CARDS/.FALSE./,CORD/0.0/,ENDFL/.FALSE./,FG/0/,GCARDS/.FALSE./
1,ICUDE/0/,ICSQZ/1/,IGSQZ/1/,IH/0/,IHDR/0/,IP/0/,IPS/8000/,ISCL/0/,
2,IDEPTH/1/,IDSC/0/,ISTA/999/,ITSC/0/,
3,ISQZ/1/,ISTOP/0/,JJJ/0/,JJJ/0/,JREC/0/,JSAV/0/,KBARF/0/,KSCARF/0/
4,KDTAF/1/,KDTA/1/,KDT1/1/,KDT2/1/,KDT1/1/,KDT2/1/,KDT1/1/,
5,KS2/1/,KT/1/,KT1/1/,KT2/1/,NE/0/,NOIRG/0/,NSKP/0/,PLT1/.FALSE./,
6PLT2/.FALSE./,PRT1/.TRUE./,PRT2/.FALSE./,SCOR/0.0/,SKIP/.FALSE./,
7TAPE/.FALSE./,TCOR/0.0/

250 *****
255 ***** INITIALIZE ALL ARRAYS *****
260 *****
265 *****
270 *****
275 *****
280 *****
285 *****
290 *****
295 *****
300 *****
305 *****
310 *****
315 *****
320 *****
325 *****
330 *****
335 *****
340 *****
345 *****
350 *****
355 *****
360 *****
365 *****
370 *****
375 *****
380 *****
385 *****
390 *****
400 *****

GIVE THE ARRAYS INITIAL VALUES

DO 20 J=1,50
SH(J) = 0.0
TH(J) = -5.0
DH(J) = 0.0
20 CONTINUE

DO 30 J=1,1801
D(J) = 0.0
T(J) = -5.0
S(J) = 0.0
D2(J) = 0.0
T2(J) = -5.0
S2(J) = 0.0
T1(J) = -5.0
S1(J) = 0.0
IREC(J) = 0
30 CONTINUE

DO 40 J=1,99
NRCSKP(J) = 0
40 CONTINUE

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415
420
425
430
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445
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455
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465
470
475
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485
490
500
505
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520
525
530
535
540
545
550
555
560
565
570
575
580
585
590
595
600
605
610
615
620
625
630
635
640
645
650
655

40 CONTINUE

      DO 50 J=1,7,1
      CORR(J) = 0.0
      CORR(J) = 0.0
      CONTINUE
50

      PROVIDE INITIAL INDICES FOR 10 SALINITY SEGMENTS (INSA) AND 10
      TEMPERATURE SEGMENTS (INTA).
      INSA(1) = 1
      INSA(2) = 1
      INTA(1) = 1
      INTA(2) = 1

      DO 60 J=3,10
      INSA(J) = 980
      INTA(J) = 980
      CONTINUE
60

      COMPUTE A TABLE OF CONVERSION FACTORS FOR SALINITY AND
      TEMPERATURE. CORR AND CORR REPRESENT THE S OR T VALUE AT THE
      LEFT HAND SIDE OF THE STD TRACE. THE VALUE (J) TO BE USED WILL
      COME FROM ISCL AND ITSCL. HYTECH STD MODEL 9006 STANDARD
      TEMPERATURE AND SALINITY SCALES 1 THRU 7 ARE PROVIDED FOR IN
      THIS PROGRAM IN ADDITION TO DEPTH SCALES 1,2, AND 3. FOR
      CONVENIENCE THE SCALES FOR TEMPERATURE, SALINITY, AND DEPTH ARE
      DEFINED HERE.
      TEMPERATURE SCALES:
      ITSCL 1 = -2 TO 3 (DEG CELSIUS)
      ITSCL 2 = -2 TO 7 (DEG CELSIUS)
      ITSCL 3 = 0 TO 11 (DEG CELSIUS)
      ITSCL 4 = 10 TO 15 (DEG CELSIUS)
      ITSCL 5 = 14 TO 19 (DEG CELSIUS)
      ITSCL 6 = 18 TO 23 (DEG CELSIUS)
      ITSCL 7 = 22 TO 27 (DEG CELSIUS)

      SALINITY SCALES:
      ISCL 1 = 30.0 TO 32.0 (PPT)
      ISCL 2 = 31.0 TO 33.0 (PPT)
      ISCL 3 = 33.0 TO 35.0 (PPT)
      ISCL 4 = 34.0 TO 36.0 (PPT)
      ISCL 5 = 36.0 TO 38.0 (PPT)
      ISCL 6 = 37.0 TO 39.0 (PPT)
      ISCL 7 = 30.0 TO 40.0 (PPT)

      DEPTH SCALES:

```



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C      READ WILL BE SKIPPED; WHEREAS NRCSKP=22,23,24,50 PERMITS RECORD
C      NUMBERS 22,23,24,50 TO BE SKIPPED INDIVIDUALLY.)
C
C      IPS = -8000
C      80 CALL TPRD (A,IPS,&100,&120)
C
C      ***** RESET IPS FOR NORMAL TAPE PROCESSING *****
C      *****
C      IPS = 8000
C      90 WRITE (6,90) IIS
C      90 FORMAT (/5X,15,' RECORDS SKIPPED'/)
C      90 GO TO 140
C
C      IF END OR ERROR MESSAGES OCCUR DURING SKIP ROUTINE, PROGRAM
C      STOPS.
C      100 WRITE (6,110) IIS
C      110 FORMAT (/5X,'FOUND END OF FILE ON RECORD',I4,'DURING SKIP PROCESS',
C      110 /)
C      120 GO TO 1580
C      130 WRITE (6,130) IIS,A(1),A(2),A(3),A(4)
C      130 FORMAT (/5X,'READ ERROR ON RECORD',I5,'ERROR STATISTICS ARE: ',4Z8
C      130 /)
C      140 GO TO 1580
C      ***** END SKIP LOOP *****
C      *****
C      REDEFINE LOOP INDEX TO START AT ONE.
C      140 NNN = NN-NSKP
C      ***** START MAIN LOOP FOR EACH RECORD *****
C      *****
C      IT = 1
C      150 IF (IT.GT.NNN) GO TO 1580
C      IPS = 8000
C      NREC = IT+NSKP
C      160 WRITE (6,160) NREC
C      160 FORMAT (/5X,'LABEL 150; START MAIN LOOP. RECORD NO. ',I3/)
C
C      PROGRAM PERMITS TREATMENT OF A KNOWN NUMBER OF RECORDS, NN, OR
C      STOPPING WHEN I STOP=1 ON STATION LABEL CARD. THE LABEL CARD HAS
C      TWO DIGITS FOR CONTROL. THE 77-TH COLUMN IS JSKIP; IF JSKIP=0,
C      ONLY TWO CARDS ARE READ. THE 78-TH COLUMN IS ISTOP; IF ISTOP=1,
C      THE PROGRAM STOPS. NORMAL TERMINATION OF THE PROGRAM MAY BE
C      ACCOMPLISHED IN TWO DISTINCT WAYS. EITHER SET NN TO DESIRED
C      RECORD TO STOP OR PLACE A 'STATION END' LABEL CARD AT END OF DATA
C      DECK WITH A ONE IN COLUMN 78. THE 79-TH COLUMN IS AMONC; AMONC IS

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900
 905
 910
 915
 920
 925
 930
 935
 940
 945
 950
 955
 960
 965
 970
 975
 980
 985
 990
 995
 1000
 1005
 1010
 1015
 1020
 1025
 1030
 1035
 1040
 1045
 1050
 1055
 1060
 1065
 1070
 1075
 1080
 1085
 1090
 1095
 1100
 1105
 1110
 1115
 1120
 1125
 1130
 1135


```

C      AN ALPHABETIC LETTER CODE FOR MONTH AND YEAR. THIS CODE IS
C      CONVERTED TO LITERAL MONTH AND YEAR LATER ON IN PROGRAM.
C
170  READ (5,170) LABEL,JSKIP,ISTOP,AMONC
      FORMAT (19A4,2I1,A1)
      IF (ISTOP.GT.0) GO TO 1580
      READ (5,DAT)
      WRITE (6,180) LABEL
      WRITE (6,DAT)
C      NORMALLY TWO CARDS, LABEL AND DAT, ARE READ PER RECORD.
C      LESS FREQUENTLY CHANGED VARIABLES ARE ON CONTRL DATA CARD.
      JJJ = 0
      NOIRG = 0
      IF (JSKIP.EQ.0) GO TO 190
      READ (5,CONTRL)
      WRITE (6,CONTRL)
180  FORMAT (/5X,19A4/)

C      PROVISION IS MADE HERE FOR A MISSED HEADER LABEL ON TAPE (AN
C      OPERATOR ERROR). IF IHDR=1, AND ALL INFORMATION REQUIRED IS PLACED
C      ON PARTICULAR DAT CARD, THE PROGRAM BRANCHES OFF TO 610 AND
C      WRITES STATION INFORMATION AND MESSAGE THAT HEADER IS MISSING,
C      AND FINALLY RETURNS TO 150 TO START NORMAL PROCESSING OF TRACE
C      RECORD DATA. NOTE, RECORD COUNT IS NOT INCREMENTED IN THIS LOOP.
190  IF (IHDR.EQ.1) GO TO 610
200  CONTINUE

C      NOTE: IN EARLIER VERSIONS OF THIS PROGRAM, THERE WAS AN
C      INTERPOLATION ROUTINE HERE FOR HAND-ENTERED DATA BUT IT WAS
C      DELETED SINCE VERY SELDOM ONE HAD CAUSE TO USE IT. HOWEVER, THE
C      CAPABILITY FOR HAND-ENTERED DATA HAS BEEN RETAINED BUT IN A
C      DIFFERENT FORM. SEE COMMENTS FOLLOWING STATEMENT NO. 1130.
C-----
210  FORMAT (5X,11F7.2/5X,11F7.2/5X,11F7.2/5X,11F7.2/5X,11F7.
      12/5X,11F7.2/5X,11F7.2/5X,3F7.2,60X,16)
220  FORMAT (5X,10I5,10INSA,1)
230  FORMAT (5X,10I5,10INTA,1)
240  FORMAT (5X,10KS,KS1,KS2,KT,KT1,KT2,JJJ,NE,KDTH1,KDTH2,KD
      1TA,KDT1,JJJJ,/4X,8I5,2I6,3I5)
C-----
C-----
IPLACE=245
WRITE (6,210) (D(J),J=1,1801,20)
WRITE (6,210) (T(J),J=1,1801,20),IPLACE

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WRITE (6,210) (S(J),J=1,1801,20),IPLACE
WRITE (6,220) (INSA(J),J=1,10)
WRITE (6,230) (INTA(J),J=1,10)
WRITE (6,240) KS,KS1,KS2,KT1,KT2,JJJ,NE,KDTH1,KDTH2,KDTA,KDT1,J
1JJJ

FILL THE A ARRAY WITH DOLLARS

DO 250 I=1,2001
THE 2001 ASSURES THAT THE LAST WORD OF A WILL CONTAIN DOLLARS
SINCE 2000 WORDS OR 8000 BYTES OF DATA ARE READ IN.
A(I) = DOL
250 CONTINUE

FILL B WITH BLANKS

DO 260 I=1,8000
B(I) = BLANK
260 CONTINUE

PROGRAM EXAMINES LIST OF INDIVIDUAL BAD RECORDS,NRCSKP,AND
SKIPS THEM. IF NRCSKP(1)=0, THE SKIP ROUTINE IS BY-PASSED.
CAUTION: DO NOT REMOVE PAIRS OF DATA CARDS FOR INDIVIDUALLY
SKIPPED CARDS.

IN USING THE CALMA DIGITIZER, SPURIOUS BLANK RECORDS OCCURRED
THROUGHOUT THE TAPE ON NUMEROUS OCCASSIONS. MANY OF THESE
OCCURRENCES WERE LATER TRACED TO EQUIPMENT MALFUNCTION.
HOWEVER, IF A BLANK RECORD OCCURS DURING A HEADER LABEL RECORD
NOTHING IS LOST SINCE HEADER INFO MAY BE INSERTED BY CARD AND
SETTING IHDR=1. ON THE OTHER HAND, IF A BLANK RECORD OCCURS
DURING A TRACE RECORD THE COMPLETE STATION IS LOST. FROM
EXPERIENCE, A BLANK RECORD WILL GENERALLY HAVE TWO CHARACTERS.
AFTER THE FIRST PROGRAM RUN AND A DETERMINATION OF BLANK OR
BAD RECORDS HAS BEEN MADE, THESE MAY BE SKIPPED INDIVIDUALLY VIA
NRCSKP ROUTINE.
IF (NRCSKP(1).EQ.0) GO TO 320

1580
1585
1590
1595

***** START INDIVIDUAL RECORD SKIP LOOP *****


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1600 DO 270 LB=1,99
1605 NRC = NRCSKP(LB)-NSKP
1610 IF (NRC.EQ.1) GO TO 280
1615 270 CONTINUE
1620
1625 GO TO 300
1630 280 IPS = -8000
1635 290 FORMAT (//5X,'LABEL 290. RECORD NO.',15,' SKIPPED VIA NRCSKP SKIP
1640 1 ROUTINE.//')
1645 WRITE (6,290) IT
1650 CHANGING IPS TO NEGATIVE CAUSES TPRD TO SKIP A RECORD
1655 IF (ICODE.EQ.0) GO TO 320
1660 WRITE (6,310) IDEPTH,ICODE,ISCL
1665 310 FORMAT (5X,'SALINITY VERSUS DEPTH',/
1670 1 5X,'STD RECORD STARTS AT ',13,' METERS',/
1675 2 5X,'CODE = ',12,/
1680 3 5X,'SCALE = ',12//)
1685
1690 ***** READ TAPE *****
1695 *****
1700 320 CALL TPRD (A,IPS,&350,&330)
1705 *****
1710 IPS IS THE MAXIMUM NUMBER OF BYTES OF DATA WHICH WILL BE READ
1715 FROM ONE RECORD OF DIGITIZER TAPE BY TPRD. IPS/2 IS THE MAXIMUM
1720 TOTAL TRAVEL ALONG THE CURVE MEASURED IN 0.01 INCHES IN THE X
1725 AND Y DIRECTION SEPARATELY. 350 IS THE END OF FILE EXIT, AND 330
1726 IS THE READ-ERROR EXIT.
1730 GO TO 360
1735 330 WRITE (6,340) A(1),A(2),A(3),A(4)
1740 340 FORMAT (5X,'110 ERROR STATISTICS TABLE IS ',428)
1745
1750 350 CONTINUE
1755 360 CONTINUE
1760
1765 ***** END INDIVIDUAL RECORD SKIP LOOP *****
1770 *****
1775 PROCESS THE LAST RECORD
1780 MOVE THE BYTES OF A INTO THE 4-BYTE WORDS OF B USING CHMOVE.
1785 JJ = 0
1790 JJJ = 0
1795
1800 DO 370 II=1,2000
1805
1810
1815 DO 370 I=1,4
1820 JJ = JJ+1
1825
1830

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C      CALL CHMOVE (A(II),I,B(JJ),4)
C      IF (B(JJ).EQ.DLR) GO TO 380
C      END OF DATA DETECTED
C      THERE MAY BE A STAR BEFORE THE DOLLAR
C      CONTINUE
C
C      370 CONTINUE
C
C      380 CONTINUE
C      B(8001) = DLR
C
C      ***** PREPARE TO PROCESS RAW ARRAY *****
C      *****
C      WRITE (6,390) JJ,(B(JJ),J=1,25)
C      FORMAT (/5X,'LABEL 390. ARRAY B IS FILLED; LOOK FOR MODE CHARACTE
C      1R. THE NUMBER OF ARRAY ELEMENTS PROCESSED INCLUDING STARS AND ,/
C      2 5X,'DOLLARS. JJ=' ,I5,/5X,'FIRST 25 CHAKACTERS ARE: ',
C      3 10(1X,Z8)/5X,10(1X,Z8)/5X,5(1X,Z8)/)
C
C      ***** START MISSING IRG ROUTINE *****
C      *****
C      JJ = I
C      GO TO 430
C
C      ***** START MISSING IRG ROUTINE *****
C      *****
C      THE FOLLOWING ROUTINE READS ANOTHER SET OF CARDS. THIS IS THE
C      ENTRY FOR THE SITUATIONS IN WHICH THE IRG IS MISSED.
C      400 READ (5,170) LABEL,JSKIP,ISTOP,AMONC
C      IF (ISTOP.GT.0) GO TO 1580
C      IF (JSKIP.EQ.0) GO TO 410
C      READ (5,DAT)
C      WRITE (6,180) LABEL
C      WRITE (6,DAT)
C      READ (5,CNTRL)
C      WRITE (6,CNTRL)
C
C      -----
C      410 IPPLACE=410
C      WRITE (6,210) (D(J),J=1,1801,20)
C      WRITE (6,210) (T(J),J=1,1801,20),IPPLACE
C      WRITE (6,210) (S(J),J=1,1801,20),IPPLACE
C      WRITE (6,220) (INSA(J),J=1,10)
C      WRITE (6,230) (INTA(J),J=1,10)
C      WRITE (6,240) KS,KSL,KS2,KT,KT1,KT2,JJJ,NE,KDTH1,KDTH2,KDTA,KDT1,J
C      1 JJJ
C      WRITE (6,420) NOIRG,JJJJ
C      420 FORMAT (/5X,'LABEL 410. PROCESSING SECOND HALF. NOIRG=',I3,

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2295 JJ = JJ+1.EQ.KEY) GO TO 490
2305 IF (B(JJ+1).EQ.KEY) GO TO 490
2310 IF (B(JJ).EQ.KEY) GO TO 490
2315 JJ = JJ+1
2320 IF (B(JJ+1).EQ.KEY) GO TO 490
2330 IF (B(JJ).EQ.KEY) GO TO 490
2335 JJ = JJ-1
2340 IF (KL.EQ.1) GO TO 500
2345 IF (KL.EQ.2) GO TO 500
2350 NO KEYBOARD SYMBOL: MAY HAVE FORGOTTEN IT. TEST THE 5TH AND
2355 6TH SYMBOLS (IDEPTH). IF BOTH ARE NINES CALL IT A KEYBOARD.
2360 IF (B(5).EQ.NINE.AND.B(6).EQ.NINE) GO TO 450
2370 GO TO 670
2375 IJJ = JJ+12
2380 WRITE (6,460) (B(I),I=JJ,IJJ)
2385 FORMAT (75X,'AT 450, MISSING KEY. B(1) TO B(13)=' ,13A1/)
2390 GO TO 500
2395
2400 450 WRITE (6,460) (B(I),I=JJ,IJJ)
2405 FORMAT (75X,'AT 450, MISSING KEY. B(1) TO B(13)=' ,13A1/)
2410 GO TO 500
2415
2420 470 WRITE (6,480)
2425 FORMAT (5X,'FOUND EIGHT KEYBOARD SYMBOLS IN SEQUENCE. STOP.')
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```

KY1 = J
KY2 = KY1+2
KY3 = KY1+3
KY4 = KY1+4
KY5 = KY1+5
KY6 = KY1+6
KY7 = KY1+7
KY8 = KY1+8
KY9 = KY1+9
KY10 = KY1+10
KY11 = KY1+11

DLTREC ARE FOUND HERE IN THE HEADER. IF DLTREC OCCURS , READ IN
A NEW RECORD AND USE SAME CARDS.

DO 510 J=KY1,KY10
IF (B(J).EQ.DLTREC) GO TO 520
510 CONTINUE

GO TO 550
520 WRITE (6,530)
530 FORMAT (/5X,'DLTREC IN HEADER. REPEAT,USING SAME CARDS.'/)
540 IT = IT+1
GO TO 200
550 KT2 = 10
KS2 = 10
THESE TWO STATEMENTS GIVE MAXIMUM VALUES TO KT2 AND KS2 SO THAT
THEY WILL ALWAYS BE DEFINED, EVEN IF ONLY ONE VARIABLE IS TRACED

DO THE CONVERSION, COMPARE WITH VALUES READ FROM THE CARDS, ACCEPT
THE CARDS.

DO 560 J=KY1,KY2
B(J) = B(J)-ZER
IB = B(J)
ISTAA = ISTAA+IB*10**(KY2-J)
560 CONTINUE

AMONT = B(KY3)

DO 570 J=KY4,KY5
B(J) = B(J)-ZER
IB = B(J)
IDEPT = IDEPT+IB*10**(J-KY4)

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3010 GO TO 1550
3015 *****
3020 ***** END KEYBOARD DECODE *****
3025 *****
3030 *****
3035 *****
3040 *****
3045 *****
3050 *****
3055 *****
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3065 *****
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3205 *****
3210 *****
3215 *****
3220 *****
3225 *****
3230 *****
3235 *****
3240 *****
3245 *****

*****
***** END KEYBOARD DECODE *****
*****
***** START OF NORMAL TRACE PROCESSING *****
*****

THE FOLLOWING PROCEDURE PERMITS THE PRESENCE OF ANY REASONABLE
NUMBER OF TRACER SYMBOLS (STAR) INCLUDING NONE.
NE = 0
NF = 0
670 IF (B(JJ).EQ.STAR) GO TO 700

COUNT STARS AND WRITE MESSAGE
680 WRITE (6,690) NSTAR
690 FORMAT (/5X,'START TRACER MODE; NO. OF TRACER SYMBOLS =',I2/)
    WHEN THERE ARE NO MORE STARS, START TESTING FOR COUNT SYMBOLS ETC
    GO TO 710
700 JJ = JJ+1
    NSTAR = NSTAR+1
    WE CONTINUE TO TEST FOR STARS UNTIL NO MORE APPEAR.
    GO TO 680

THE NEXT BLOCK OF OPERATIONS TO STATEMENT NO. 950 LOOPS BACK TO
710 CONTINUALLY, TESTING EACH CHARACTER FOR IDENTITY AND X COUNTS
CONTINUING TO ADD OR SUBTRACT FROM THE CUMULATIVE Y AND X COUNTS
UNTIL A DELETE-RECORD SYMBOL OR A STAR OR A DOLLAR INDICATES
THE END OF DATA. THE FLAG IS PLACED AT THE POINT WHERE THE TRACE
ENTERS THE CROSS-SECTIONED AREA; PREVIOUS COUNTS RESULT FROM THE
TRACER TRAVELLING FROM THE COORDINATE ZERO TO THIS POINT.
710 IF (B(JJ).EQ.ONE) GO TO 730
    IF (B(JJ).EQ.BLANK) GO TO 740
    IF (B(JJ).EQ.MINUS) GO TO 750
    IF (B(JJ).EQ.FLAG) GO TO 900
    THE NEXT GROUP OF STATEMENTS ALLOW FOR OCCASIONAL COUNTS GREATER
    THAN + OR -1
    IF (B(JJ).EQ.TWO) GO TO 760
    IF (B(JJ).EQ.THREE) GO TO 770
    IF (B(JJ).EQ.FOUR) GO TO 780
    IF (B(JJ).EQ.FIVE) GO TO 790
    IF (B(JJ).EQ.SIX) GO TO 800
    IF (B(JJ).EQ.SEVEN) GO TO 810
    IF (B(JJ).EQ.EIGHT) GO TO 820
    IF (B(JJ).EQ.NINE) GO TO 830
    IF (B(JJ).EQ.TEN) GO TO 840
    IF (B(JJ).EQ.ELEVEN) GO TO 850

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IF (B(JJ).EQ.MTWO) GO TO 860
IF (B(JJ).EQ.MTHREE) GO TO 870
IF (B(JJ).EQ.MFOUR) GO TO 880
IF (B(JJ).EQ.MFIVE) GO TO 890
IF (B(JJ).EQ.DLTREC) GO TO 970
IF (B(JJ).EQ.KEY) GO TO 440
IF (B(JJ).EQ.X) GO TO 1570
720  FORMAT ('/75X','SYMBOL NOT RECOGNIZED = ',Z8//)
      IF SYMBOL IS NOT RECOGNIZED, STATION DATA IS NOT PRINTED IF IP=1.
      PROGRAM BRANCHES AND RE-INITIALIZES ALL VARIABLES FOR PROCESSING
      NEXT STATION IF IP=1. OTHERWISE, IT RETURNS TO READ NEXT RECORD.
      IF (IP.EQ.1) GO TO 1510
      GO TO 1570
730  RX = 1.
740  GU TO 910
750  RX = 0.
760  RX = -1.
770  RX = 2.
780  RX = 3.
790  RX = 4.
800  RX = 5.
810  RX = 6.
820  RX = 7.
830  RX = 8.
840  RX = 9.
850  RX = 10.
860  RX = 11.
870  RX = -2.
880  RX = -3.
890  RX = -4.
900  JJ = NE

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C
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C


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3490 JJ = JJ+1
3495 FG = 1
3500 GO TO 710
3505
3510 PROGRAM ADDS AND STORES CUMULATIVE SUMS. ONE UNIT EQUALS 0.01
3515 INCH.
3520 N = N+1
3525 NE = N/2
3530 IF (NF.EQ.N) GO TO 920
3535 THIS FIDDLING AROUND DETERMINES IF THE COUNT IS EVEN OR ODD.
3540 START COUNTING IN THE ORDER YXX. X AND Y HAVE NORMAL INVERTED
3545 ORIENTATIONS ON THE STRIP CHART. HOWEVER, X AND Y ARE INVERTED
3550 WITH RESPECT TO THE CALMA DIGITIZER. SPECIFICALLY, DEPTH
3555 INCREASES ALONG THE POSITIVE X-AXIS AND TEMP AND SALINITY ARE
3560 INCREASING FUNCTIONS ALONG THE Y-AXIS ON THE CALMA DIGITIZER.
3565 WARNING: DIGITIZE TRACES ACCORDING TO ABOVE ORIENTATION OR BE
3570 PREPARED TO RE-DIGITIZE TAPE LATER AFTER DISCOVERING GOOF.
3575
3580 IF ODD
3585 SUMD = SUMD+RX
3590 ODD INDEX IS INCREASED TO KEEP IT SAME AS EVEN.
3595 NE = NE+1
3600 Y(NE) = SUMD
3605 JJ = JJ+1
3610 GO TO 930
3615 IF EVEN
3620 SUMT = SUMT+RX
3625 X(NE) = SUMT
3630 JJ = JJ+1
3635 IF STAR OR DOLLAR FOUND, END OF DATA HAS BEEN REACHED.
3640 IF (B(JJ).EQ.DLR) GO TO 990
3645 IF (B(JJ).EQ.DLR) GO TO 990
3650 ***** END OF NORMAL TRACE PROCESSING *****
3655 *****
3660 ***** BEGIN TROUBLE-SHOOTING *****
3665 ***** IF THERE IS NO IRG AT END OF HEADER BUT THERE IS A TRACER SYMBOL,
3670 ***** THE PROGRAM SEPARATES THE TWO RECORDS BY FIRST SETTING NDIRG=1
3675 ***** AND PROCESSING FIRST PART OF B-ARRAY AND THEN READING A NEW SET
3680 ***** OF CARDS TO PROCESS SECOND PART OF B-ARRAY.
3685 ***** IF (B(JJ).NE.STAR) GO TO 950
3690 ***** NDIRG = 1
3695 ***** SAVE THE INDEX OF THE START OF THE SECOND HALF, JJJ.
3700 JJJ = JJ
3705 WRITE (9,940)
3710 FORMAT (1/5X,'FOUND A STAR AT END OF TRACER ASSUME THERE IS NO IRG.
3715
3720
3725

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1, /5X, 'PROCESS RECORD IN TWO PARTS, READING CARDS FOR BOTH PARTS.' /
2)
GO TO 990
950 IF (B(JJ).NE.KEY) GO TO 710
JJJJ = JJ
WRITE (6, 960)
960 FORMAT ( /5X, 'FOUND A KEYBOARD SYMBOL. PROCESS NEXT PORTION OF B-A
ARRAY AFTER READING NEW CARDS.' / )
NOIRG = 1
GO TO 990
C
970 WRITE (6, 980) JJ
980 FORMAT (5X, 'FOUND DELETE RECORD SYMBOL AT JJ= ', I5)
IF DELETE RECORD FOUND, PROGRAM INCREMENTS RECORD COUNT, IT,
AND RESTARTS PROCESSING BUT DOES NOT READ A NEW PAIR OF CARDS.
GO TO 540
990 JJ = JJ-1
C
***** END TRACER AND ASSOCIATED TROUBLE-SHOOTING *****
*****
UP TO THIS POINT, PROCESSING IS IDENTICAL FOR S AND T.
START CONVERTING T AND D TO SCIENTIFIC UNITS
WRITE (6, 1000) JJJ, NE, Y(NE), X(NE)
1000 FORMAT ( /5X, 'LABEL 1000. START CONDENSING UNCONVERTED ARRAY AND CO
INVERTING TO SCIENTIFIC UNITS. /5X, 'THE TRACER ENTERED THE FRAME (F
2LAG) AT JJJ= ', I5 /5X, 'THE END OF THE TRACE HAS INDEX NE= ', I5 /
3 5X, 'LAST (UNCONVERTED) DEPTH AND TEMP ARE: ', F7.1, 2X, F7.1 / )
C
CHECK TO SEE IF FLAG WAS FOUND.
IF (FG.EQ.1) GO TO 1020
WRITE (6, 1010)
1010 FORMAT ( /5X, 'NO FLAG FOUND; PROCESS ANYWAY.' / )
1020 WRITE (6, 1030)
1030 FORMAT ( ' ', )
FG = 0
C
THE X AND Y ARRAYS ARE FILLED AND THE START AND END OF THIS BATCH
OF DATA ARE LABELLED WITH JJJ AND NE.
CONVERT THE ARRAYS INDEXED ON 0.01-INCH DEPTH SPACINGS.
SUBROUTINE CONDENSES THIS PURPOSE ALTHOUGH IT NO LONGER
CONDENSES A SECOND ARRAY TO SMALLER SIZE, NOR DOES IT PAD THE
GAP BETWEEN ARRAYS, BUT WITHIN ONE SEGMENT, IT DOES INTERPOLATE
TO FILL ANY BLANK ARRAY POSITIONS.
C
TO THOSE FAMILIAR WITH EARLIER VERSIONS OF THIS PROGRAM, THE

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3965 FOLLOWING CONDENSE ROUTINES WILL NOT EVEN APPEAR REMOTELY
3970 SIMILAR. THE EARLIER VERSION HAD TO BE EXTENSIVELY MODIFIED
3975 TO PERMIT MULTIPLE DEPTH SCALES. SPECIFICALLY, WHEN USING
3980 MULTIPLE DEPTH SCALES ONE'S DEPTH AXIS REFERENCE CHANGES AND
3985 CONSEQUENTLY IN CONSTRUCTING THE S AND D OR T AND D ARRAYS
3990 THIS ROUTINE WORKS WELL.
3995 IF (ICODE.EQ.0) GO TO 1080
4000 *
4005 S*****S
4010 CONDENSE THE X AND Y ARRAYS INTO S AND D *****S
4015 S*****S
4020 *
4025 KS = KS+2
4030 KS1 = KS-1
4035 KS2 = KS+1
4040 IF (IDSCL.EQ.1) GO TO 1040
4045 KDT1 = KSCARF+1
4050 GO TO 1050
4055 1040 KDT1 = INSA(KS1)
1050 CALL CONDNS (X,Y,S1,JJJ,NE,KDT1,KDTH1,KDTH2)
4060 KDTA = KDT1+1
4065 K = KDTH1
4070 IF (IDSCL.EQ.1) GO TO 1060
4075 K = KDT1
4080
4085
4090
4095
4100 DO 1070 J=KDTH1,KDTH2
4105 D(K) = (J-1)/DCON(IDSCL)+CORD
4110 S(K) = S1(J)/SCON+CORRS(IDSCL)+SCOR
4115 K = K+1
4120 KSCARF = K
4125
4130
4135
4140
4145 INSA(KS) = KDTH1
4150 INSA(KS2) = KDTH2
4155 GO TO 1130
4160 *
4165 T*****T
4170 CONDENSE THE X AND Y ARRAYS INTO T AND D *****T
4175 T*****T
4180 *
4185
4190
4195
4200

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1090 KDT1 = INTA(KT1)
1100 CALL CONDNS (X,Y,T1,JJJ,NE,KDT1,KOTH1,KOTH2)
      KDTA = KOTH1+1
      K = KOTH1
      IF (IDSCL.EQ.1) GO TO 1110
      K = KDT1
C
1110 DO 1120 J=KOTH1,KOTH2
      D(K) = (J-1)/DCON(IDSCL)+CORD
      T(K) = T1(J)/ICON+CURRT(ITSCL)+ICOR
      K = K+1
      KBARF = K
1120 CONTINUE
C
      INTA(KT) = KOTH1
      INTA(KT2) = KOTH2
C
      *
      T
1130 CONTINUE

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*****
***** HAND-ENTERED DATA *****
*****

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CONVERSION OF X AND Y ARRAYS INTO T AND S ARRAYS IS COMPLETE.
AT THIS POINT, SURFACE AND NEAR-SURFACE DATA WILL BE INSERTED.
NORMALLY, ONLY SURFACE VALUES NEED TO BE INSERTED DUE TO THE
DIGITIZER OPERATOR BEGINNING TO TRACE SLIGHTLY BELOW HIS ZERO
DEPTH REFERENCE POINT. SURFACE DATA VALUES ARE INSERTED BY
CHECKING THE VALUE OF IH. IF IH=0, DATA IS NOT INSERTED. IF IH=1,
SURFACE DEPTH, TEMP, AND SALINITY VALUES ARE INSERTED VIA &DAT
DATA CARD FOR PARTICULAR STATION.
CAUTION: HAND-ENTERED DATA VALUES SHOULD BE CORRECTED VALUES
IF CORRECTLY, DATA VALUES BELOW THE SURFACE DOWN TO APPROXIMATELY
PROVISION IS MADE FOR NEAR-SURFACE DEPTHS AS ABOVE. A NOT
15 METERS. THIS OCCURS DUE TO THE SAME REASON AS ABOVE.
SUMMATION OF THIS OCCURS SINCE SELEDOOM, AND INVOLVES A SIGNIFICANT
POINT. OF LABOR TO MANUALLY READ THE STD TRACE, CORRECTION WILL
VALUES IF NEEDED AND PLACED ON &DAT CARD, THIS OPERATION WILL
ONLY BE DONE FOR FINAL OUTPUT TO TAPE, CARD OR PRINTER.
CONSEQUENTLY, TO INSERT NEAR-SURFACE DATA ISQZ MUST EQUAL 1,
IH MUST BE GREATER THAN OR EQUAL TO 2. DH, TH, AND SH WERE
DIMENSIONED AT 50. THIS EQUATES TO APPROXIMATELY 15 METERS.
ISQZ=1 WAS CHOSEN AS DETERMINING VALUE DUE TO ALL ELEMENTS OF D,T,
AND S ARRAYS ARE PRINTED OUT VIA OUT1. THIS ELIMINATES

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C      'GUESSWORK' OF WHICH VALUES SHOULD BE INSERTED. IN OTHER WORDS,
C      ALL OF THEM ARE INSERTED.
C      IF (IH.EQ.0) GO TO 1150
C      S(1) = SH(1)
C      T(1) = TH(1)
C      IF (IH.LT.2) GO TO 1150
C      IF (ISQZ.GT.1) GO TO 1150
C
C      DO 1140 J=2, IH
C      S(J) = SH(J)
C      T(J) = TH(J)
C      D(J) = DH(J)
C      1140 CONTINUE
C
C      1150 CONTINUE
C      *
C      -----
C      IPLACE=1155
C      WRITE (6,210) (D(J),J=1,1801,20)
C      WRITE (6,210) (T(J),J=1,1801,20), IPLACE
C      WRITE (6,210) (S(J),J=1,1801,20), IPLACE
C      WRITE (6,220) (INSA(J),J=1,10)
C      WRITE (6,230) (INTA(J),J=1,10)
C      WRITE (6,240) (KS,KSI,KS2,KI,KT1,KT2,JJJ,NE,KDTH1,KDTH2,KDTA,KDTL,J
C      1JJJ
C      -----
C
C      IF (IP.EQ.1) GO TO 1160
C      IF (NOIRG.EQ.1) GO TO 400
C      GO TO 1570
C      1160 IN1 = KBARF
C      IN2 = KSCARF
C      KDTA = MINO(IN1,IN2)
C      1170 FORMAT (5X,'LABEL=1170.',3I7//)
C      WRITE (6,1170) IN1,IN2,KDTA
C      ***** EDITING OF UNWANTED ZERO DATA VALUES *****
C      *****
C      IN DIGITIZING TEMP AND SALINITY SEGMENTS OF TRACES ONE CAN NOT
C      AVOID GETTING GAPS SOMETIMES BETWEEN TRACE SEGMENTS. WHEN THIS
C      HAPPENS THE OUTPUT PRINTOUT WILL SHOW -5.0 AND 0.0 FOR THE
C      TEMPERATURE AND SALINITY VALUES RESPECTIVELY. THESE VALUES ARE
C      THE PRE-INITIALIZED VALUES OF THE T AND S ARRAYS, AND INDICATE
C      NO ATTEMPT HAS BEEN MADE TO PLACE DATA IN THE PARTICULAR ARRAY
C      POSITION (IE A GAP IN DATA). IT IS DESIRABLE THAT THESE UNWANTED
C      VALUES OR GAPS BE ELIMINATED PRIOR TO WRITING A TAPE OR PUNCHING

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C      A CARD.  THUS A CHECK IS MADE TO SEE IF T(J) OR S(J) ARE -5.0 OR
C      0.0 RESPECTIVELY.  IF T(J) AND S(J) ARE NOT -5.0 OR 0.0
C      RESPECTIVELY, THE VALUES ALONG WITH DEPTH ARE PLACED INTO D2,T2,
C      AND S2 ARRAYS.  IF GAPS DO EXIST, THE VALUES ARE WRITTEN OUT AND
C      COUNTED BUT NOT PUT INTO THE D2,T2, AND S2 ARRAYS.  THIS PROCESS
C      IN EFFECT DISCARDS THE GAPS IN THE DATA, T, AND S ARRAYS
C      ARE THEN RE-INITIALIZED, AND THE D2,T2, AND S2 ARRAYS ARE PUT BACK
C      INTO THE D,T, AND S ARRAYS.  NOTE, THE VALUE OF KDTA WHICH OF
C      IS EQUAL TO TOTAL NUMBER OF RECORDS IS REDUCED BY NUMBER OF
C      UNWANTED RECORDS BY MAKING USE OF THE VARIABLE KDTAF.
C      K = 0
C      L = 1
C
C      DO 1200 J=1,KDTA
C      IF ((T(J).EQ.-5.0).OR.(S(J).EQ.0.0)) GO TO 1180
C      D2(L) = D(J)
C      T2(L) = T(J)
C      S2(L) = S(J)
C      L=L+1
C      GO TO 1200
1180 K = K+1
C      D(J),T(J),S(J),J
C      JSAV = K
1190 FORMAT (//5X,3F7.2,I6,/)
1200 CONTINUE
C
C      FORMAT (//5X,' JSAV=',I6,/)
C      WRITE (6,1210) JSAV
C      KDTAF = KDTA-JSAV
C      KDTA = KDTAF
C
C      DO 1220 J=1,1801
C      D(J) = 0.0
C      T(J) = -5.0
C      S(J) = 0.0
1220 CONTINUE
C
C      DO 1230 J=1,KDTA
C      D(J) = D2(J)
C      T(J) = T2(J)
C      S(J) = S2(J)
1230 CONTINUE

```



```

1 1X,'DEG.C.',1X,'PPT.',4X,'M/SEC',10X,/)
  WRITE (7,1380)
  ICS2 = ICSQZ#2
  J = 1
  KK = 1
  KK = 1
  1400 FORMAT (1X,3F7.2,F8.3,3X,3F7.2,F9.2,F8.3)
  WRITE (7,1400) D(K1),T(K1),S(K1),SV(K1),SIG(K1),D(KK),T(KK),S(KK),
    1SV(KK),SIG(KK)
  J = 3
  1410 IF (J.GI.NCRDS) GO TO 1420
  K1 = (J-1)*ICS2
  KK = K1+ICSQZ
  WRITE (7,1400) D(K1),T(K1),S(K1),SV(K1),SIG(K1),D(KK),T(KK),S(KK),
    1SV(KK),SIG(KK)
  J = J+1
  GO TO 1410
  1420 IF (IDIF.EQ.0) GO TO 1430
  K1 = KDTA
  WRITE (7,1400) D(K1),T(K1),S(K1),SV(K1),SIG(K1)
  C
  C
  C
  C ***** HYDROGRAPHIC PROGRAM CARD PUNCH *****
  C
  1430 IF (.NOT.GCARDS) GO TO 1500
  GCRD = KDTA/IGSQZ
  WRITE (7,1350)
  1440 FORMAT (1X,14,' VALUES OF D , T , AND S FOR STATION ',I4,A12,
    1', COMPRESSED BY ',I3,/)
  WRITE (7,1440) GCRD,ISTA,WMONTH,IGSQZ
  1450 FORMAT (2X,'DEPTH',7X,'TEMP.',4X,'SALINITY',15X,'STATION',4X,'DATE
    1',5X,'VALUE',9X)
  1460 FORMAT (2X,'METERS',6X,'DEG.C.',5X,'PPT.',51X,/)
  WRITE (7,1450)
  WRITE (7,1460)
  J = 1
  K1 = 1
  1470 FORMAT (1X,F7.1,2X,F9.2,1X,F10.3,18X,I3,A12,' K1=',I4,I8)
  WRITE (7,1470) D(K1),T(K1),S(K1),ISTA,WMONTH,K1,J
  J = 2
  1480 K1 = (J-1)*IGSQZ
  GO TO 1490
  WRITE (7,1470) D(K1),T(K1),S(K1),ISTA,WMONTH,K1,J
  J = J+1
  IF (J.GE.500) GO TO 1500
  GO TO 1480
  1490 K1 = KDTA

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5625 WRITE (7,1470) D(K1),T(K1),S(K1),ISTA,WMONTH,K1,J
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*****
JREC IS INCREMENTED HERE BY 1 TO ACCOUNT FOR TAPE ID LABEL FOR
NEXT STATION TO BE PROCESSED. THIS KEEPS SERIALIZATION OF
RECORDS ON TAPE CONSECUTIVE AND INCLUDES LABELS FOR EACH STATION.
1500 JREC = JREC+1 *****
*****
1510 IF (ENDFL) END FILE 8
      NORMALLY, ENDFL MUST BE TRUE ONCE ON THE LAST TAPE WRITING
      OPERATION. HOWEVER, IT IS NOT REQUIRED BY IBM. IT IS WRITTEN
      ALWAYS AFTER LAST TAPE WRITING OPERATION WITHOUT COMMAND.
*****
***** INITIALIZE VARIABLES AND ARRAYS FOR NEXT STATION *****
DO 1520 J=1,1801
D(J) = 0.0
T(J) = -5.0
S(J) = 0.0
D2(J) = 0.0
T2(J) = -5.0
S2(J) = 0.0
T1(J) = -5.0
S1(J) = 0.0
IREC(J) = 0
1520 CONTINUE
*****
INSA(1) = 1
INSA(2) = 1
INTA(1) = 1
INTA(2) = 1
KBARF = 0
KSCARF = 0
DO 1530 J=3,10
INSA(J) = 980
INTA(J) = 980
1530 CONTINUE
*****

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```

C      KS = 1
C      KT = 1

      DO 1540 J=1,50
      SH(J) = 0.0
      TH(J) = -5.0
      DH(J) = 0.0
1540 CONTINUE
C
      SKIP = .FALSE.
      JSAY = 0
      KDTAF = 1
      IDEPTH = 0
      IH = 0
      IF (NOIRG.EQ.1) GO TO 400
      GO TO 1570
      ***** RETURN *****
C
1550 CONTINUE
1560 FGRMAT('1')
1570 IT = IT+1
1580 STOP
      END

```



```

C -----SUBROUTINE OUT1 MOD1,JUNE 1975-----
SUBROUTINE OUT1 (D,T,S,SV,SIG,N,ISTA,WMONTH,IREC,JREC,ISQZ)
REAL #8WMONTH
DIMENSION D(1), T(1), S(1), SV(1), SIG(1), IREC(1)
PRODUCE HEADING
20 WRITE (6,30) ISTA,WMONTH,ISQZ
30 FORMAT (//T38,'OCEANOGRAPHIC DATA FROM U C M II'//T41,'STATION ',
1 I3,A12/T41,'COMPRESSED BY FACTOR ',I3//)
FORMAT FOR PRINTING TWO BLOCKS OF DATA PER PAGE.
WRITE (6,40)
40 FORMAT (I6,'DEPTH',T14,'TEMP.',T20,'SALNTY.',T28,'SND.VEL.',T36,'
1 SIGMA-T',T48,'DEPTH',T56,'TEMP.',T62,'SALNTY.',T70,'SND.VEL.',
2 T80,'SIGMA-T')
WRITE (6,50)
50 FORMAT (I6,'METERS',T14,'DEG.C.',T21,'PPT.',T29,'M/SEC',T48,'
1 'METERS',T56,'DEG.C.',T63,'PPT.',T71,'M/SEC')
NN = N/2
NO = N-2*NN

C
C DO 60 J=1,NN,ISQZ
K = NN+J
WRITE (6,70) D(J),T(J),S(J),SV(J),SIG(J),D(K),T(K),S(K),SV(K),SIG(
1K),IREC(J),IREC(K)
60 CONTINUE

C
C 70 FORMAT (I6,F5.1,T14,F5.2,T21,F5.2,T28,F7.2,T39,F6.3,T48,F5.1,T56,F
15.2,T63,F5.2,T70,F7.2,T81,F6.3,T90,2I8)
IF (NO.EQ.0) GO TO 90
WRITE (6,80) D(N),T(N),S(N),SV(N),SIG(N),IREC(N)
80 FORMAT (I48,F5.1,T56,F5.2,T63,F5.2,T70,F7.2,T81,F6.3,T90,8X,I8)
90 WRITE (6,100)
100 FORMAT ('1')
RETURN
END

```


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----- SUBROUTINE CHMOVE -----
SUBROUTINE CHMOVE (A,I,B,J)
THIS SUBROUTINE RETURNS A LOGICAL#1 VARIABLE TO A 4-BYTE ADDRESS
IN THE MAIN PROGRAM, UNPACKING THE ORIGINAL 4-BYTE WORDS A
BYTE AT A TIME.
LOGICAL *1A(1),B(1)
B(J) = A(I)
RETURN
END

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C
C
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C


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----- SUBROUTINE CONDNS -----
SUBROUTINE CONDNS (X,Y,T1,JJJ,NE,KDTH1,KDTH2)
SUBROUTINE CONDNS MOD. 3,17 SEPT 74 BY R. G. PAQUETTE.
THIS SUBROUTINE FINDS THE ARRAY LOCATIONS FOR X, INDEXED
SEQUENTIALLY FOR EACH UNIT OF Y. EACH UNIT OF Y IS 1.0 AND
CORRESPONDS TO .01 INCHES OF TRAVEL IN THE DEPTH DIRECTION.
MOD. 3 FILLS IN BLANK ARRAY POSITIONS DUE TO THE DIGITIZER STEPP-
ING AHEAD MORE THAN .01 INCHES AT A STEP AND WRITES A MESSAGE
CN THE PRINTER.
DIMENSION X(1), Y(1), T1(1), KINS(10), KNO(10)
IF FIRST INDEX IS ZERO OR NEGATIVE THERE IS A MISBEHAVIOR ELSE-
WHERE IN THE PROGRAM. RESET JJJ TO 1.
IF (JJJ.GE.1) GO TO 30
JJJ = 1
WRITE (6,20)
FORMAT (/,5X, '***** JJJ RESET TO ONE - SOMETHING WRONG *****')
20 KDTH1 BECOMES THE INDEX OF THE START OF THIS ARRAY SEGMENT.
30 KDTH1 = Y(JJJ)+1.50
IF KDTH1 BECOMES ZERO OR LESS (THE ORIGIN OF MEASUREMENT IS
POSITIVE WITH RESPECT TO THE START OF TRACE), USE THE START
OF THE CURVE AS THE ORIGIN OF INDEXING.
THIS CAUSES AN OVERLAP BETWEEN ARRAYS, BUT IT SHOULD BE SMALL.
XINC = 0.
IF (KDTH1.GT.0) GO TO 40
XINC = FLOAT(1-KDTH1)
KDTH1 = 1
40 JJJ = JJJ+1
NE1 = NE-1
FORM SUBSCRIPTS FROM THE DEPTH INCREMENTS AND STORE X'S AT THOSE
ARRAY LOCATIONS.
SEARCH FOR BLANKS IN ARRAY BETWEEN INDEXES KDTH1 AND KDTH2.
KCT COUNTS THE NUMBER OF BLANKS
KCT = 0
KSAV = KDTH1
KINS(J) IS THE NUMBER OF THE ARRAY POSITION FILLED.
DO 50 J=1,10
KNO(J) = 0
50 KINS(J) = 0

```



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245 DO 80 J=JJ1,NE1
250 KDTH = Y(J)+1.50*XINC
255 T1(KDTH) = X(J)
260 TEST TO SEE IF INDEX IS THE SAME OR ONE GREATER THAN THE LAST
265 ONE. IF NOT, INTERPOLATE VALUES.
270 NREP = KDTH-KSAV
275 IF (NREP.LE.1) GO TO 70
280 KCT = KCT+1
285 IF (KCT.GT.10) KCT = 10
290 KNO(KCT) = NREP
295 KINS(KCT) = KDTH
300 I1 = KSAV+1
305 I11 = KDTH-1
310 E = FLOAT(NREP)
315 G = T1(KDTH)
320 F = G-T1(KSAV)
325
330 DO 60 I=I1,I11
335 T1(I) = (FLOAT(I-KSAV)/E)*F+T1(KSAV)
340
345 60 CONTINUE
350
355 70 KSAV = KDTH
360 80 CONTINUE
365
370 KDTH2 = Y(NE)+1.50*XINC
375 INSERT THE FIRST POINT, WHICH OTHERWISE WOULD BE THE LAST
380 ONE FOR WHICH Y(J).LT.1.
385 T1(KDTH1) = X(JJ)
390 T1(KDTH2) = X(NE)
395 SAVE INDEX OF END OF ARRAY.
400
405 WRITE DOWN NUMBER AND LOCATIONS OF INTERPOLATED VALUES.
410 WRITE (6,90) KCT,(KINS(I),I=1,KCT)
415 FORMAT (/5X,'BLANK ARRAY POSITIONS FILLED IN ',15,' PLACES.
420 BEGIN
425 INDEXING INDEXES AND NO. OF STEPS',5X,'(10 EACH) ARE:',5X,10I6/
430 2
435 RETURN
440 END
445

```


LA	R10,TPDCB	TPR01610
USING	IHADCB,R10	TPR01620
TM	DCBOFLGS,X'10'	TPR01630
BO	OOKK	TPR01640
IM	BAUBOMB,X'AA'	TPR01650
BNO	ONWITHIT	TPR01660
SPACE	2,DUMP	TPR01670
ABEND	2	TPR01680
SPACE	2	TPR01690
OPEN	(TPDCB,INPUT)	TPR01700
TM	DCBOFLGS,X'10'	TPR01710
BNO	KIKIT	TPR01720
L	R9,DCBDEBAD	TPR01730
L	R9,32(R9)	TPR01740
SR	R6,R6	TPR01750
IC	R6,9(R9)	TPR01760
MH	R6,=H'10'	TPR01770
L	R9,16	TPR01780
L	R9,112(R9)	TPR01790
LA	R9,0(R6,R9)	TPR01800
ST	R9,STATTAB	TPR01810
MVC	OLDSTAT,0(R9)	TPR01820
SPACE	2	TPR01830
L	R0,SHOVALN	TPR01840
STH	R0,BYICNT	TPR01850
L	R1,SHOVAAD	TPR01860
ST	R1,TPBUFLOC	TPR01870
MVC	TPBLOC,TPBUFLOC+1	TPR01880
LTR	R0,R0	TPR01890
BP	OOKK	TPR01900
MVI	TPCCW,X'37'	TPR01910
BAL	R9,TPGET	TPR01920
MVI	TPCCW,X'02'	TPR01930
BAL	R9,TPWAIT	TPR01940
B	RETURN	TPR01950
SPACE	2	TPR01960
SPACE	2	TPR01970
BAL	R9,TPGET	TPR01980
SPACE	2	TPR01990
BAL	R9,TPWAIT	TPR02000
LA	R15,0	TPR02010
L	R13,4(R13)	TPR02020
L	R14,12(R13)	TPR02030
LM	R0,R12,20(R13)	TPR02040
BR	R14	TPR02050
SPACE	2	TPR02060
MVI	RETURN+3,X'04'	TPR02070
SPACE	2	TPR02080

KIKIT	HAS DCB BEEN OPENED?	TPR01610
ONWITHIT	HAS THERE BEEN PREVIOUS CATASTROPHE?	TPR01620
	NOPE, GO AND OPEN IT	TPR01630
	NOPE, GO AND OPEN IT	TPR01640
	SHOULDNT EVER GET HERE, CRASH	TPR01650
		TPR01660
		TPR01670
		TPR01680
		TPR01690
		TPR01700
		TPR01710
		TPR01720
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		TPR01740
		TPR01750
		TPR01760
		TPR01770
		TPR01780
		TPR01790
		TPR01800
		TPR01810
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		TPR01990
		TPR02000
		TPR02010
		TPR02020
		TPR02030
		TPR02040
		TPR02050
		TPR02060
		TPR02070
		TPR02080

OUT	CLOSE	TPDCB				TPR02090
	SPACE 2	BADBOMB,X'AA'	TURN ON FLAG			TPR02100
	MVI B	RETURN				TPR02110
	SPACE 2					TPR02120
GETSTAT	LVC	R9,STATTAB	ARRIVE HERE ON BAD READ			TPR02130
	L	NEWSTAT,0(R9)	GET CURRENT STAT TABLE			TPR02140
	L	R9,SHOVAAD	MOVE OLD AND NEW STAT	TABLES TO FTN		TPR02150
	MVC	0(16,R9),OLDSTAT	ARRAY BEFORE ERROR	RETURN		TPR02160
	MVI B	RETURN+3,X'08'	SET I/O ERROR RETURN			TPR02170
	SPACE 2					TPR02180
TPGET	MVI	TPECB,X'00'	CLEAR ECB			TPR02190
	MVC	TPEXCP,TPCCW				TPR02200
	MVI	RDFLG,X'FF'	TURN ON READ FLAG			TPR02210
	EXCP	TPIOB	DO IT			TPR02220
	BR	R9	RETURN			TPR02230
	SPACE 2					TPR02240
TPWAIT	TM	TPECB,X'40'	IS IT ALREADY DONE?			TPR02250
	BU	NOWAIT	YES			TPR02260
	WAIT	ECB=TPECB	NO, WAIT FOR IT			TPR02270
	CLI	TPECB,X'7F'	DID IT DO IT OK?			TPR02280
NOWAIT	BE	OKI	YES, CONTINUE			TPR02290
	SPACE 2					TPR02300
	CLI	TPCSW+3,X'0D'	PROBABLE EOF IF CHAN-DEV END & UNIT EXCPT			TPR02310
	BNE	GETSTAT	NOPE, GO FIND ERROR			TPR02320
	BNE	FLAGS1,X'04'	EXCEPTIONAL CONDIT BIT ON? (=EOF)			TPR02330
	L	GETSTAT	NO EOF			TPR02340
	BCTR	R1,DCBBLKCT	DECREMENT DCBBLKCT SO IT MATCHES TAPE			TPR02350
	ST	R1,0	TRAILER LABELS			TPR02360
	EOV	R1,DCBBLKCT				TPR02370
	SPACE 2	TPDCB	YES, EOF - FORCE CONTROL TO EODAD RTN			TPR02380
OKI	BR	R9	RETURN			TPR02390
	SPACE 2					TPR02400
SAV1	DC	18F'0'				TPR02410
	SPACE 2					TPR02420
OLDSTAT	DC	D'0'	COPY OF STAT TABLE AFTER OPEN			TPR02430
NEWSTAT	DC	D'0'	COPY OF STAT TABLE UPON ERROR			TPR02440
	SPACE 2					TPR02450
TPEXCP	DC	D'0'	LOC CONTAINING CCW BEING USED			TPR02460
TPCCW	DC	X'02'	READ			TPR02470
TPBLOC	DC	AL3(0)	DATA ADDRESS			TPR02480
FLGS	DC	X'20'	SUPPRESS INCORRECT LNLT			TPR02490
BYTCNT	DC	H'0'	BYTE COUNT			TPR02500
	SPACE 2					TPR02510
SHOVSMF	DC	A(0)	LOC OF SMF INFO			TPR02520
SHOVAAD	DC	A(0)	ADDR OF FORTRAN ARRAY			TPR02530
						TPR02540
						TPR02550
						TPR02560

SHOVALN	DC	F'0'	BYTE LENGTH OF FORTRAN ARRAY	TPR02570
TPBUFLOC	SPACE 2	A(0)	LOC OF DCBBLKSI LENGTH TAPE BUFFER	TPR02580
STATTAB	DC	A(0)	LOC OF STAT TABLE	TPR02590
	SPACE 2			TPR02600
	SPACE 2			TPR02610
	SPACE 2			TPR02620
RDFLG	DC	X'00'	=X'FF' AFTER READ, BEFORE WAIT	TPR02630
BADBOMB	DC	X'00'	FLAG TO TELL WHETHER DCB USED BEFORE	TPR02640
	SPACE 2			TPR02650
TPDCB	DCB	DDNAME=METTAP,MACRF=(E),EODAD=IPEOF,DSORG=PS,		TPR02660
	SPACE 2	IOBAD=TPIOB,DEV=TA		*TPR02670
	DS	OF		TPR02680
TPIOB	DS	OCL32		TPR02690
FLAGSI	DC	X'00'		TPR02700
FALGS2	DC	X'00'		TPR02710
SENSEL	DC	X'00'		TPR02720
SENS2	DC	X'00'		TPR02730
ECBCOD	DC	X'00'		TPR02740
ECBADD	DC	AL3(TPECB)		TPR02750
FALGS3	DC	X'00'		TPR02760
TPCSW	DC	7X'00'		TPR02770
SIOCODE	DC	X'00'		TPR02780
EXCPADD	DC	AL3(TPEXCP)		TPR02790
RESERC	DC	X'00'		TPR02800
DCBADDR	DC	AL3(TPDCB)		TPR02810
REPOMOD	DC	X'00'		TPR02820
RESTADR	DC	AL3(0)		TPR02830
BLCINC	DC	H'1'		TPR02840
ERGRCNT	DC	H'0'		TPR02850
	SPACE 2			TPR02860
TPECB	DC	F'0'		TPR02870
	SPACE 2			TPR02880
ARGS	USECT		ADDRESS OF FORTRAN ARRAY	TPR02890
AADD	DC	A(0)	ADDRESS OF LENGTH OF FORTRAN ARRAY	TPR02900
ALADD	DC	A(0)		TPR02910
	SPACE 2			TPR02920
	PRINT	NOGEN		TPR02930
	DCBD	DSORG=PS,DEV=TA		TPR02940
	PRINT	GEN		TPR02950
	SPACE 2			TPR02960
TPRD	CSECT			TPR02970
	LTORG			TPR02980
	END			TPR02990
				TPR03000
				TPR03010

C C C	TITLE	DIGIXBT		5
C C C	PROGRAMERS	R.E.BLUMBERG, R.E. GREER. ADAPTED FROM DIGISTD PROGRAM WHICH WAS AN EXTENSIVE MODIFICATION OF AN ORIGINAL PROGRAM, MIZ2, BY R.G. PAQUETTE.		10
C C C	DOCUMENTATION	R.E.BLUMBERG		15
C C C	DATE	26 JUNE 1975		20
C C C	PURPOSE	PROGRAM READS AND PROCESSES DIGITIZED TEMPERATURE AND DEPTH DATA FROM A CALMA DIGITIZER 7-TRACK TAPE. THE DATA IS COMPUTED AND STORED FOR EVERY 0.01 OF AN INCH OF DEPTH INCREMENT ON THE XBT TRACE. PROGRAM COMPUTES DEPTH AND TEMPERATURE FOR EACH INDIVIDUAL OCEANOGRAPHIC STATION AND PERMITS PRINTED, PUNCHED CARD OR 9-TRACK TAPE OUTPUT. NOTE, THIS PROGRAM IS SET UP TO PROCESS WATER TEMPS BETWEEN 1 AND 25 DEGREES CELSIUS.		25
C C C	SEQUENCE	THE PROGRAM PERFORMS THESE FUNCTIONS IN THE FOLLOWING SEQUENCE: (A) INITIALIZES ALL ARRAYS AND VARIABLES (B) SKIPS XXX NUMBER OF RECORDS IF NSKP>GREATER THAN ZERO. (C) READ PAIR OF DATA CARDS (LABEL AND DAT) FOR RECORD BEING PROCESSED. COUNT RECORDS. (D) PROGRAM TERMINATES IF ISTOP=1 OR DESIRED NUMBER OF RECORDS PROCESSED. (E) HEADER INFO MISSING ON TAPE, INSERT ON CARDS BY SETTING IHDR=1. (F) SKIP UNREADABLE OR BAD RECORD IF NRCSKP SET EQUAL TO THE BAD RECORD NUMBER. (G) READ USABLE RECORD INTO THE A ARRAY (H) MOVE BYTES OF A ARRAY INTO 4-BYTE WORDS OF B ARRAY TO ALLOW PROCESSING BY STANDARD FORTRAN. (I) PROCESS RAW B ARRAY (1) IF HEADER RECORD, PROGRAM DECODES HEADER LABEL AND COMPARES TO LABEL SUPPLIED BY DATA CARD. (2) IF TRACER RECORD, PROGRAM ADDS AND STORES CUMULATIVE SUMS OF X AND Y DISTANCE TRAVEL. SUBROUTINE CONDNS INDEXES THE VALUES OF		30
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C C C				220

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(J) CUMULATIVE DISTANCE BY INCREASING DEPTH UNITS.
(K) CONVERT THE X AND Y ARRAYS TO DEPTH AND TEMPERATURE.
(L) MANUALLY INSERT SURFACE AND NEAR SURFACE VALUES VIA DATA CARDS.
(M) ELIMINATE EXCESSIVELY HIGH OR LOW VALUES.
(N) COMPUTE CONSECUTIVE RECORD SERIALIZATION FOR TAPE OUTPUT NUMBERING SCHEME.
(O) CONVERTS LETTER DESIGNATOR MONTH/YEAR CODE, AMONC, TO REAL*8 MONTH AND YEAR.
(P) DATA OUTPUT IN EITHER REGULAR PRINTOUT, TAPE, OR PUNCHED CARDS. CARD OUTPUT SUITABLE FOR THESIS.
(Q) INITIALIZE ARRAYS AND VARIABLES FOR PROCESSING NEXT STATISTICS DATA.
(R) REPEAT STEPS (C) THRU (P) UNTIL ALL RECORDS ARE PROCESSED, ISTOP=1, OR THE NUMBER OF DESIRED RECORDS (NN) ARE READ.

THIS IS A HIGHLY VERSATILE PROGRAM FOR PROCESSING OF THE OCEANOGRAPHIC DATA FROM 7-TRACK TAPE. FEATURES OF THE PROGRAM ARE LISTED UNDER THE FOLLOWING SIX GENERAL CATEGORIES:

(A) INPUT

(1) 7- TRACK CALMA DIGITIZER TAPE IN BCD. SEGMENT
(2) TWO DATA CARDS REQUIRED PER TRACE. PER
RECORD OR HEADERS LABEL PAIR FOR AN XBT TRACE
REQUIRES 4 CARDS, ONE PAIR FOR THE HEADER AND
ONE PAIR FOR THE TRACE. THE FOLLOWING IS A
SAMPLE DATA DECK SHOWING DATA CARDS FOR STATION
207 AND 208. ALSO SHOWN IS THE STATION END.
CARD WITH I STOP SET EQUALS TO ONE. THIS IS
FOLLOWED BY THE JCL NECESSARY TO READ THE 7-
TRACK TAPE. COLUMN 1 IS BLANK ON THE DATA CARDS.
IDISCL=1, ICODE=0, ITISCL=1, ISCL=1, IP=1, ISQZ=01,
CARDS=F, TCCR=-.13, XBTICOR=0.0, NSKP=6, &END
CONS 201V THRU 317V TAPE UCM011

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&CONTRL NN=104,IDSCL=1,ICODE=0,ITSCL=1,ISCL=1,IP=1,ISQZ=01,
ICSQZ=3,TAPE=F,CARDS=F,TCGR=-.13,XBTCOR=0.0,NSKP=6,&END
UCMXBT STATIONS 201V THRU 317V TAPE UCM011
HEADER XBT
&DAT IDEPTH=99,ISTA=207,AMONC='V',&END
TRACER XBT
&DAT IDEPTH=00,DH=0.0,TH=12.12,IH=1,&END
HEADER XBT
&DAT IDEPTH=99,ISTA=208,AMONC='V',&END
TRACER XBT
&DAT IDEPTH=00,&END
STATION END
//GO.METTAP DD UNIT=2400-1,VOL=SER=UCM011,DISP=OLD,LABEL=(,NL),
//DCB=(DEN=1,TRICH=ET)
// (B) SUBROUTINES

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[illegible]

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- (1) TPRD-READS THE 7-TRACK MAGNETIC TAPE.
- (2) CHMOVE- TAKES THE DATA THAT HAS BEEN READ INTO THE A ARRAY AND STORES IT IN USABLE FORM IN THE B ARRAY.
- (3) CONDENS- INDEXES THE VALUES OF CUMULATIVE DISTANCE BY INCREASING DEPTH UNITS.
- (4) OUT2- PRINTS OUT OCEANOGRAPHIC STATION DATA.
- (C) AUTOMATIC DATA PROCESSING/HANDLING IN TRACING XBT CURVES ON CALMA DIGITIZER.
- (1) HANDLES OPERATOR MISTAKES MADE IN TRACING XBT CURVES ON CALMA DIGITIZER.
- (2) SKIPS INITIAL NUMBER AND INDIVIDUAL BAD RECORDS ON 7-TRACK TAPE.
- (3) DECODES 7-TRACK TAPE HEADER LABELS AND TRACE RECORDS.
- (4) COMPUTES DATA FOR EVERY 0.01 INCH OF CALMA DIGITIZER STYLUS MOVEMENT.
- (5) ALLOWS ENTRY OF HAND ENTERED DATA FOR SURFACE AND NEAR SURFACE VALUES.
- (6) EDITS OUT EXCESSIVELY LOW & HIGH VALUES.
- (7) PROVIDES CONSECUTIVE RECORD SERIALIZATION FOR TAPE OUTPUT.
- (D) DIAGNOSTICS
- (1) WRITES FIRST TWENTY FIVE VALUES OF DEPTH AND TEMPERATURE FOR DATA INSPECTION.
- (E) TROUBLE-SHOOTING
- (1) HANDLES MULTIPLE KEYBOARD AND TRACER SYMBOL ENTRIES.
- (2) PROVIDES FOR A MISSED OR INCOMPLETE HEADER LABEL.
- (3) HANDLES MISSING INTER-RECORD GAP (IRG).
- (4) HANDLES DELETE RECORD BY INCREMENTING RECORD COUNT AND READING SAME PAIR OF CARDS AGAIN.
- (5) COMPARES CARD HEADER LABEL AND TAPE HEADER LABEL AND ACCEPTS CARD VALUES IF CARD AND TAPE DISAGREE.
- (F) OUTPUT
- (1) PRINTER- TWO PRINTING VARIABLES, PRT1 AND PRT2. PRT2 PROVISION ONLY.
- (2) CARD-PUNCHED DATA CARDS SUITABLE FOR USE WITH THE SISI.
- (3) TAPE- 9-TRACK TAPE
- (4) PLOTTING- PROVISION FOR PLOTTING ROUTINES ACTUATED BY PLT1 AND PLT2 ARE NOT PRESENTLY PROGRAMMED.

PROGRAM CONSISTS OF MANY TERMS, ARRAYS, AND VARIABLES.
SOME OF THESE VARIABLES ARE USED IN THE DIGISTD
PROGRAM. THEY WERE INCLUDED IN THIS PROGRAM TO KEEP

ARGUMENTS

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IP = INSERTED ON CARDS. IDENTIFIES LAST RECORD OF
PARTICULAR STATION. SINCE XBT IS A
SINGLE TRACE IP IS A CONSTANT = 1.
ISCL = VARIABLE HELD OVER FROM DIGISTD
PROGRAM ISCL IS A CONSTANT = 1.
ISQZ = VARIABLE USED TO COMPRESS NUMBER
OF DATA POINTS PRINTED BY PRINTER.
ISTA = VARIABLE IDENTIFIES STATION NUMBER.
ISTOP = VARIABLE TERMINATES PROGRAM IF = 1 ON
FINAL & DAT CARD.
ITSCL = VARIABLE HELDOVER FROM DIGISTD PROGRAM
ITSCL IS A CONSTANT = 1.
JREC = VARIABLE USED TO COUNT RECORDS FOR
RECORD SERIALIZATION PURPOSES.
JSKIP = VARIABLE USED TO CONTRL NUMBER OF
DATA CARDS READ.
KEY = KEYBOARD SYMBOL ON THE DIGITIZED TAPE.
KDTHT2 = NUMBER OF RECORD PROCESSED FOR
PARTICULAR STATION.
LABEL = HEADER TYPE STATION CARD WHICH
IDENTIFIES STATION NUMBER, MONTH, ETC.
NCRDS = NUMBER OF CARDS PUNCHED BY CARDS
PUNCHING ROUTINE.
NE = AN INDEX AT THE LAST USEFUL ARRAY
POSITION OF THE X(DEPTH) ARRAY.
NOIRG = VARIABLE USED TO INDICATE MISSING
END OF RECORD GAP ON TAPE.
NPTS = NUMBER OF DATA POINTS TO BE PUNCHED
BY CARDS PUNCHING ROUTINE.
NSKP = NUMBER OF INITIAL RECORDS ON TAPE
TO BE SKIPPED
TCOR = CORRECTION FACTOR ADDED TO
TEMPERATURE DATA VALUES.
WMONTH = REAL*8 - MONTH AND YEAR

TPRD IS IN ASSEMBLER LANGUAGE AND REQUIRES SPECIAL JCL. CARDS ARE
THE COMMENT CARDS ARE INCLUDED HERE BECAUSE NO COMMENT CARDS ARE
ALLOWED TO BE MIXED WITH THE ASSEMBLER LANGUAGE SUBROUTINE.
A /* FOLLOWED BY A // ASM.SYSIN DD * MUST PRECEDE THE DECK.
THIS DECK IS RUN UNDER // EXEC FORTCALG.
TPRD IS A MODIFIED VERSION OF TAPRD, WHICH ALLOWS THE USER TO
READ MAGNETIC TAPE RECORDS WHICH CANNOT BE READ BY STANDARD
METHODS. TPRD DIFFERS FROM TAPRD ONLY IN THAT IT ALLOWS
RECORDS TO BE SKIPPED. THIS IS ACCOMPLISHED BY ALTERING THE
FOLLOWING CARDS:

CARD NO. TAPRD VERSION TPRD VERSION

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CCCCCCCC

TPRO1430
TPRO1910
TPRO2990

TAPRD CSECT
MVI TPCCW,X'3F'
TAPRD CSECT

TPRD CSECT
MVI TPCCW,X'37'
TPRD CSECT

OTHERWISE, THE PROGRAMS ARE IDENTICAL. A LISTING OF TPRD VERSION
MINUS THE DOCUMENTATION IS PROVIDED BELOW. SEE W.R.CHURCH
COMPUTER CENTER LIBRARY FOR LISTING OF TAPRD AND APPLICABLE
DOCUMENTATION.

DIMENSION X(4001), Y(4001), LABEL(19), TH(12), DH(12), IREC(1801),
1 NRCSKP(99), DCON(1), AMONCA(13), EVENT(13), D(1801), T(1801)
1 INTEGER B(8001),ZER,DOL,STAR,ONE,FLAG,DLIREC,DLR,BLANK,A(2001),TWO
1,THREE,FOUR,FIVE,SIX,SEVEN,EIGHT,TEN,ELEVEN,AMONC
LCCICAL,PRTI,PRTI2,PLTI,PLTI2,TAPE,ENDFL,CARDS,SKIP

NAMLIST /CTRL/ NN,PRTI,PRTI2,PLTI,PLTI2,TAPE,ENDFL,CARDS,ISTOP,IP
1,IH,NRCSKP,NSKP,JSKP,ISQZ,ISCL,ISCL,ISCL,XBICOR,ICSQZ,TCO
2R/DAT/TH,DH,IH,ICODE,ISCL,ITSC,ITSC,IP,IDEN,ISQZ,ICSQZ,TCO
3R,IHDR,NOIRG,CARDS,ISTA,DCON,DCOR,SKIP,AMONC,TAPE

REAL #8EVENT,WMONTH
DATA AMONCA/H,I,C,K,L,G,P,Q,R,U,V,W,Z/
DATA EVENT/AUG 1973,SEP 1973,OCT 1973,NOV 1973,DEC 1973,
1,JAN 1974,FEB 1974,MAR 1974,APR 1974,MAY 1974,JUN 1974,
2,JUN 1974,AUG 1974/

DEFINE SYMBOLS, NOTEING THAT THE LEFT THREE HEX BYTES IN EACH
ELEMENT OF B END UP FILLED WITH BLANKS
DATA DOL/,\$\$,\$\$,STAR/Z4040405C/,KEY/Z4040405F/,ONE/Z404040F1/,
1FLAG/Z40404050/,DLIREC/Z40404060/,MINUS/Z40404061/,
2DLR/Z4040405B/,BLANK/,ZER/Z404040F0/,TWO/Z404040F2/,
3THREE/Z404040F3/,FOUR/Z404040F4/,FIVE/Z404040F5/,
4MTHU/Z404040E2/,MTHREE/Z404040E3/,MFOUR/Z404040E4/,MFIVE/Z404040E5
5/,SIX/Z404040F6/,SEVEN/Z404040F7/,EIGHT/Z404040F8/,NINE/Z404040F9
6/,TEN/Z404040F0/,ELEVEN/Z4040407B/

*****(A) INITIALIZE VARIABLES AND ARRAYS. *****
THE FOLLOWING CONVERSION FACTOR IS IN HUNDREDS OF INCHES PER
UNIT OF T. IT MAY BE OVERRIDDEN BY THE DATA CARDS.
DCON(1) = 1.0475

DATA CARDS/.FALSE./,DCOR/0.0/,ENDFL/.FALSE./,FG/0./,ICODE/0/,ICSQZ

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1/1/,IDSCCL/1/,IH/O/,IHDR/O/,IP/O/,IPS/8000/,ISCL/1/,ISQZ/1/,ISTOP/O
2/,ITSCCL/1/,ITSQZ/1/,JJJ/O/,JJJ/O/,JREC/1/,JSAV/O/,KOTH1/1/,KOTH2/
31/,NE/O/,NOIRG/O/,NSKP/O/,PL1/.FALSE./,PLI2/.FALSE./,PR1/.TRUE./
4,PR2/.FALSE./,SKIP/.FALSE./,TAPE/.FALSE./,TCOR/O./

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GIVE THE ARRAYS INITIAL VALUES

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DO 20 J=1,12
  TH(J) = 0.
  DH(J) = 0.
20 CONTINUE

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DO 30 J=1,1801
  D(J) = 0.
  T(J) = 0.
30 CONTINUE

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DO 40 J=1,99
  NRCSKP(J) = 0
40 CONTINUE

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READ (5,CTRL) LABEL
WRITE (6,150) LABEL
REWIND HERE IF TAPE IS USED. NOTE THAT IF TAPE=T, JCL
MUST BE PROVIDED TO DEFINE IT.
IF (TAPE) REWIND 8
IF (NSKP.EQ.0) GO TO 110

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***** SKIP RECORDS.*****

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NOTE: THE PROGRAM DIFFERENTIATES BETWEEN INITIALLY SKIPPED RECORDS (NSKP) AND BAD RECORDS (NRCSKP). NRCSKP REQUIRES DATA CARDS FOR BAD RECORDS SKIPPED AND NSKP DOESN'T. PLUS NRCSKP ONLY SKIPS A SINGLE RECORD FOR EACH VALUE ASSIGNED TO NRCSKP, WHEREAS NSKP SKIPS MULTIPLE RECORDS (IE. NSKP=40, THE FIRST 40 RECORDS ON THE TAPE

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C-----
C      FILL THE A ARRAY WITH DOLLARS
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C
C
C      DO 200 I=1,2001
C      THE 2001 ASSURES THAT THE LAST WORD OF A WILL CONTAIN DOLLARS
C      SINCE WE READ IN ONLY 8000 BYTES OF DATA.
C      200 A(I) = DOL
C
C
C      FILL B WITH BLANKS
C
C
C      DO 210 I=1,8000
C      210 B(I) = BLANK
C
C      *****
C      ***(F) SKIP BAD RECORDS.*****
C      THE LIST OF BAD RECORDS IS EXAMINED AND SKIPPED.
C      DO NOT REMOVE THE DATA CARDS FOR THE BAD RECORD.
C      NOTE THAT IF NRCSKP(1) IS ZERO, THE TEST IS SKIPPED.
C      IF (NRCSKP(1).EQ.0) GO TO 250
C
C
C      DO 220 J=1,99
C      NRC = NRCSKP(J)-NSKP
C      IF (NRC.EQ.1) GO TO 230
C      220 CONTINUE
C
C
C      GO TO 250
C      CHANGING IPS TO NEGATIVE CAUSES TPRD TO SKIP A RECORD
C      IPS = -8000
C      230 FORMAT (/5X,'LABEL 240. RECORD NO.',15,' SKIPPED VIA NRCSKP SKIP
C      240 ROUTINE. '//)
C      1 WRITE (6,240) IT
C
C      *****
C      ***(G) READ USABLE RECORD INTO A ARRAY.*****
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2515 AND PERMIT THE POSSIBILITY THAT EITHER 'KEYBOARD' OR 'TRACER'
2520 BUTTONS HAVE BEEN PUSHED TWICE.
2525
2530 IN USING THE CALMA DIGITIZER, SPURIOUS BLANK RECORDS WOULD
2535 APPEAR AT RANDOM THROUGHOUT THE TAPE. WHEN THESE BLANK RECORDS
2540 OCCUR DURING A HEADER RECORD NOTHING IS LOST SINCE HEADER
2545 INFO IS EASILY INSERTED VIA DATA CARDS BY SETTING IHDR=1. THE
2550 HOWEVER, IF A BLANK RECORD OCCURS DURING A TRACE RECORD THE
2555 COMPLETE STATION IS LOST. FROM EXPERIENCE A BLANK RECORD
2560 NORMALLY WILL HAVE TWO CHARACTERS (IE. JJ=2). AFTER THE FIRST
2565 RUN THE BLANK RECORDS CAN BE LOCATED AND CAN BE SKIPPED DEPENDING
2570 INDIVIDUALLY OR THE ENTIRE STATION CAN BE SKIPPED DEPENDING
2575 CN WHETHER THE BLANK RECORD IS IN THE HEADER OR TRACE.
2580 THIS PROBLEM IS SUSPECTED TO BE THE RESULT OF MECHANICAL
2585 PROBLEMS WITH THE DIGITIZER ITSELF AND SHOULD NOT BE A
2590 RECURRING PROBLEM.
2595 JJ=1
2600 GO TO 360
2605
2610 THE FOLLOWING ROUTINE READS ANOTHER SET OF CARDS. THIS IS THE
2615 ENTRY FOR THE SITUATIONS IN WHICH THE IRG IS MISSED.
2620 READ (5,140) LABEL,JSKIP,ISTOP,AMONG
2625 IF (ISTOP.GT.0) GO TO 1370
2630 IF (JSKIP.EQ.0) GO TO 340
2635 READ (5,DAT)
2640 WRITE (6,DAT)
2645 READ (5,CONTRL)
2650 WRITE (6,CONTRL)
2655 DIAGNOSTIC WRITE STATEMENTS FOLLOW:
2660 IPLACE = 185
2665 WRITE (6,180) (D(J),J=1,180),IPLACE
2670 WRITE (6,180) (T(J),J=1,180),IPLACE
2675 WRITE (6,190) (JJ,NE,KDTH1,KDTH2,JJJ)
2680
2685 WRITE (6,350) NOIRG,JJJ
2690 FORMAT (/5X,'LABEL 185. NOIRG=',I3,
2695 1,JJJ=' ',15/)
2700 NOIRG = 0
2705 JJ = JJJJ
2710
2715 INITIALIZE ADDERS,ETC.
2720 SUMU = 0.
2725 SUMT = 0.
2730 N = 0
2735 KL = 0
2740
2745 *****
2750 *****

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C      DO 490 J=KY1,KY2
      B(J) = B(J)-ZER
      IB = B(J)
      490 ISTAA = ISTAA+IB*10**((KY2-J))
C
C      AMONT = B(KY3)
C
C      DO 500 J=KY4,KY5
      B(J) = B(J)-ZER
      IB = B(J)
      500 IDENT = IDENT+IB*10**((J-KY4))
C
C      ICSC = B(KY6)-ZER
      ICOD = B(KY7)-ZER
      ITSC11 = B(KY8)-ZER
      ITSC1 = B(KY9)-ZER
      IPP = B(KY10)-ZER
C
      IF THERE IS A DISAGREEMENT, WRITE A MESSAGE.
      IF (ISTAA.NE. ISTA) GO TO 520
      IF (IDENT.NE. IDEN) GO TO 520
      IF (IDSC.NE. IDSC1) GO TO 520
      IF (ICOD.NE. ICODE) GO TO 520
      IF (ITSC1.NE. ITSC1) GO TO 520
      IF (IPP.NE. IPP) GO TO 520
      IF (IPPP.NE. IPPP) GO TO 520
      510 FORMAT (5X, 'I3,A1/5X, 'IDEPH= ',I3/)
      1 STATEION 'I3,A1/5X, 'IDEN= ',I3/
      WRITE (6,510) ISTA,AMONC,IDEN
      GO TO 540
      520 WRITE (6,530) ISTA,AMONC,IDEN,IDSC1,ICODE,ITSC1,IP,ISTAA,AMON
      1,IDENT, IDSC, ICOD, ITSC1, ITSC1, IPP
      530 FORMAT (/3X, CARD AND TAPE DISAGREE, CARD ON TOP:/3X, ' ISTA AMON
      1C IDENT IDSC1 ICODE ITSC1 IP:/3X, I7, A1, 6I7/3X, I7,
      2 A4, I10, 5I7/)
      C      WRITE THE RESULTS
      540 WRITE (6,550) ISTA,AMONC,IDEN
      550 FORMAT (5X, 'LABEL 550. HEADER PROCESSING COMPLETE EXCEPT SEARCH
      1 FOR ERRORS ON STATION 'I3,A1/5X, 'IDEN= ',I3/)
C
C      CONSIDER IT POSSIBLE THAT NO IRG EXISTS AFTER THE HEADER.

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C THE PROGRAM HAS FILLED THE B ARRAY WITH BOTH THE HEADER AND
C TEMPERATURE TRACE. ASSUME THERE IS A TRACER SYMBOL IN POS-
C ITION 12. IF THIS IS SO, CONTINUE TO PROCESS THE B ARRAY.
  IF (B(KY11).NE.STAR) GO TO 570
  JJJJ = KY11
  WRITE (6,560)
560 FORMAT (75X,'NO IRG AFTER HEADER; CONTINUE TO PROCESS B ARRAY.'//)
  GO TO 330
570 IF (IHDR.EQ.0) GO TO 1360

C THIS BRANCH RETURNS TO 120 IF THE HEADER IS MISSING. SET IHDR=1
C ON THE CARD.
  WRITE (6,580)
580 FORMAT (75X,'HEADER MISSING; INFO INSERTED WITH CARDS.'//)
  IHDR = 0
  GO TO 120

C *****
C***(2) PROCESS TRACE BY SUMMING X AND Y.*****
C THE FOLLOWING PROCEDURE PERMITS THE PRESENCE OF ANY REASONABLE
C NUMBER OF TRACER SYMBOLS (STAR) INCLUDING NONE.
590 NE = 0
  NF = 0
  NSTAR = 0
600 IF (B(JJ).EQ.STAR) GO TO 620

C COUNT STARS AND WRITE MESSAGE
  WRITE (6,610) NSTAR
610 FORMAT (75X,'START TRACER MODE; NO. OF TRACER SYMBOLS =',I2//)
  WHEN THERE ARE NO MORE STARS, START TESTING FOR COUNT SYMBOLS ETC
  GO TO 630
  JJ = JJ+1
620 NSTAR = NSTAR+1
  CONTINUE TO TEST FOR STARS UNTIL NO MORE APPEAR.
  GO TO 600

C THE NEXT BLOCK OF OPERATIONS TO JUST BEYOND 820 LOOPS BACK TO
630 CONTINUALLY, TESTING EACH CHARACTER FOR IDENTITY AND
  CONTINUING TO ADD OR SUBTRACT FROM THE CUMULATIVE AND X COUNTS
  UNTIL A DELETE-RECORD SYMBOL OR A STAR OR A DOLLAR INDICATES
  THE END OF DATA. THE FLAG IS PLACED AT THE POINT WHERE THE TRACE
  ACTUALLY BEGINS TO RECORD T VS D. PREVIOUS COUNTS RESULT
  FROM THE TRACER TRAVELING FROM THE COORDINATE ORIGIN TO THIS
  POINT.
  IF (B(JJ).EQ.ONE) GO TO 650
  IF (B(JJ).EQ.BLANK) GO TO 660
  IF (B(JJ).EQ.MINUS) GO TO 670

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```

IF (B(JJ))-EQ.FLAG) GO TO 820
IF (B(JJ))-EQ.KEY) GO TO 390
THE NEXT GROUP OF STATEMENTS ALLOW FOR OCCASIONAL COUNTS GREATER
THAN + OR - 1.
IF (B(JJ))-EQ.TWO) GO TO 680
IF (B(JJ))-EQ.THREE) GO TO 690
IF (B(JJ))-EQ.FOUR) GO TO 700
IF (B(JJ))-EQ.FIVE) GO TO 710
IF (B(JJ))-EQ.SIX) GO TO 720
IF (B(JJ))-EQ.SEVEN) GO TO 730
IF (B(JJ))-EQ.EIGHT) GO TO 740
IF (B(JJ))-EQ.NINE) GO TO 750
IF (B(JJ))-EQ.TEN) GO TO 760
IF (B(JJ))-EQ.ELEVEN) GO TO 770
IF (B(JJ))-EQ.TWELVE) GO TO 780
IF (B(JJ))-EQ.MTHREE) GO TO 790
IF (B(JJ))-EQ.MFOUR) GO TO 800
IF (B(JJ))-EQ.MFIVE) GO TO 810
IF (B(JJ))-EQ.DLTREC) GO TO 920
WRITE (6,640) B(JJ)
FORMAT (//5X,'SYMBOL NOT RECOGNIZED = ',Z8//)
WE ELIMINATE PRINTING OF THIS STATION AND INITIALIZE VARIABLES
IF (IP.EQ.1) GO TO 1330
GO TO 1560
640      RX = 1.860
650      RX = 0.860
660      RX = -1.860
670      RX = 2.860
680      RX = 3.860
690      RX = 4.860
700      RX = 5.860
710      RX = 6.860
720      RX = 7.860
730      RX = 8.860
740      RX = 9.860
750      RX = 10.860
760      RX = 10.860

```



```

770 GO TO 860
780 RX = 11.
790 RX = -2.
800 RX = -3.
810 RX = -4.
820 RX = -5.
    GO TO 860
    JJ = NE
    JJ = JJ+1
    FG = 1
    GO TO 830
    CHECK HERE FOR MULTIPLE KEYBOARD SYMBOLS. IF NUMBER EXCEEDS
    CHECK TERMINATE THE PROGRAM. THE NUMBER EIGHT IS ARBITRARY.
    SELEDOM DOES ONE GET MORE THAN THREE KEYBOARD SYMBOLS ON THE TAPE
    ACCIDENTALLY.
830 WRITE (6,840)
840 FORMAT (5X,'FOUND EIGHT KEYBOARD SYMBOLS IN SEQUENCE. STOP.')
```

```

850 KL = KL+1
    JJ = JJ+1
    IF (KL.EQ.8) GO TO 830
    IF (8(JJ).EQ.STAR) GO TO 590
    TRY AGAIN
    GO TO 390
```

```

    THE ADDING IS DONE HERE AND THE CUMULATIVE SUM STORED, ONE
    UNIT PER .01 INCH.
860 NE = N+1
    NE = N/2
    IF (NF.EQ.N) GO TO 870
    THIS FIDDLING AROUND DETERMINES IF THE COUNT IS EVEN OR ODD.
    START COUNTING IN THE ORDER YXYYX (BECAUSE THE CHART IS READ
    SIDEWAYS. X AND Y IN THIS PROGRAM HAVE THE NORMAL ORIENTATIONS
    ON THE STRIP CHART. THEY ARE INVERTED WITH RESPECT TO THE
    CALMA DIGITIZER. SPECIFICALLY DEPTH DECREASES ALONG THE
    POSITIVE X AXIS AND TEMP INCREASES ALONG THE POSITIVE Y AXIS
    CN THE CALMA DIGITIZER.
    IF ODD
    SUMD = SUMD+RX
    INCREASE THE ODD INDEX TO KEEP IT THE SAME AS THE EVEN.
    NE = NE+1
    Y(NE) = SUMD
```



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C      JJ = JJ+1
C      GO TO 880
C      IF EVEN
C      SUMT = SUMT+RX
C      X(NE) = SUMT
C      JJ = JJ+1
C      IF A STAR OR DOLLAR IS FOUND, THIS IS THE END OF THE DATA.
C      880 IF (B(JJ).EQ.DLR) GO TO 940
C      END NORMAL TRACE PROCESSING
C      BEGIN TROUBLE SHOOTING
C      IF THERE IS NO IRG BETWEEN TRACES BUT THERE IS A TRACER SYMBOL,
C      THE TWO CAN BE SEPARATED BY FIRST SETTING
C      NOIRG=1, DOING NORMAL PROCESSING ON THE FIRST PART OF THE
C      B ARRAY, READING A NEW SET OF CARDS, AND THEN PROCESSING THE
C      SECOND PART OF B.
C      IF (B(JJ).NE.STAR) GO TO 900
C      NOIRG = 1
C      SAVE THE INDEX OF THE START OF THE SECOND HALF, JJJJ.
C      JJJJ = JJ
C      WRITE (6,890)
C      890 FORMAT (//5X,'FOUND A STAR AT END OF TRACER ASSUME THERE IS NO IRG.
C      1,75X,'PROCESS RECORD IN TWO PARTS, READING CARDS FOR BOTH PARTS.//
C      2)
C      GO TO 940
C      900 IF (B(JJ).NE.KEY) GO TO 630
C      JJJJ = JJ
C      WRITE (6,910)
C      910 FORMAT (//5X,'FOUND A KEYBOARD SYMBOL.  PROCESS NEXT PORTION OF B A
C      RRAY AFTER READING NEW CARDS.//)
C      NOIRG = 1
C      GO TO 940
C      920 WRITE (6,930) JJ
C      930 FORMAT (5X,'FOUND DELETE RECORD SYMBOL AT JJ=',I5)
C      IF DELETE RECORD IS FOUND, GO TO 470 AND INCREMENT THE
C      VARIABLE, IT, BUT RETURN TO STATEMENT 170. A NEW SET OF CARDS
C      IS NOT READ BUT THE RECORD COUNT, IT, IS INCREMENTED.
C      GO TO 470
C      940 JJ = JJ-1
C      END TRACER AND ASSOCIATED TROUBLE SHOOTING
C      *****
C      *** (J) CONVERT X AND Y ARRAYS TO DEPTH AND TEMPERATURE. *****
C      WRITE (6,950) JJJ,NE,Y(NE),X(NE)

```



```

950 FORMAT (/5X,'LABEL 950.  START CONDENSING UNCONVERTED ARRAY AND CO
INVERTING TO SCIENTIFIC UNITS.  ',/5X,'THE TRACER ENTERED THE FRAME (F
2LAG) AT JJJ=',/15/5X,'THE END OF THE TRACE HAS INDEX NE=',/15/
3 5X,'LAST (UNCONVERTED) DEPTH AND TEMP ARE: ',F7.1,2X,F7.1//)
CC
CHECK TO SEE IF FLAG WAS FOUND.
IF (FG.EQ.1) GO TO 970
WRITE(6,960)
960 FORMAT (/5X,'NO FLAG FOUND; PROCESS ANYWAY. '//)
970 WRITE(6,980)
980 FORMAT (/,/,)
FG = 0
CC
THE X AND Y ARRAYS ARE FILLED AND THE START AND END OF THIS BATCH
OF DATA ARE LABELED WITH JJJ AND NE.  THE ARRAYS ARE INDEXED
ON 0.01 INCH DEPTH SPACING.  SUBROUTINE CONDNS INTERPOLATES TO
FILL ANY BLANK ARRAY POSITIONS.
CALL CONDNS (X,Y,T,JJJ,NE,KDTH1,KDTH2)
CC
DO 1060 J=KDTH1,KDTH2
D(J) = (J-1)/DCON(IDUSCL)+DCOR
SUBROUTINE WLQ2, LOCATED IN THE SUBROUTINE LIBRARY OF THE W. R.
CHURCH COMPUTER CENTER WAS USED TO DETERMINE THE COEFFICIENTS
FOR A BEST FIT SECOND DEGREE POLYNOMIAL THAT DESCRIBED THE
RELATIONSHIP BETWEEN THE TEMP AND THE MOVEMENT OF THE STYLUS
AS MEASURED IN HUNDREDS OF INCHES.  IT ACCURATELY DESCRIBE
A SINGLE POLYNOMIAL DID NOT ACCURACY TO BREAK THE TRACE INTO
THIS RELATIONSHIP.  IT WAS NECESSARY TO DETERMINE FOR TEMPS FROM
FIVE SEGMENTS.  THE FIRST EQUATION WAS DETERMINED FOR TEMPS FROM
1 TO 5 DEG.  THE NEXT EQUATION FROM 5 TO 10 DEG., ETC, UP TO A
MAXIMUM OF 25 DEG.  BY USING SEGMENTS THE EQUATIONS ARE ACCURATE
TO WITHIN AT LEAST 0.01 DEG.
CC
TCOR IS A TEMP CORRECTION WHICH MAY BE APPLIED TO A SINGLE
STATION IF NECESSARY.  A SINGLE STATION MAY BE IN ERROR DUE
TO IMPROPER DIGITIZING A TECHNIC.  IF THE OPERATOR STARTS TO
TRACE AT A POINT WHICH IS NOT THE ORIGIN, THE ORIGIN A CONSTANT CORR. CAN
SHIFT THE TRACE BACK TO THE ORIGIN.
XBTCOR IS A CORRECTION DESIGNED TO MAKE THE XBT READING
AGREE WITH A STANDARD.  EITHER WAS MADE AT THE SAME TIME.
STANDARDIZED STD TRACE WHICH WAS NOTICABLY HIGHER THAN THE TEMPS
GENERALLY BY THE OTHER TWO METHODS.  THIS CORRECTION ENABLES ONE TO
COMPARE TEMPS TAKEN BY DIFFERENT METHODS.

```



```

C C C
VALUES ARE INSERTED. IF THERE IS A GAP BETWEEN HAND ENTERED
DATA AND XBT DATA , IT IS NOT FILLED.
C C C
IF (IH.EQ.0) GO TO 1080
T(1) = IH(1)
IF (IH.LT.2) GO TO 1080
IF (ISQZ.GT.1) GO TO 1080
C C C
DO 1070 J=2,IH
D(J) = DH(J)
T(J) = IH(J)
1070 CONTINUE
C C C
1080 CONTINUE
C C C
DIAGNOSTIC WRITE STATEMENTS FOLLOW:
C-----
IPLACE = 1080
WRITE (6,180) (D(J),J=1,180),IPLACE
WRITE (6,180) (T(J),J=1,180),IPLACE
WRITE (6,190) JJJ,NE,KDTH1,KDTH2,JJJJ
C-----
C C C
***** UNWANTED DATA. *****
C C C
***(L) ELIMINATE UNWANTED DATA. *****
C C C
IN DIGITIZING TEMP SEGMENTS ONE FREQUENTLY GETS UNUSUAL VALUES
AT THE TOP OR BOTTOM OF THE TRACE SEGMENT (ZERO OR VERY HIGH). IT
IS DESIRABLE THAT THESE UNWANTED VALUES BE ELIMINATED PRIOR TO
WRITING A TAPE OR PUNCHING CARDS. THUS A CHECK IS MADE TO SEE
IF T(J) IS ZERO OR GREATER THAN 25.
C C C
THESE VALUES ARE WRITTEN OUT
AND COUNTED FOR RECORD PURPOSES BUT ARE DISCARDED FROM THE
D AND T ARRAYS. NOTE THE VALUE OF KDTH2, WHICH IS EQUAL TO THE
TOTAL NUMBER OF RECORDS, IS REDUCED BY THE NUMBER OF UNWANTED
RECORDS.
C C C
K = 0
L = 1
C C C
DO 1110 J=1,KDTH2
IF ((T(J).EQ.0.0).OR.(T(J).GT.25.0)) GO TO 1090
C C C

```



```

D(L) = D(J)
T(L) = T(J)
L = L+1
GO TO 1110
1090 WRITE (6,1100) D(J),T(J),J
K = K+1
JSAV = K
1100 FORMAT (//5X,2F7.2,16,/)
1110 CONTINUE
CC
CC
1120 FORMAT (//5X,' JSAV=',16,/)
WRITE (6,1120) JSAV
KDTH2 = KDTH2-JSAV
CC
CC
***** GENERATE SERIAL NUMBERS FOR TAPE OUTPUT.*****
CC
CC
***** GENERATE SERIAL NUMBERS FOR THE RECORDS. A RECORD IS
***** EITHER A HEADER FOR A STATION OR THE VALUES (D AND T) FOR
***** A SINGLE DEPTH.
CC
CC
DO 1130 J=1,KDTH2
JREC = JREC+1
JREC(J) = JREC
1130 CONTINUE
CC
CC
***** CONVERT LETTER CODE TO MONTH/YEAR.*****
CC
CC
***** THIS SECTION CONVERTS THE LETTER DESIGNATOR FOR MONTH (AMONC)
***** FROM THE SINGLE LETTER CODE ON THE DIGITIZED TAPE TO THE
***** APPROPRIATE MONTH AND YEAR IN PREPARATION FOR WRITING THE OUTPUT.
CC
CC
DO 1140 J=1,13
IF (AMONC.EQ.AMONCA(J)) GO TO 1160
1140 CONTINUE
CC
CC
1150 FORMAT (15X,'AMONC NEVER DID EQUAL AMONC(J) CONSEQUENTLY,

```



```

5395 1 WMONTH WILL NOT BE DEFINED./)
5400 WRITE (6,1150)
5405 GO TO 1170
5410 1160 WMONTH = EVENT(J)
5415 1170 CONTINUE
5420
5425 *****
5430 *** (0) OUTPUT. *****
5435 *****
5440 *****
5445 *****
5450 *****
5455 *****
5460 *****
5465 *****
5470 *****
5475 *****
5480 *****
5485 *****
5490 *****
5495 *****
5500 *****
5505 *****
5510 *****
5515 *****
5520 *****
5525 *****
5530 *****
5535 *****
5540 *****
5545 *****
5550 *****
5555 *****
5560 *****
5565 *****
5570 *****
5575 *****
5580 *****
5585 *****
5590 *****
5595 *****
5600 *****
5605 *****
5610 *****
5615 *****
5620 *****
5630 *****

C PRINT DATA
C
C THE PARAMETER ISQZ PERMITS CONDENSING THE PRINTED DATA BY THE
C FACTOR ISQZ
C
C IF (.NOT.PRT1) GO TO 1190
C
C WRITE (6,1180)
C FORMAT (1,1)
C CALL OUT2 (D,T,KDTH2,ISTA,WMONTH,IREC,JREC,ISQZ)
C
C WRITE TAPE
C
C TAPE MUST BE TRUE ONLY ONCE, AT THE BEGINNING OF TAPE WRITING.
C THE PROGRAM EXPECTS JCL TO WRITE CARD IMAGES ON THE TAPE
C IN RECORDS 20 DIGITS LONG.
C
C 1190 IF (.NOT.TAPE) GO TO 1230
C WRITE THE HEADER INFO HERE.
C WRITE (8,1200) ISTA,WMONTH,KDTH2
C FORMAT (14,A9,I6)
C 1200 WRITE (8,1210) (D(J),T(J),J=1,KDTH2)
C FORMAT (F8.2,F6.2)
C 1210 WRITE (6,1220) ISTA,WMONTH,JREC
C FORMAT (5X,'DATA FOR STATION ',I5,A12,' WRITTEN ON TAPE UP TO
C 1 RECORD ',I6)
C
C PUNCH CARDS
C
C COMPRESS THE PUNCHED DATA BY A FACTOR ICSQZ. FORMAT FOR FOUR
C DATA SETS ON A CARD. NPTS BECOMES THE NUMBER OF DATA PRINTED
C IF IT IS EVENLY DIVISIBLE. OTHERWISE THE LAST DATUM IS ALSO
C PUNCHED. SUPPLY JCL FOR CARD PUNCHING.
C
C 1230 IF (.NOT.CARDS) GO TO 1330
C
C THE NUMBER OF POINTS TO BE RETAINED AFTER CONDENSATION IS
C 1+(N-1)/ISQZ. IF THIS DOES NOT COME OUT INTEGRAL ADD THE LAST
C POINTS.
C NPTS = (KDTH2-1)/ICSQZ

```



```

5635 NPT1 = KDIH2-1-ICSQZ*NPTS
5640 NPTS = NPTS+1
5645 WRITE A HEADER CARD
5650 FORMAT (14X,'OCEANOGRAPHIC DATA FROM U C M II',/)
5655 FORMAT (1X,14,'VALUES OF D,T FOR XBT STA.',I3,A8,'COMPRESSED BY',
5660 I3,/)
5665 FORMAT (4X,'DEPTH',2X,'TEMP.',2X,'DEPTH',2X,'TEMP.',2X,'DEPTH',
5670 1 2X,'TEMP.',2X,'DEPTH',2X,'TEMP.',)
5675 FORMAT (4X,'METERS',1X,'DEG.C.',1X,'METERS',1X,'DEG.C.',1X,'METERS
5680 1,'1X,'DEG.C.',1X,'METERS',1X,'DEG.C.',/)
5685 WRITE (7,1240)
5690 WRITE (7,1250) NPTS,1STA,WMONTH,ICSQZ
5695 WRITE (7,1260)
5700 WRITE (7,1270)
5705 NOW FIND THE NUMBER OF CARDS
5710 NCARDS = NPTS/4
5715 NCRD1 = NPTS-4*NCARDS
5720 THERE WILL BE ONE MORE CARD IF NCRD1.NE.0.
5725 INCR = 4*ICSQZ
5730 J = 1-INCR
5735 K = 0
5740 J = J+INCR
5745 K = K+1
5750 J1 = J+ICSQZ
5755 J2 = J1+ICSQZ
5760 J3 = J2+ICSQZ
5765 FORMAT (2X,4(F8.2,F6.2),3X,I3,A10,I6A
5770 WRITE (7,1290) D(J),T(J),D(J1),D(J2),D(J3),T(J3),1STA,
5775 1WMONTH,JREC
5780 IF (K.LT.NCARDS) GO TO 1280
5785 IF (NCRD1.EQ.0) GO TO 1320
5790 WRITE THE LAST CARD
5795 J = J3+ICSQZ
5800 WRITE (7,1290) D(J),T(J)
5805 IF (J.EQ.KDTH2) GO TO 1320
5810 J = J+ICSQZ
5815 FORMAT (1H+,16X,F8.2,F6.2)
5820 WRITE (7,1300) D(J),T(J)
5825 IF (J.EQ.KDTH2) GO TO 1320
5830 J = J+ICSQZ
5835 FORMAT (1H+,30X,F8.2,F6.2)
5840 WRITE (7,1310) D(J),T(J)
5845 1320 CONTINUE
5850 C
5855 IF (ENDFL) END FILE 8
5860 C
5865 C
5870 C

```

```

C*** (P) INITIALIZE VARIABLES FOR NEXT STATION. *****
C
C      JREC = JREC+1
C
C
C      DO 1340 J=1,1801
C      D(J) = 0.
C      T(J) = 0.
C      1340 CONTINUE
C
C
C      DO 1350 J=1,12
C      TH(J) = 0.
C      DH(J) = 0.
C      1350 CONTINUE
C
C
C      SKIP = .FALSE.
C      IDEN = 0
C      IH = 0
C      IP = 0
C      JSAB = 0
C      IF (NOIRG.EQ.1) GO TO 330
C
C      1360 IT = IT+1
C      GO TO 120
C      1370 STOP
C      END

```

5875
5880
5885
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5900
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5990
5995
6000
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6010
6015
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6025
6030

```

C
C      SUBROUTINE OUT2
C      THIS OUTPUT SUBROUTINE FOR DIGIXBT PRINTS DEPTHS AND TEMPS
C      FOUR COLUMNS TO A PAGE.
C
C      SUBROUTINE OUT2 (D,T,KDTH2,ISTA,WMONTH,IREC,JREC,ISQZ)
C      REAL *8 WMONTH
C      DIMENSION D(1801), T(1801), IREC(1801)
C      PRODUCE HEADING
C      20 FORMAT (14X,'OCEANOGRAPHIC DATA FROM U C M II',/)
C      30 FORMAT (1X,14,' VALUES OF D,T FOR XBT STA.',I3,A8,'COMPRESSED BY',
C      1 13,/)

```

5
10
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50
55

40	FORMAT(4X,'DEPTH',2X,'TEMP.',2X,'DEPTH',2X,'TEMP.',2X,'DEPTH',	60
1	2X,'TEMP.',2X,'DEPTH',2X,'TEMP.')	65
50	FORMAT(4X,'METERS',1X,'DEG.C.',1X,'METERS',1X,'DEG.C.',1X,'METERS	70
1	1X,'DEG.C.',1X,'METERS',1X,'DEG.C.',1X,'DEG.C.',1X,'METERS	75
	NPTS = NPIS+1	80
	INCR = 4*ISQZ	90
	NPTS = (KDT2-1)/ISQZ	95
	WRITE(6,20)	100
	WRITE(6,30) NPTS,ISTA,WMONTH,ISQZ	105
	WRITE(6,40)	110
	WRITE(6,50)	115
	COMPUTE NUMBER OF FULL LINES	120
	NLNS = (KDT2-1+ISQZ)/INCR	125
	NLN1 = KDT2-1-(4*NLNS-1)*ISQZ	130
	J = 1-INCR	135
	K = 0	140
60	J = J+INCR	145
	K = K+1	150
	J1 = J+ISQZ	155
	J2 = J1+ISQZ	160
	J3 = J2+ISQZ	165
70	FORMAT(2X,4(F8.2,F6.2),10X,2I6)	170
	WRITE(6,70) D(J),T(J),D(J1),T(J1),D(J2),T(J2),D(J3),T(J3),IREC(J)	175
1	IREC(J3)	180
	IF (K.LT.NLNS) GO TO 60	185
	IF (NLN1.EQ.0) GO TO 120	190
	WRITE THE LAST LINE	195
	J = J3+ISQZ	200
	WRITE(6,70) D(J),T(J)	205
	IF (J.EQ.KDT2) GO TO 110	210
	J = J+ISQZ	215
80	FORMAT(1H+,15X,F8.2,F6.2)	220
	WRITE(6,80) D(J),T(J)	225
	IF (J.EQ.KDT2) GO TO 110	230
	J = J+ISQZ	235
90	FORMAT(1H+,29X,F8.2,F6.2)	240
	WRITE(6,90) D(J),T(J)	245
100	FORMAT(1H+,73X,I6)	250
110	WRITE(6,100) IREC(J)	255
120	CONTINUE	260
	COUNT RECORDS	265
130	FORMAT(/5X,'THIS STATION CONTAINS RECORDS ',15,' TO ',15,' INCLU	270
1	ISIVE.'/)	275
	WRITE(6,130) IREC(1),JREC	280
140	FORMAT(1H1)	285
	WRITE(6,140)	290
		295

RETURN
END

```

C-----SUBROUTINE CONDNS-----
C THIS SUBROUTINE FINDS THE ARRAY LOCATIONS FOR X, INDEXED
C SEQUENTIALLY FOR EACH UNIT OF Y. EACH UNIT OF Y IS 1.0 AND
C CORRESPONDS TO .01 INCHES OF TRAVEL IN THE DEPTH DIRECTION.
C
C SUBROUTINE CONDNS (X,Y,T,JJJ,NE,KDTH1,KDTH2)
C DIMENSION X(1), Y(1), I(1), KINS(10), KNO(10)
C IF FIRST INDEX IS ZERO OR NEGATIVE THERE IS A MISBEHAVIOR ELSE-
C WHERE IN THE PROGRAM. RESET JJJ TO 1.
C IF (JJJ.GE.1) GO TO 30
C JJJ = 1
C WRITE (6,20)
C 20 FORMAT (/5X, '***** JJJ RESET TO ONE - SOMETHING WRONG *****')
C 30 KDTH1 BECOMES THE INDEX OF THE START OF THIS ARRAY SEGMENT.
C KDTH1 = Y(JJJ)+1.50
C BUT IN CASE KDTH1 BECOMES ZERO OR LESS, USE THE START OF THE
C CURVE AS THE ORIGIN OF INDEXING.
C THIS CAUSES AN OVERLAP BETWEEN ARRAYS, BUT IT SHOULD BE SMALL.
C XINC = 0.
C IF (KDTH1.GT.0) GO TO 40
C XINC = FLDAT(1-KDTH1)
C KDTH1 = 1
C
C 40 JJJ = JJJ+1
C NE1 = NE-1
C FORM SUBSCRIPTS FROM THE DEPTH INCREMENTS AND STORE X'S AT THOSE
C ARRAY LOCATIONS.
C SEARCH FOR BLANKS IN ARRAY BETWEEN INDEXES KDTH1 AND KDTH2.
C KCT COUNTS THE NUMBER OF BLANKS
C KCT = 0
C KSAV = KDTH1
C KINS(J) IS THE NUMBER OF THE ARRAY POSITION FILLED.
C
C DO 50 J=1,10
C KNO(J) = 0
C 50 KINS(J) = 0
C

```



```

C      DO 80 J=JJ1,NE1
C      KDTH = Y(J)+1.50+XINC
C      T(KDTH) = X(J)
C      TEST TO SEE IF INDEX IS THE SAME OR ONE GREATER THAN THE LAST
C      ONE. IF NOT, INTERPOLATE VALUES.
      NREP = KDTH-KSAV
      IF (NREP.LE.1) GO TO 70
      KCT = KCT+1
      IF (KCT.GT.10) KCT = 10
      KNO(KCT) = NREP
      KINS(KCT) = KDTH
      I1 = KSAV+1
      I11 = KDTH-1
      E = FLOAT(NREP)
      G = T(KDTH)
      F = G-T(KSAV)

      DO 60 I=I1,I11
      60 T(I) = (FLOAT(I-KSAV)/E)*F+G

      70 KSAV = KDTH
      80 CCNT=INUE

      KDTH2 = Y(NE)+1.50+XINC
      PUT IN THE FIRST POINT, WHICH OTHERWISE WOULD BE THE LAST
      CNE FOR WHICH Y(J).LT.1.
      T(KDTH1) = X(JJ)
      T(KDTH2) = X(NE)
      SAVE INDEX OF END OF ARRAY.

      WRITE DOWN NUMBER AND LOCATIONS OF INTERPOLATED VALUES.
      WRITE (6,90) KCT,(KINS(I),I=1,KCT),(KNO(I),I=1,KCT)
      90 FORMAT (/5X,'BLANK ARRAY POSITIONS FILLED IN ',I3,' PLACES. BEGIN
      1 FINE INDEXES AND NO. OF STEPS',5X,'(10 EACH) ARE: ',5X,10I6/
      2 RETURN
      END

```



```

C-----SUBROUTINE CHMOVE-----
C      SUBROUTINE CHMOVE (A,I,B,J)
C      THIS SUBROUTINE RETURNS A LOGICAL*1 VARIABLE TO A 4-BYTE ADDRESS
C      IN THE MAIN PROGRAM, UNPACKING THE ORIGINAL 4-BYTE WORDS A
C      BYTE AT A TIME.
C      LOGICAL *1A(1),B(1)
C      B(J) = A(I)
C      RETURN
C      END

```

```

**
.....
MACRO
REGS
LCLA
LCCLC
ANUP
SETC
EQU
SETA
AIF
MEND
SPACE 2
CSECT
SPACE 2
REGS
SPACE 2
STM
R14,R12,12(R13)
L R12,R15
USING R12,R12
LA R11,SAVE
ST R13,4(R11)
ST R11,8(R13)
L R13,R11
L R11,R1
USING ARG, R11
L R10,4ADD
L R10,SHOVAAD
L R10,ALADD
L R10,0(R10)
L R10,SHOVALN
L R10,TPDCB
LA R10,DCB
USING DCB, R10
TM DCBOFLGS,X,10' HAS DCB BEEN OPENED?
.....
TPRO1300
TPRO1310
TPRO1320
TPRO1330
TPRO1340
TPRO1350
TPRO1360
TPRO1370
TPRO1380
TPRO1390
TPRO1400
TPRO1410
TPRO1420
TPRO1430
TPRO1440
TPRO1450
TPRO1460
TPRO1470
TPRO1480
TPRO1490
TPRO1500
TPRO1510
TPRO1520
TPRO1530
TPRO1540
TPRO1550
TPRO1560
TPRO1570
TPRO1580
TPRO1590
TPRO1600
TPRO1610
TPRO1620
TPRO1630

```


BO	OOKK	YES		TPR01640
TM	BADBOMB,X'AA'	HAS THERE BEEN PREVIOUS CATASTROPHE?		TPR01650
BND	ONWITHIT	NOPE, GO AND OPEN IT		TPR01660
SPACE	2,DUMP	SHOULDN'T EVER GET HERE, CRASH		TPR01670
SPACE	2			TPR01680
OPEN	(TPDCB,INPUT)			TPR01690
TM	DCBOFLGS,X'10'	DID STUPID THING OBEY?		TPR01700
BND	KIKIT	NOPE, GO PUNT		TPR01710
L	R9,DCBDEBAD	GET POINTER AND DEVICE STATISTICS TABLE		TPR01720
L	R9,32(R9)	GET UCB ADDR OUT OF DEB		TPR01730
SR	R6,R6			TPR01740
IC	R6,9(R9)	GET STAT TABLE POINTER		TPR01750
NH	R6,H'10'	POINTER * 10		TPR01760
L	R9,16	POINTER TO CVT		TPR01770
L	R9,112(R9)	POINTER TO STAT TABLE START		TPR01780
LA	R9,0(R6,R9)	POINTER TO STAT TABLE		TPR01790
ST	R9,STATTAB	GOTCHA STAT TABLE		TPR01800
MVC	OLDSTAT,0(R9)	SAVE ADDRESS OF STAT TABLE		TPR01810
SPACE	2	SAVE ITS INFO		TPR01820
L	RO,SHOVALN	GET BLKSIZE FOR TAPE EXCP BUFFER		TPR01830
STH	RO,BYTCNT	PUT DATA LENGTH INTO CCM		TPR01840
L	R1,SHOVAAD			TPR01850
ST	R1,TPBUFLC			TPR01860
MVC	TPBLOC,TPBUFLC+1	PUT BUFFER LOC IN CCM		TPR01870
LTR	RO,RO			TPR01880
BP	OOKKK			TPR01890
MVI	TPCCW,X'37'			TPR01900
BAL	R9,TPGET			TPR01910
MVI	TPCCW,X'02'			TPR01920
BAL	R9,TPWAIT			TPR01930
B	RETURN			TPR01940
SPACE	2			TPR01950
SPACE	2	GO READ A BUFFER		TPR01960
BAL	R9,TPGET			TPR01970
SPACE	2			TPR01980
BAL	R9,TPWAIT			TPR01990
LA	R15,0	GO WAIT TILL READ FINISHED		TPR02000
L	R13,4(R13)	NORMAL RETURN, MODIFIED ELSEWHERE		TPR02010
L	R14,12(R13)	RESTORE REGISTERS		TPR02020
LM	RO,R12,20(R13)			TPR02030
BR	R14			TPR02040
SPACE	2	ALL RETURNS THRU HERE		TPR02050
MVI	RETURN+3,X'04'	SET EOF RETURN		TPR02060
SPACE	2			TPR02070
CLOSE	TPDCB			TPR02080
SPACE	2			TPR02090
MVI	BADBOMB,X'AA'	TURN ON FLAG		TPR02100
				TPR02110

GETSTAT	B SPACE 2	RETURN			TPR02120
	L MVC	R9, STATTAB	ARRIVE HERE ON BAD READ		TPR02130
	L MVC	NEWSTAT, O(R9)	GET CURRENT STAT TABLE		TPR02140
	MVI	R9, SHOVAAD	MOVE OLD AND NEW TABLES TO FTN		TPR02150
	B	O(16, R9), OLDSSTAT	ARRAY BEFORE ERROR RETURN		TPR02160
		RETURN+3, X'08'	SET I/O ERROR RETURN		TPR02170
		OUT			TPR02180
TPGET	B SPACE 2	I, PECB, X'00'	CLEAR ECB		TPR02190
	MVI	TPEXCP, TPCCW			TPR02200
	MVI	RDFLG, X'FF'	TURN ON READ FLAG		TPR02210
	EXCP	TPIOB	DO IT		TPR02220
	BR	R9	RETURN		TPR02230
	B SPACE 2	TPECB, X'40'	IS IT ALREADY DONE?		TPR02240
TPWAIT	TM	TPECB	YES		TPR02250
	BO	NOWAIT	NO, WAIT FOR IT		TPR02260
	WAIT	ECB=TPECB	DID IT DO IT OK?		TPR02270
	CLI	TPECB, X'7F'	YES, CONTINUE		TPR02280
NOWAIT	BE	OK1			TPR02290
	B SPACE 2	TPECB, X'40'	PROBABLE EOF IF CHAN-DEV END & UNIT EXCPT		TPR02300
	CLI	TPECB	NOPE, GO FIND ERROR		TPR02310
	BNE	GETSTAT	EXCEPTIONAL CONDIT BIT ON? (=EOF)		TPR02320
	CLI	FLAGS1, X'04'	NO EOF		TPR02330
	BNE	GETSTAT	DECREMENT DCBBLKCT SO IT MATCHES TAPE		TPR02340
	LCTR	R1, DCBBLKCT	TRAILER LABELS		TPR02350
	ST	R1, 0			TPR02360
	EOV	R1, DCBBLKCT			TPR02370
	B SPACE 2	TPDCB	YES, EOF - FORCE CONTROL TO EODAD RTN		TPR02380
OK1	BR	R9	RETURN		TPR02390
SAV1	B SPACE 2	I8F'0'			TPR02400
	DC	D'0'			TPR02410
OLDSTAT	DC	D'0'	COPY OF STAT TABLE AFTER OPEN		TPR02420
NEWSTAT	DC	D'0'	COPY OF STAT TABLE UPON ERROR		TPR02430
	B SPACE 2	D'0'	LOC CONTAINING CCW BEING USED		TPR02440
TPEXCP	DC	X'02'	READ		TPR02450
TPCCW	DC	AL3(0)	DATA ADDRESS		TPR02460
TPBLOC	DC	X'20'	SUPPRESS INCORRECT LNGT		TPR02470
FLGS	DC	H'0'	BYTE COUNT		TPR02480
BYTCNT	DC	A(0)	LOC OF SMF INFO		TPR02490
	B SPACE 2	A(0)	ADDR OF FORTRAN ARRAY		TPR02500
SHOVSMF	DC	F'0'	BYTE LENGTH OF FORTRAN ARRAY		TPR02510
SHOVAAD	DC	A(0)	LOC OF DCBBLKSI LENGTH TAPE BUFFER		TPR02520
SHOVALN	DC	A(0)			TPR02530
TPBUFLOC	DC	A(0)			TPR02540
					TPR02550
					TPR02560
					TPR02570
					TPR02580
					TPR02590

STATTAB	SPACE	A(0)	LOC OF STAT TABLE
DC	2		
SPACE	2		
SPACE	2		
DC	X'00'		
DC	X'00'		
SPACE	2		
DCB			
SPACE	2		
DS	OF		
DS	QCL32		
DC	X'00'		
DC	X'00'		
DC	X'00'		
DC	X'00'		
DC	X'00'		
DC	X'00'		
DC	X'00'		
DC	AL3(TPECB)		
DC	X'00'		
DC	7X'00'		
DC	X'00'		
DC	AL3(TPEXCP)		
DC	X'00'		
DC	AL3(TPDCB)		
DC	X'00'		
DC	AL3(0)		
DC	H'1'		
DC	H'0'		
SPACE	2		
DC	F'0'		
SPACE	2		
DSECT			
DC	A(0)		
DC	A(0)		
SPACE	2		
PRINT	NOGEN		
DCBD	DSORG=P,S,DEV D=TA		
PRINT	GEN		
SPACE	2		
CSECT			
LTORG			
END			
TPRD			

A P P E N D I X C

C	TITLE	HYDRO - A MODIFIED VERSION
C	PROGRAMMER	R.E.GREER MODIFIED AN ORIGINAL PROGRAM, HYDRO, DEVELOPED BY THE U.S. NAVAL POSTGRADUATE SCHOOL, DEPARTMENT OF OCEANOGRAPHY.
C	PURPOSE	THE PROGRAM READS AND INTERPOLATES TEMPERATURE AND SALINITY DATA FOR STANDARD DEPTHS, AND CALCULATES SIGMA-T, SPECIFIC VOLUME ANOMALY, SOUND VELOCITY, DYNAMIC HEIGHT, DYNAMIC HEIGHT ANOMALY, AND GEOSTROPHIC CURRENTS AND TRANSPORT.
C	MODIFICATIONS	THE ORIGINAL PROGRAM HYDRO HAS BEEN MODIFIED TO INCLUDE AN INCREASED CAPABILITY TO PROCESS TEMPERATURE AND SALINITY DATA ON A VERTICAL DEPTH SCALE INTERVAL AS FINE AS 2.5 METERS, AND A CARD PUNCHING ROUTINE WHICH PRODUCES COMPOSITE DATA CARDS, EACH CONTAINING DEPTH, TEMPERATURE, SALINITY, GEOSTROPHIC VELOCITY, DYNAMIC HEIGHTS, AND MASS TRANSPORT. MODIFICATIONS AFFECT ONLY THE MAIN PROGRAM AND SUBROUTINE GEOCUR.
C	DATE	26 JUNE 1975


```

REAL *8 ITL(12), INFO(200,4)
DIMENSION ID(200), IT(200), IS(200), IO(200)
DIMENSION D(200), ST(98), SS(98), SGT(98), SV(98), SVA(98)
DIMENSION SGP(200), DH(98), BDH(98), DD(98), SLEV(48), BSLVA(98)
DIMENSION NPA(48), NPB(48), NO(48), NSTA(48,3), ALT(48), ALM(48)
DIMENSION ALN(48), ANM(48), IDATE(48,3), DHT(48,98), ADH(98)
COMMON /INFO/ ASS(2000), ASGT(2000), AST(2000), KB
FORMAT (I1, STATE, ION, 3A4, LATITUDE, I2, F5.1, N LONGITUDE,
1 I3, F5.1, W, DATE, I3, F5.1, W, DATE, 3A4//)
2 N LONGITUDE
9 FORMAT (I8(1X, 2I2, F5.0), 3A4, LATITUDE =, I2, F5.1, N LONGITUDE =,
1 I4, F5.1, W, DATE, 3A4//)
11 FORMAT (10X, * INDICATES ADJUSTED VALUE)
12 FORMAT (10X, ? INDICATES QUESTIONABLE VALUE)
13 FORMAT (14, 3A4, F4.0, F4.1, F4.0, F5.1, 3A4)
15 FORMAT (F8.1, A1, 1X, F9.2, A1, F10.3, A1, F9.3, A1, 7X, 4A8)
  
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16 FORMAT (10X,'DEPTH TEMPERATURE SALINITY SIGMA-T OXYGEN'//)
17 FORMAT (20X,'OBSERVED VALUES'//)
18 FORMAT (/20X,'INTERPOLATED VALUES'//)
19 FORMAT (10X,'DEPTH TEMPERATURE SALINITY SIGMA-T SND VEL SPE
1C VOL SPEC V ANOM MEAN SVA DELTA D DYNAMIC HEIGHT'//)
20 FORMAT(10X,F5.0,F10.2,F12.3,F9.3,F12.2,F10.4,F12.6,25X,F10.5/80X,
12F12.6)
21 FORMAT (10X,F6.1,A1,F8.2,A1,F11.3,A1,F8.3,F9.3,A1,4X,4A8/)
DATA SD/0.,5.,10.,15.,20.,25.,30.,35.,40.,45.,50.,55.,60.,65.,70.,
175.,80.,85.,90.,95.,100.,105.,110.,115.,120.,125.,130.,135.,140.,
2145.,150.,155.,160.,165.,170.,175.,180.,185.,190.,195.,200.,205.,
3210.,215.,220.,225.,230.,235.,240.,245.,250.,255.,260.,265.,270.,
4275.,280.,285.,290.,295.,300.,310.,320.,330.,340.,350.,375.,400.,
5425.,450.,475.,500.,525.,550.,575.,600.,625.,650.,675.,700.,725.,
6750.,775.,800.,825.,850.,900.,1000.,1100.,1200.,1300.,1500.,1700.,
72000.,2500.,3000.,4000.,5000./

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CCCC

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READ THE NUMBER OF GEOSTROPHIC CURRENTS & TRANSPORTS
TO BE CALCULATED

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```

READ (5,13) NGC
IF(NGC.EQ.0) GO TO 410
READ (5,9) (NPA(I),NPB(I),SLEV(I),I=1,NGC)
410 NPA(NGC+1)=0

```

```

M=1
KB=1
FORMAT(1X,' KB = ',I8,///)
WRITE(6,999) KB
DO 41 L=1,48
999

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CCCC

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READ HEADING CARD, CHECK FOR END OF DATA, THEN
READ NOV DATA CARDS.

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READ (5,13) NOV,(NSTA(L,K),K=1,3),ALT(L),ALM(L),ALN(L),ANM(L),
1(IDATE(L,K),K=1,3)
IF (NOV) 32,32,24
24 DO 25 I=1,NOV
READ (5,15) D(I),ID(I),T(I),S(I),IS(I),O2(I),IO(I),
1(INFO(I,J),J=1,4)

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CCCC

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SGTSVA IS SUBROUTINE TO COMPUTE SIGMA-T, SPECIFIC VOLUME
AND SPECIFIC VOLUME ANOMALY.

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25 CALL SGTSVA (T(I),S(I),D(I),SGP(I),SVNO,SVNO)

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CCCC

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LGTP IS SUBROUTINE TO COMPUTE INTERPOLATED VALUES

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CALL LGTP(NOV,D,T,SD,ST,NA)

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CALL LGTP(NOV,D,S,SD,SS,NB)
NO(L)=NA
DO 27 I=1,NA

C
C
C      SNDVEL IS SUBROUTINE TO COMPUTE SOUND VELOCITY

CALL SNDVEL (ST(I),SS(I),SD(I),SNDV(I))
CALL SGT SVA (ST(I),SS(I),SD(I),SGT(I),SV(I),SVA(I))
CONTINUE
NLT=ALT(L)
NLN=ALN(L)
WRITE(6,10) (NSTA(L,K),K=1,3),NLT,ALM(L),NLN,ANM(L),
1(IDATE(L,K),K=1,3)
WRITE(6,18)
WRITE(6,19)
NA=NA-1
DH(1)=0
DO 30 I=1,NA
BSVA(I)=(SVA(I)+SVA(I+1))*5
DD(I)=BSVA(I)*(SD(I+1)-SD(I))
30 DH(I+1)=DH(I)+DD(I)
DO 31 I=1,NA
DHT(L,I)=DH(I)
ASS(M)=SS(I)
ASGT(M)=SGT(I)
AST(M)=ST(I)
M=M+1
31 WRITE (6,20) SD(I),ST(I),SS(I),SGT(I),SNDV(I),SV(I),SVA(I),DH(I),
1BSVA(I),DO(I)
I=NA+1
DHT(L,I)=DH(I)
ASS(M)=SS(I)
ASGT(M)=SGT(I)
AST(M)=ST(I)
M=M+1
3 WRITE (6,20) SD(I),ST(I),SS(I),SGT(I),SNDV(I),SV(I),SVA(I),DH(I)
FORMAT(1X,' M = ',I4,///)
41 WRITE(6,3) M
CONTINUE
3 IF (NGC.EQ.0) GO TO 33
42 L=1,48
32 IF (NPA(L).EQ.0) GO TO 33
BASE=SLEV(L)
N1=NPA(L)
N2=NPB(L)
NUI=NO(N1)
NU2=NO(N2)
DO 43 I=1,NU1

```



```

43 ADH(1)=DHT(N1,I)
DO 44 I=1,NU2
44 BDH(1)=DHT(N2,I)
NLN=ALN(N1)
MLN=ALN(N2)
130 FORMAT(1X,3A4,I4)
ISAVE=(NU1/2.0)+1.0
IF(IISAVE.EQ.37) GO TO 131
ISAVE=37
131 WRITE(6,130) (NSTA(N1,K),K=1,3),ISAVE
WRITE(6,8) (NSTA(N1,K),K=1,3),NLN,ANM(N1),
1(IDATE(N1,K),K=1,3),(NSTA(N2,K),K=1,3),MLN,
2ANM(N2),(IDATE(N2,K),K=1,3)
ALAT=ALT(N1)+ALM(N1)/60.
ALON=ALN(N1)+ANM(N1)/60.
BLAT=ALT(N2)+ALM(N2)/60.
BLCN=ALN(N2)+ANM(N2)/60.

CCC
DSTSTA IS SUBROUTINE TO COMPUTE DISTANCE BETWEEN STATIONS
CALL DSTSTA (ALAT,ALON,BLAT,BLON,X2,DIST)
CCC
GEOCUR IS SUBROUTINE TO COMPUTE GEOSTROPHIC CURRENTS
AND TRANSPORTS
42 CALL GEOCUR(NU1,ADH,NU2,BDH,SD,BASE,X2,NNN,DIST)
33 STOP
END

```



```

SUBROUTINE:GEOCUR(NA,ADH,NB,BDH,SD,BASE,X2,NNN,DIST)
DIMENSION ADH(NA),BDH(NB),SD(98),RVEL(98),VEL(98),AMB(98),AVT(98)
COMMON /INFO/ ASS(2000),ASGT(2000),AST(2000),KB
FORMAT (13X,DEPTH DYN HT STA A STA B REL VEL ABS CM/SEC
1 VEL ABS VOL/14X,M.
2 CM/SEC TRANSPORT *./)
11 FORMAT(13X,F5.0,2X,3(F9.5,1X),2(F8.2,2X)/72X,F9.5)
12 FORMAT('***** LEVEL OF NO MOTION MUST BE EQUAL TO A STANDARD DEPT
1H *****')
14 FORMAT(' ,10X,'TOTAL VOLUME TRANSPORT IS COMPUTED BY SUMMING INCR
MENTAL TRANSPORTS ABOVE LEVEL OF NO MOTION: '//5X,'TOTAL TRANSPORT
2 PERPENDICULAR TO THE PLANE OF THE STATIONS IS ',F7.3,' SVERDRUPS
3 RELATIVE TO ',F5.0,' METERS,')
15 FORMAT('// * VALUES IN THIS COLUMN REPRESENT TRANSPORTS IN LAYER
1 INCREMENTS//')
IF(NA.LE.NB) GO TO 51
N=NB
GO TO 52
51 N=NA
52 DO 53 I=1,N
53 AMB(I)=ADH(I)-BDH(I)
RVEL(I)=-AMB(I)*X2
DO 54 I=1,98
54 IF(BASE.EQ.SD(I))GO TO 55
CONTINUE
WRITE(6,12)
GO TO 70
55 NM=1
IF(NM.GT.N) NM=N
BASE=SD(NM)
DO 56 I=1,N
56 VEL(I)=RVEL(I)-RVEL(NM)
DO 553 I=2,N
J=I-1
AVEL=(VEL(I)+VEL(J))*0.005
553 AVT(J)=AVEL*DIST*(SD(I)-SD(J))*1.0E-03
NM=NM-1
VT=0.
DO 57 I=1,NM
57 VT=VT+AVT(I)

IF STATION A IS TO THE RIGHT OF STATION B AS AN OBSERVER LOOKS AT
THE PLANE OF THE STATIONS, A POSITIVE CURRENT FLOWS AWAY FROM THE
OBSERVER.

58 WRITE (6,10)
N=N-1
DO 60 I=1,N

```

C
C
C
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C


```

60 WRITE (6,11) SD(I),ADH(I),BDH(I),AMB(I),RVEL(I),VEL(I),AVT(I)
   N=N+1
   I=N
   WRITE (6,11) SD(I),ADH(I),BDH(I),AMB(I),RVEL(I),VEL(I)
   NNN=N
   WRITE(6,15)
   WRITE(6,14)VT,BASE
100 FORMAT(1X,F4.0,2F8.3,F9.2,F7.0,2F5.0,F7.2,F8.2,F10.5,2I4)
110 FORMAT(1X,'SD',5X,'SS',6X,'SGT',6X,'VEL',5X,'VEL',3X,'ADH',2X,
110 1,'BDH',3X,'ST',5X,'RVEL',5X,'AVT',4X,'J',3X,'K',//)
120 FORMAT(1I1)
125 FORMAT(10)
130 FORMAT(1X,F4.0,2F8.3,F9.2,F7.0,2F5.0,F7.2,F8.2,10X,2I4)
      K=1
5  FORMAT(1X,' KB = ',I4,//)
      WRITE(6,5) KB
45 DO 50 J=1,N,2
   ADH(J)=(ADH(N)-ADH(J))*100
   BDH(J)=(BDH(N)-BDH(J))*100
   WRITE(6,100) SD(J),ASS(KB),ASGT(KB),VEL(J),VEL(J),ADH(J),BDH(J),
1 1AST(KB),RVEL(J),AVT(J),J,K
   WRITE(7,100) SD(J),ASS(KB),ASGT(KB),VEL(J),VEL(J),ADH(J),BDH(J),
1 1AST(KB),RVEL(J),AVT(J),J,K
   K=K+1
   JSCAR=J
   KB=KB+2
50 CONTINUE
   J=JSCAR+1
   KB=KB-1
   ADH(N)=0.0
   BDH(N)=0.0
1 1WRITE(6,130) SD(N),ASS(KB),ASGT(KB),VEL(N),VEL(N),ADH(N),BDH(N),
1 1AST(KB),RVEL(N),J,K
1 1WRITE(7,130) SD(N),ASS(KB),ASGT(KB),VEL(N),VEL(N),ADH(N),BDH(N),
1 1AST(KB),RVEL(N),J,K
   KB=KB+1
70 RETURN
   END

```



```

SUBROUTINE DISTSTA(SATI,ONGI,SATII,ONGII,X2,DIST)
IMPLICIT REAL*4 (K)
REAL*8 A,E
DATA A/111132.09/,B/566.05/,C/1.20/,D/.002/
DATA E/1111415.13/,F/94.55/,G/.012/
10 FORMAT (10X,'MEAN LATITUDE = ',F6.2/15X,'DISTANCE = ',F6.2,
1, ' KILOMETERS.'/)
CCN=2*3.1416/360
AATII=SATII*CON
$MERI=A-B*COS(2*AATII)+C*COS(4*AATII)-D*COS(6*AATII)
PARI=E-COS(AATII)-F*COS(3*AATII)+G*COS(5*AATII)
$MERII=A-B*COS(2*AATII)+C*COS(4*AATII)-D*COS(6*AATII)
PARIIE=E-COS(AATII)-F*COS(3*AATII)+G*COS(5*AATII)
ALLAT=($MERI+$MERII)/2
ALLCN=(PARI+PARII)/2
DLAT=SATI-SATII
DLON=ONGI-ONGII
KLAT=DLAT*ALLAT/1000
KLONG=DLON*ALLON/1000
KDIX=SQRT(KLAT**2+KLONG**2)
DIST=1.458E-4
PSI=(SATI+SATII)*0.5
PSJ=(2.*3.14159/360.)*PSI
SPSI=SIN(PSJ)
IF(SPSI.LT.0.1) SPSI=0.1
X2=1./((W2*SPSI*KDIX)
WRITE(6,10) PSI,KDIX
RETURN
END

```



```

SUBROUTINE LGTP(N,D,V,SD,CV,NN)
DIMENSION D(N),V(N),CV(98),SD(98)
111 DO 188 J=1,98
112 DO 186 I=1,N
115 IF(SD(J)-D(N))113,115,190
115 CV(J)=V(N)
GO TO 191
113 IF(SD(J)-D(I))114,114,116
114 CV(J)=V(I)
GO TO 188
116 IF(SD(J)-D(I+1))120,118,186
118 CV(J)=V(I+1)
GO TO 188
120 IF(I-1)132,132,126
126 XA=(SD(J)-D(I))*SD(J)-D(I+1))*V(I-1)/
1((D(I-1)-D(I))*D(I-1))*SD(J)-D(I+1))*V(I)/
1((D(I)-D(I-1))*D(I-1))*SD(J)-D(I+1))
1XC=(SD(J)-D(I-1))*SD(J)-D(I+1))*V(I+1)/
1((D(I+1)-D(I-1))*D(I+1))-D(I))
ANSU=XA+XB+XC
132 IF(I+2)-N)133,133,134
133 YA=(SD(J)-D(I+1))*SD(J)-D(I+2))*V(I)/
1((D(I)-D(I+1))*D(I+1))*SD(J)-D(I+2))
1YB=(SD(J)-D(I+1))*SD(J)-D(I+2))*V(I+1)/
1((D(I+1)-D(I+1))*D(I+1))-D(I+2))
1YC=(SD(J)-D(I+1))*SD(J)-D(I+2))*V(I+2)/
1((D(I+2)-D(I+1))*D(I+2))-D(I+1))
ANSD=YA+YB+YC
134 ZA=(SD(J)-D(I+1))*V(I)/(D(I)-D(I+1))
ZB=(SD(J)-D(I+1))*V(I+1)/(D(I+1)-D(I))
ANSL=ZA+ZB
136 IF(I-1)136,136,138
136 CV(J)=(ANSD+ANSL)/2.
DLL=(ANSD+ANSL+ANSL)/3.
GO TO 188
138 IF(I+2)-N)140,140,142
140 CV(J)=(ANSU+ANSD+ANSL)/3.
UD=(ANSU+ANSD)/2.
GO TO 188
142 CV(J)=(ANSU+ANSL)/2.
ULL=(ANSU+ANSL+ANSL)/3.
GO TO 188

```



```
186 CONTINUE  
188 CONTINUE  
190 J=J-1  
191 NN=J  
    RETURN  
    END
```



```

SUBROUTINE SNDVEL (T,S,D,SVL)
IF(D.LE.100.) GO TO 10
IF(D.LE.200.) GO TO 20
IF(D.LE.400.) GO TO 30
IF(D.LE.700.) GO TO 40
IF(D.LE.1500.) GO TO 50
IF(D.LE.2000.) GO TO 60
P=D*(.10318+(D-2000.)*2.6E-7)
GL TO 5
10 P=D*(.10245+D*3.0E-7)
GO TO 5
20 P=D*(.10248+(D-100.)*7.0E-7)
GO TO 5
30 P=D*(.10255+(D-200.)*6.0E-7)
GO TO 5
40 P=D*(.10267+(D-400.)*4.33E-7)
GO TO 5
50 P=D*(.10280+(D-700.)*3.0E-7)
GO TO 5
60 P=D*(.10304+(D-1500.)*2.7E-7)
5 CONTINUE
VT=I*(4.5721-T*(.044532-T*(2.6045E-4+T*(7.9851E-6))))
VP=P*(.160272+P*(1.0268E-5+P*(3.5216E-9-P*(3.3603E-12))))
VS=(S-35.)*(.1.39799+(S-35.)*1.69202E-3)
A1=I*(-.011244+3.1580E-8*P+T*(7.7711E-7+1.5790E-9*P))
A2=P*(7.7016E-5-1.2943E-7*P)
A3=P*P*(.1.8607E-4+T*(7.4812E-6+T*(4.5283E-8)))
A4=P*P*P*(T*(-2.5294E-7+T*1.8563E-9)+P*T*(-1.9646E-10))
SVL=1449.14+VT+VP+VS+(S-35.)*(A1+A2)+A3+A4
RETURN
END

```



```

SUBROUTINE SGT(SVA(I,S,D,SGT,SV,SVA)
SI=-((I-3.98)**2)/503.57)*(I+283.)/(I+67.26))
CL=(S-.030)/1.805
SO=-.069+1.4708*CL-.00157*CL**2+3.98E-5*CL**3
      ALTERNATE METHOD OF COMPUTING SIGMA-ZERO:
SO=-0.093+0.8149*S-.000482*S**2+6.8E-6*S**3
AT=T*(4.7867-.098185*T+.0010843*T**2)*1.E-3
BT=T*(18.030-.8164*T+.01667*T**2)*1.E-6
SGT=SI+(SO+.1324)*(1.-AT+BT*(SO-.1324))
AFST=1./((1.+SGT*1.E-3)
A=D*AFST*1.E-9
B=4886./((1.+1.83E-5*D)
C=227.+28.33*T-.551*T**2+.004*T**3
E=D*1.E-4
G=(SO-28.)/10.
H=147.3-2.72*T+.04*T**2
U=105.5+9.5*T-.158*T**2
V=1.5*D**2*T*1.E-8
W=32.4-.87*T+.02*T**2
X=4.5-.1*T
Y=1.8-.06*T
SV=AFST-A*(B-C+E*U-V-G*(H-E*W)+G**2*(X-E*Y))
AZ=.972643
YA=-227.+01055*D
YB=.0126*(147.5-.00324*D)
AP=AZ-D*AZ*(B+YA-YB)*1.E-9
SVA=SV-AP
RETURN
END

```

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